Stormwater Management Report

Definitive Subdivision Plan of 27 Charge Pond Road

27 Charge Pond Road Wareham, Massachusetts

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Prepared by:



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1.0 INTRODUCTION

The proposed project includes a stormwater management system designed to mitigate potential impacts the proposed project could have on the existing watershed. Stormwater controls have been proposed to control peak runoff rates, provide water quality, promote groundwater recharge and sediment removal. The proposed system has been designed to comply with:

- The 2008 Massachusetts Department of Environmental Protection (DEP) Stormwater Management Handbook,
- The Massachusetts Wetland Protection Act (310 CMR 10.00)
- Town of Wareham Rules & Regulations Governing the Subdivision of Land

The pre- and post-development hydrologic conditions were modeled using HydroCAD[™] version 10.10 to demonstrate that post-development stormwater runoff rates will be less than or equal to the pre-development rates. Watershed maps with soil types as well as detailed analysis of the model results are also included. The following table summarizes the peak runoff rates for the pre- and post-development conditions.

Storm	2 Y	ear	10 \	/ear	25 ۱	/ear	50 \	/ear	100	Year
Event	Pre	Post	Pre	Post	Pre	Post	Pre	Post	Pre	Post
DP-1	0.00	0.00	0.73	0.73	3.85	3.85	10.76	10.76	23.07	23.07
DP-2	0.00	0.00	0.00	0.00	0.03	0.03	0.10	0.10	0.49	0.49
DP-3	0.00	0.00	0.00	0.00	0.04	0.04	0.12	0.12	0.60	0.60
DP-4	0.00	0.00	0.01	0.01	0.07	0.06	0.23	0.22	0.98	0.96
DP-5	0.00	0.00	0.00	0.00	0.04	0.04	0.12	0.12	0.62	0.62
DP-6	0.00	0.00	0.01	0.01	0.13	0.13	0.43	0.43	1.84	1.84
DP-7	0.00	0.00	0.00	0.00	0.03	0.03	0.12	0.12	0.49	0.49

Table 1: Pre- & Post-development Peak Runoff Rate Comparison, units are in cubic feet per second (cfs).

2.0 PRE-DEVELOPMENT CONDITIONS

2.1 Site Conditions

The existing site is generally forested and undeveloped, although a previously cleared/disturbed area, is located in the northeastern portion of the Site. According to the Wareham Assessor's Office, the Property is comprised of two discontinuous areas lying east and west of Parker Mills Pond. The area of the proposed roadway, infrastructure, and subdivided lots (the Site), which consists of forested uplands typical of this region, is located west of Charge Pond Road. The Site can be accessed via Charge Pond Road, an existing public way.

The general topography of the Site slopes east to west with exceptions in the form of isolated depressions throughout, some of which contain wetland resource areas. The primary design point, DP-1, used for the stormwater analysis represents flows to Parker Mills Pond. Additional design points include DP-2, which represents flows to the south to an adjacent property containing a natural gas distribution facility. DP-3, 4, 5, and 6 consider flows to existing depressions that contain resource areas. DP-7 represents flows to the east onto a Town owned parcel with ball fields.

The site does not contain, nor is it tributary to any Critical Areas.

The site does not discharge to a surface water with a TMDL or draft TMDL.

2.2 Soil Description

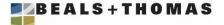
The Natural Resources Conservation Service (NRCS) lists the on-site soils types as predominantly hydrologic soil class A. These soil groups include Windsor loamy sand, Deerfield loamy fine sand, and Udipsamments. Another area partially on site but mostly in the Town's ball fields, is mapped as Udorthents, refuse substratum, which is considered hydrologic soil class B. Finally, a small area of hydrologic soil class D soils is present at the southwestern corner of the proposed project locus, which is mapped as Scarboro muck, coastal lowland.

Windsor loamy sand is an excessively drained soil comprised of loose sandy glaciofluvial deposits. Generally, this soil is in outwash plains, dunes and terrace landforms, and has a loamy sand top and subsoil layer over top of sand. Deerfield loamy sand is a moderately well drained soil that is characterized by sandy outwash deposits. Udorthents, refuse substratum is filled loamy land over man made land. Udipsamments are areas of sandy human transported material over gravelly glaciofluvial deposits. Scarboro muck is poorly drained soil found in outwash terrace depressions and drainage ways.



2.3 Hydrologic Analysis

Sub-catchment areas were delineated based on existing runoff patterns and topographic information. This information is shown on the *Pre-Development Conditions Hydrologic Areas Map* included in Attachment 2. Summaries of each area with respect to Curve Number and Time of Concentration calculations can be found in the model results also in Attachment 2.



3.0 POST-DEVELOPMENT CONDITIONS

3.1 Design Strategy

During the design phase of the site layout, consideration was given to conserving environmentally sensitive features and minimizing impact on the existing hydrology. To achieve this, extensive grading was avoided, and the site was designed to match the existing terrain where feasible. Minimizing earthwork helps to maintain the existing drainage patterns to the maximum extent practicable under post-development conditions.

Wetlands in the vicinity of the site were excluded from the development envelope and will not be altered by the proposed project. The hydrologic analysis considers these wetlands in order to maintain their existing hydrology.

Through careful site planning the proposed impervious surfaces have been minimized, reducing the impact the project may have on the existing watershed. This minimization of impervious surfaces was achieved without compromising compliance to local bylaw requirements.

A stormwater management system has been designed to provide treatment for stormwater runoff associated with the proposed impervious surfaces on site. All stormwater BMPs were designed to treat a minimum of the first 1.0 inch of runoff generated by the on-site impervious areas. Proprietary stormwater treatment systems were designed to treat the runoff rate associated with the water quality volume in accordance with the requirements of the DEP Stormwater Handbook. Stormwater BMP sizing worksheets and water quality sizing calculations are included in Attachment 5 of this report.

To mitigate increased stormwater flow rates associated with the proposed impervious area, a modified depression has been proposed. The modified depression will discharge to the adjacent wetland system, consistent with the existing hydrology of the site.

3.2 Hydrologic Analysis

The established design points used in the pre-development conditions analysis were used in the post-development analysis for direct comparison. The tributary areas and flow paths were modified to reflect post-development conditions. See Attachment 3 for the *Post- Development Conditions Hydrologic Areas Map.* Summaries of each area with respect to Curve Number and Time of Concentration calculations can be found in the model results in Attachment 3.



3.3 Hydraulic Calculations

In compliance with Town of Wareham requirements, the proposed storm drain system was analyzed based on the 50-year storm event using the Rational Formula. A watershed map and detailed hydraulic analysis are provided in Attachment 4.

3.4 Compliance with DEP Stormwater Management Standards

The proposed stormwater management system was designed in compliance with the ten (10) DEP Stormwater Management Standards. The following summary provides key information related to the proposed stormwater management system, its design elements, and mitigation measures for potential impacts.



STANDARD 1: No new stormwater conveyance (e.g. outfalls) may discharge untreated stormwater directly to or cause erosion in wetlands or waters of the Commonwealth.

There will be no direct discharge of untreated stormwater to nearby wetlands or waters of the Commonwealth. Runoff from all impervious areas of the site will be conveyed to stormwater management controls for infiltration, water quality treatment, and runoff rate attenuation prior to discharge to adjacent wetlands.

STANDARD 2: Stormwater management systems shall be designed so that postdevelopment peak discharge rates do not exceed pre-development peak discharge rates.

The stormwater management design will control post-development peak discharge rates for the 2-, 10-, 25-, 50- and 100-year, 24-hour storms so as to maintain pre-development peak discharge rates. Refer to Section 1.0 Introduction for a summary of the peak runoff rates.

STANDARD 3: Loss of annual recharge to groundwater shall be eliminated or minimized through the use of environmentally sensitive site design, low impact development techniques, stormwater management practices and good operation and maintenance. At a minimum, the annual recharge from the post-development site shall approximate the annual recharge from pre-development conditions based on soil types. This Standard is met when the stormwater management system is designed to infiltrate the required recharge volume as determined in accordance with the Massachusetts Stormwater Handbook.

The stormwater management system includes a modified depression that will effectively recharge groundwater on-site. Infiltration BMPs were sized using the static method based on the required recharge volume for the post-development site. As a result, annual recharge from the post-development site will approximate the annual recharge from the site under predevelopment conditions. See Attachment 5 for stormwater BMP design worksheets and Groundwater Recharge Calculation.



STANDARD 4: Stormwater management systems shall be designed to remove 80% of the average annual post-construction load of Total Suspended Solids (TSS).

The proposed project will meet the water quality requirements of Standard 4 using several onsite treatment trains that achieve 80% TSS removal. Refer to Attachment 5 for the TSS removal worksheets. Structural BMPs designed for water quality treatment, including the deep sump hooded catch basins and Contech[®] water quality treatment systems, were sized to capture and treat the flow rate associated with the first 1.0-inch of runoff from proposed impervious surfaces. All proposed stormwater management BMPs will be operated and maintained to ensure continued water quality treatment of runoff. The Site Owner's Manual complies with the Long-Term Pollution Prevention Plan (Standard 4) and the Long-Term Operation and Maintenance Plan (Standard 9) requirements of the 2008 Massachusetts Department of Environmental Protection (MassDEP) Stormwater Management Standards. The Manual outlines source control and pollution prevention measures and maintenance requirements of stormwater best management practices (BMPs) associated with the proposed development.

STANDARD 5: For land uses with higher potential pollutant loads (LUHPPLs), source control and pollution prevention shall be implemented in accordance with the Massachusetts Stormwater Handbook to eliminate or reduce the discharge of stormwater runoff from such land uses to the maximum extent practicable.

The proposed project is not associated with stormwater discharges from land uses with higher potential pollutant loads.

STANDARD 6:Stormwater discharges to critical areas must utilize certain stormwater
management BMPs approved for critical areas. Critical areas are
Outstanding Resource Waters, shellfish beds, swimming beaches,
coldwater fisheries and recharge areas for public water supplies.

There are no stormwater discharges to critical areas associated with this project.



STANDARD 7: Redevelopment of previously developed sites must meet the Stormwater Management Standards to the maximum extent practicable. However, if it is not practicable to meet all the Standards, new (retrofitted or expanded) stormwater management systems must be designed to improve existing conditions.

The proposed project is new development, and therefore this standard does not apply.

STANDARD 8: A plan to control construction-related impacts during erosion, sedimentation and other pollutant sources during construction and land disturbance activities (construction period erosion, sedimentation, and pollution prevention plan) shall be developed and implemented.

A Stormwater Pollution Prevention Plan (SWPPP) will be developed prior to construction to comply with Section 3 of the NPDES Construction General Permit for Stormwater Discharges; therefore the requirements of Standard 8 are fulfilled.

STANDARD 9: A Long-Term Operation and Maintenance (O&M) Plan shall be developed and implemented to ensure that stormwater management systems function as designed.

The Site Owner's Manual complies with the Long-Term Pollution Prevention Plan (Standard 4) and the Long-Term Operation and Maintenance Plan (Standard 9) requirements of the 2008 Massachusetts Department of Environmental Protection (MassDEP) Stormwater Management Standards. The Manual outlines source control and pollution prevention measures and maintenance requirements of the stormwater best management practices (BMPs) associated with the proposed development.

STANDARD 10: All illicit discharges to the stormwater management system are prohibited.

There will be no illicit discharges to the proposed stormwater management system associated with the proposed project. An Illicit Discharge Compliance Statement is provided on the following page.



3.5 Illicit Discharge Compliance Statement

An illicit discharge is any discharge to a stormwater management system that is not comprised entirely of stormwater, discharges from fire-fighting activities, and certain non-designated non-stormwater discharges.

To the best of my knowledge, no detectable illicit discharge exists on site. The site plans included with this report detail the storm sewers that convey stormwater on the site and demonstrate that these systems do not include the entry of an illicit discharge. A Site Owner's Manual is also included, which contains the Long Term Pollution Plan that outlines measures to prevent future illicit discharges. As the Site Owner, I will ultimately be responsible for implementing the Long Term Pollution Plan.

Signature:

's Name



Massachusetts Department of Environmental Protection Bureau of Resource Protection - Wetlands Program Checklist for Stormwater Report

A. Introduction

Important: When filling out forms on the computer, use only the tab key to move your cursor - do not use the return key.



A Stormwater Report must be submitted with the Notice of Intent permit application to document compliance with the Stormwater Management Standards. The following checklist is NOT a substitute for the Stormwater Report (which should provide more substantive and detailed information) but is offered here as a tool to help the applicant organize their Stormwater Management documentation for their Report and for the reviewer to assess this information in a consistent format. As noted in the Checklist, the Stormwater Report must contain the engineering computations and supporting information set forth in Volume 3 of the Massachusetts Stormwater Handbook. The Stormwater Report must be prepared and certified by a Registered Professional Engineer (RPE) licensed in the Commonwealth.

The Stormwater Report must include:

- The Stormwater Checklist completed and stamped by a Registered Professional Engineer (see page 2) that certifies that the Stormwater Report contains all required submittals.¹ This Checklist is to be used as the cover for the completed Stormwater Report.
- Applicant/Project Name
- Project Address
- Name of Firm and Registered Professional Engineer that prepared the Report
- Long-Term Pollution Prevention Plan required by Standards 4-6
- Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan required by Standard 8²
- Operation and Maintenance Plan required by Standard 9

In addition to all plans and supporting information, the Stormwater Report must include a brief narrative describing stormwater management practices, including environmentally sensitive site design and LID techniques, along with a diagram depicting runoff through the proposed BMP treatment train. Plans are required to show existing and proposed conditions, identify all wetland resource areas, NRCS soil types, critical areas, Land Uses with Higher Potential Pollutant Loads (LUHPPL), and any areas on the site where infiltration rate is greater than 2.4 inches per hour. The Plans shall identify the drainage areas for both existing and proposed conditions at a scale that enables verification of supporting calculations.

As noted in the Checklist, the Stormwater Management Report shall document compliance with each of the Stormwater Management Standards as provided in the Massachusetts Stormwater Handbook. The soils evaluation and calculations shall be done using the methodologies set forth in Volume 3 of the Massachusetts Stormwater Handbook.

To ensure that the Stormwater Report is complete, applicants are required to fill in the Stormwater Report Checklist by checking the box to indicate that the specified information has been included in the Stormwater Report. If any of the information specified in the checklist has not been submitted, the applicant must provide an explanation. The completed Stormwater Report Checklist and Certification must be submitted with the Stormwater Report.

¹ The Stormwater Report may also include the Illicit Discharge Compliance Statement required by Standard 10. If not included in the Stormwater Report, the Illicit Discharge Compliance Statement must be submitted prior to the discharge of stormwater runoff to the post-construction best management practices.

² For some complex projects, it may not be possible to include the Construction Period Erosion and Sedimentation Control Plan in the Stormwater Report. In that event, the issuing authority has the discretion to issue an Order of Conditions that approves the project and includes a condition requiring the proponent to submit the Construction Period Erosion and Sedimentation Control Plan before commencing any land disturbance activity on the site.



B. Stormwater Checklist and Certification

The following checklist is intended to serve as a guide for applicants as to the elements that ordinarily need to be addressed in a complete Stormwater Report. The checklist is also intended to provide conservation commissions and other reviewing authorities with a summary of the components necessary for a comprehensive Stormwater Report that addresses the ten Stormwater Standards.

Note: Because stormwater requirements vary from project to project, it is possible that a complete Stormwater Report may not include information on some of the subjects specified in the Checklist. If it is determined that a specific item does not apply to the project under review, please note that the item is not applicable (N.A.) and provide the reasons for that determination.

A complete checklist must include the Certification set forth below signed by the Registered Professional Engineer who prepared the Stormwater Report.

Registered Professional Engineer's Certification

I have reviewed the Stormwater Report, including the soil evaluation, computations, Long-term Pollution Prevention Plan, the Construction Period Erosion and Sedimentation Control Plan (if included), the Longterm Post-Construction Operation and Maintenance Plan, the Illicit Discharge Compliance Statement (if included) and the plans showing the stormwater management system, and have determined that they have been prepared in accordance with the requirements of the Stormwater Management Standards as further elaborated by the Massachusetts Stormwater Handbook. I have also determined that the information presented in the Stormwater Checklist is accurate and that the information presented in the Stormwater Report accurately reflects conditions at the site as of the date of this permit application.

Registered Professional Engineer Block and Signature



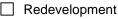
11/19/2021

Signature and Date

Checklist

Project Type: Is the application for new development, redevelopment, or a mix of new and redevelopment?

New development



Mix of New Development and Redevelopment



LID Measures: Stormwater Standards require LID measures to be considered. Document what environmentally sensitive design and LID Techniques were considered during the planning and design of the project:

\boxtimes	No disturbance to any Wetland Resource Areas
	Site Design Practices (e.g. clustered development, reduced frontage setbacks)
	Reduced Impervious Area (Redevelopment Only)
\boxtimes	Minimizing disturbance to existing trees and shrubs
	LID Site Design Credit Requested:
	Credit 1
	Credit 2
	Credit 3
	Use of "country drainage" versus curb and gutter conveyance and pipe
	Bioretention Cells (includes Rain Gardens)
	Constructed Stormwater Wetlands (includes Gravel Wetlands designs)
	Treebox Filter
	Water Quality Swale
	Grass Channel
	Green Roof
	Other (describe):

Standard 1: No New Untreated Discharges

- No new untreated discharges
- \boxtimes Outlets have been designed so there is no erosion or scour to wetlands and waters of the Commonwealth
- Supporting calculations specified in Volume 3 of the Massachusetts Stormwater Handbook included.



Standard 2: Peak Rate Attenuation

- Standard 2 waiver requested because the project is located in land subject to coastal storm flowage and stormwater discharge is to a wetland subject to coastal flooding.
- Evaluation provided to determine whether off-site flooding increases during the 100-year 24-hour storm.

Calculations provided to show that post-development peak discharge rates do not exceed predevelopment rates for the 2-year and 10-year 24-hour storms. If evaluation shows that off-site flooding increases during the 100-year 24-hour storm, calculations are also provided to show that post-development peak discharge rates do not exceed pre-development rates for the 100-year 24hour storm.

Standard 3: Recharge

Soil Analysis provided.

- Required Recharge Volume calculation provided.
- Required Recharge volume reduced through use of the LID site Design Credits.
- Sizing the infiltration, BMPs is based on the following method: Check the method used.

\bowtie	Static
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Dynamic Field¹

 \boxtimes Runoff from all impervious areas at the site discharging to the infiltration BMP.

Simple Dynamic

Runoff from all impervious areas at the site is *not* discharging to the infiltration BMP and calculations are provided showing that the drainage area contributing runoff to the infiltration BMPs is sufficient to generate the required recharge volume.

Recharge BMPs have been sized to infiltrate the Required Recharge Volume.

Recharge BMPs have been sized to infiltrate the Required Recharge Volume only to the maximum
extent practicable for the following reason:

- Site is comprised solely of C and D soils and/or bedrock at the land surface
- M.G.L. c. 21E sites pursuant to 310 CMR 40.0000
- Solid Waste Landfill pursuant to 310 CMR 19.000
- Project is otherwise subject to Stormwater Management Standards only to the maximum extent practicable.
- \boxtimes Calculations showing that the infiltration BMPs will drain in 72 hours are provided.

Property includes a M.G.L. c. 21E site or a solid waste landfill and a mounding analysis is included.

¹ 80% TSS removal is required prior to discharge to infiltration BMP if Dynamic Field method is used.



Standard 3: Recharge (continued)

The infiltration BMP is used to attenuate peak flows during storms greater than or equal to the 10year 24-hour storm and separation to seasonal high groundwater is less than 4 feet and a mounding analysis is provided.

Documentation is provided showing that infiltration BMPs do not adversely impact nearby wetland resource areas.

Standard 4: Water Quality

The Long-Term Pollution Prevention Plan typically includes the following:

- Good housekeeping practices;
- Provisions for storing materials and waste products inside or under cover;
- Vehicle washing controls;
- Requirements for routine inspections and maintenance of stormwater BMPs;
- Spill prevention and response plans;
- Provisions for maintenance of lawns, gardens, and other landscaped areas;
- Requirements for storage and use of fertilizers, herbicides, and pesticides;
- Pet waste management provisions;
- Provisions for operation and management of septic systems;
- Provisions for solid waste management;
- Snow disposal and plowing plans relative to Wetland Resource Areas;
- Winter Road Salt and/or Sand Use and Storage restrictions;
- Street sweeping schedules;
- Provisions for prevention of illicit discharges to the stormwater management system;
- Documentation that Stormwater BMPs are designed to provide for shutdown and containment in the event of a spill or discharges to or near critical areas or from LUHPPL;
- Training for staff or personnel involved with implementing Long-Term Pollution Prevention Plan;
- List of Emergency contacts for implementing Long-Term Pollution Prevention Plan.
- A Long-Term Pollution Prevention Plan is attached to Stormwater Report and is included as an attachment to the Wetlands Notice of Intent.
- Treatment BMPs subject to the 44% TSS removal pretreatment requirement and the one inch rule for calculating the water quality volume are included, and discharge:
 - is within the Zone II or Interim Wellhead Protection Area
 - is near or to other critical areas
 - is within soils with a rapid infiltration rate (greater than 2.4 inches per hour)
 - involves runoff from land uses with higher potential pollutant loads.
- The Required Water Quality Volume is reduced through use of the LID site Design Credits.
- Calculations documenting that the treatment train meets the 80% TSS removal requirement and, if applicable, the 44% TSS removal pretreatment requirement, are provided.



Cł	necklist (continued)
Sta	ndard 4: Water Quality (continued)
\square	The BMP is sized (and calculations provided) based on:
	The ½" or 1" Water Quality Volume or
	The equivalent flow rate associated with the Water Quality Volume and documentation is provided showing that the BMP treats the required water quality volume.
	The applicant proposes to use proprietary BMPs, and documentation supporting use of proprietary BMP and proposed TSS removal rate is provided. This documentation may be in the form of the propriety BMP checklist found in Volume 2, Chapter 4 of the Massachusetts Stormwater Handbook and submitting copies of the TARP Report, STEP Report, and/or other third party studies verifying performance of the proprietary BMPs.
	A TMDL exists that indicates a need to reduce pollutants other than TSS and documentation showing that the BMPs selected are consistent with the TMDL is provided.
Sta	ndard 5: Land Uses With Higher Potential Pollutant Loads (LUHPPLs)
	The NPDES Multi-Sector General Permit covers the land use and the Stormwater Pollution Prevention Plan (SWPPP) has been included with the Stormwater Report. The NPDES Multi-Sector General Permit covers the land use and the SWPPP will be submitted prior to the discharge of stormwater to the post-construction stormwater BMPs.
	The NPDES Multi-Sector General Permit does <i>not</i> cover the land use.
	LUHPPLs are located at the site and industry specific source control and pollution prevention measures have been proposed to reduce or eliminate the exposure of LUHPPLs to rain, snow, snow melt and runoff, and been included in the long term Pollution Prevention Plan.
	All exposure has been eliminated.
	All exposure has <i>not</i> been eliminated and all BMPs selected are on MassDEP LUHPPL list.
	The LUHPPL has the potential to generate runoff with moderate to higher concentrations of oil and grease (e.g. all parking lots with >1000 vehicle trips per day) and the treatment train includes an oil grit separator, a filtering bioretention area, a sand filter or equivalent.

Standard 6: Critical Areas

- The discharge is near or to a critical area and the treatment train includes only BMPs that MassDEP has approved for stormwater discharges to or near that particular class of critical area.
- Critical areas and BMPs are identified in the Stormwater Report.



Standard 7: Redevelopments and Other Projects Subject to the Standards only to the maximum extent practicable

The project is subject to the Stormwater Management Standards only to the maximum Extent Practicable as a:

Limited Project	ct
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- Small Residential Projects: 5-9 single family houses or 5-9 units in a multi-family development provided there is no discharge that may potentially affect a critical area.
- Small Residential Projects: 2-4 single family houses or 2-4 units in a multi-family development with a discharge to a critical area
- Marina and/or boatyard provided the hull painting, service and maintenance areas are protected from exposure to rain, snow, snow melt and runoff
- Bike Path and/or Foot Path
- Redevelopment Project
- Redevelopment portion of mix of new and redevelopment.
- Certain standards are not fully met (Standard No. 1, 8, 9, and 10 must always be fully met) and an explanation of why these standards are not met is contained in the Stormwater Report.

☐ The project involves redevelopment and a description of all measures that have been taken to improve existing conditions is provided in the Stormwater Report. The redevelopment checklist found in Volume 2 Chapter 3 of the Massachusetts Stormwater Handbook may be used to document that the proposed stormwater management system (a) complies with Standards 2, 3 and the pretreatment and structural BMP requirements of Standards 4-6 to the maximum extent practicable and (b) improves existing conditions.

Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan must include the following information:

- Narrative;
- Construction Period Operation and Maintenance Plan;
- Names of Persons or Entity Responsible for Plan Compliance;
- Construction Period Pollution Prevention Measures;
- Erosion and Sedimentation Control Plan Drawings;
- Detail drawings and specifications for erosion control BMPs, including sizing calculations;
- Vegetation Planning;
- Site Development Plan;
- Construction Sequencing Plan;
- Sequencing of Erosion and Sedimentation Controls;
- Operation and Maintenance of Erosion and Sedimentation Controls;
- Inspection Schedule;
- Maintenance Schedule;
- Inspection and Maintenance Log Form.

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan containing the information set forth above has been included in the Stormwater Report.



Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control (continued)

- ☐ The project is highly complex and information is included in the Stormwater Report that explains why it is not possible to submit the Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan with the application. A Construction Period Pollution Prevention and Erosion and Sedimentation Control has *not* been included in the Stormwater Report but will be submitted *before* land disturbance begins.
- The project is *not* covered by a NPDES Construction General Permit.
- The project is covered by a NPDES Construction General Permit and a copy of the SWPPP is in the Stormwater Report.
- The project is covered by a NPDES Construction General Permit but no SWPPP been submitted. The SWPPP will be submitted BEFORE land disturbance begins.

Standard 9: Operation and Maintenance Plan

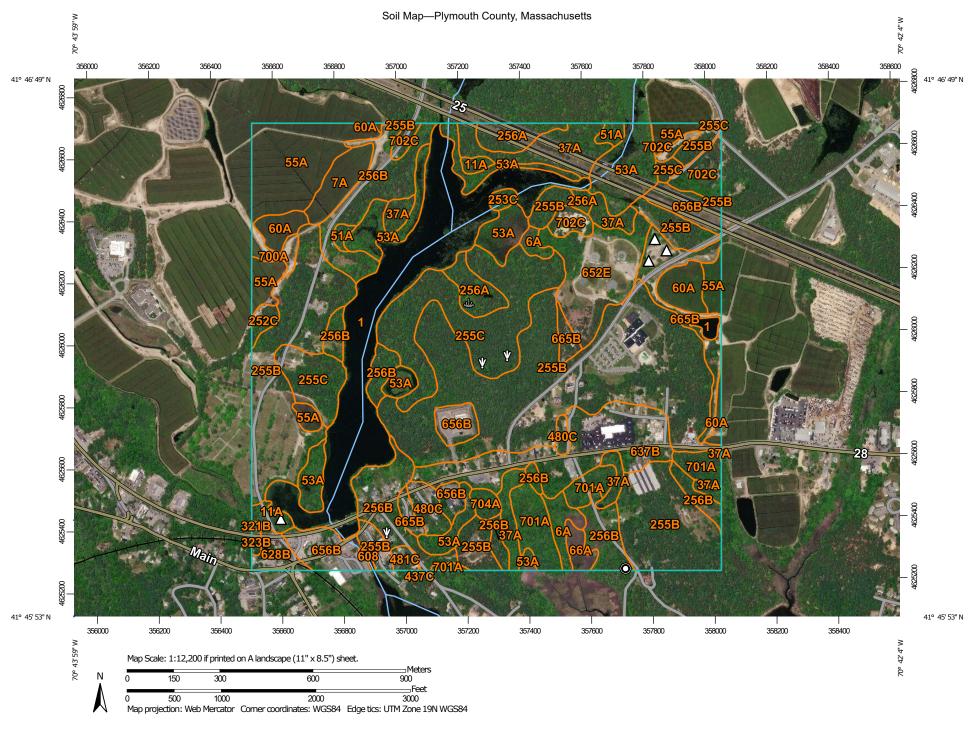
- The Post Construction Operation and Maintenance Plan is included in the Stormwater Report and includes the following information:
 - Name of the stormwater management system owners;
 - Party responsible for operation and maintenance;
 - Schedule for implementation of routine and non-routine maintenance tasks;
 - Plan showing the location of all stormwater BMPs maintenance access areas;
 - Description and delineation of public safety features;
 - Estimated operation and maintenance budget; and
 - Operation and Maintenance Log Form.
- The responsible party is **not** the owner of the parcel where the BMP is located and the Stormwater Report includes the following submissions:
 - A copy of the legal instrument (deed, homeowner's association, utility trust or other legal entity) that establishes the terms of and legal responsibility for the operation and maintenance of the project site stormwater BMPs;
 - A plan and easement deed that allows site access for the legal entity to operate and maintain BMP functions.

Standard 10: Prohibition of Illicit Discharges

- The Long-Term Pollution Prevention Plan includes measures to prevent illicit discharges;
- An Illicit Discharge Compliance Statement is attached;
- NO Illicit Discharge Compliance Statement is attached but will be submitted *prior to* the discharge of any stormwater to post-construction BMPs.

Attachment 1 Soil Data





USDA Natural Resources

Conservation Service

	MAP L	EGEND		MAP INFORMATION		
Soils Soil Soil Soil Special Point Special Point Special Borr	: (AOI) a of Interest (AOI) I Map Unit Polygons I Map Unit Lines I Map Unit Points	کاری کاری Water Fea	Spoil Area Stony Spot Very Stony Spot Wet Spot Other Special Line Features tures Streams and Canals ation	The soil surveys that comprise your AOI were mapped at 1:12,000. Please rely on the bar scale on each map sheet for map measurements. Source of Map: Natural Resources Conservation Service Web Soil Survey URL: Coordinate System: Web Mercator (EPSG:3857) Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.		
 ◇ Clos ◇ Gravity ◇ Gravity ◇ Land ▲ Land ▲ Maring ◇ Mino ○ Perevision ◇ Rooon + Salii ◇ Sani 	sed Depression vel Pit velly Spot	H H Backgrou	Rails Interstate Highways US Routes Major Roads Local Roads nd Aerial Photography	 This product is generated from the USDA-NRCS certified data a of the version date(s) listed below. Soil Survey Area: Plymouth County, Massachusetts Survey Area Data: Version 12, Sep 12, 2019 Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. Date(s) aerial images were photographed: Dec 31, 2009—Jul 2017 The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. 		
☆ Sink }∍ Slid	khole le or Slip lic Spot					

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
1	Water	58.1	10.7%
6A Scarboro muck, coasta lowland, 0 to 3 perce slopes		5.1	0.9%
7A	Rainberry coarse sand, 0 to 3 percent slopes, sanded surface	6.3	1.2%
11A	Rainberry coarse sand, 0 to 3 percent slopes	3.2	0.6%
37A	Massasoit - Mashpee complex, 0 to 3 percent slopes	21.9	4.0%
51A	Swansea muck, 0 to 1 percent slopes	2.2	0.4%
53A	Freetown muck, ponded, 0 to 1 percent slopes	35.3	6.5%
55A Freetown coarse sand, 0 to 3 percent slopes, sanded surface		29.5	5.4%
60A	60A Swansea coarse sand, 0 to 2 percent slopes		1.8%
66A Ipswich - Pawcatuck - Matunuck complex, 0 to 2 percent slopes, very frequently flooded		2.4	0.4%
252C Carver coarse sand, 8 to 15 percent slopes		1.8	0.3%
253C	Hinckley loamy sand, 8 to 15 percent slopes	1.2	0.2%
255B	Windsor loamy sand, 3 to 8 percent slopes	154.3	28.3%
255C	Windsor loamy sand, 8 to 15 percent slopes	41.8	7.7%
256A	Deerfield loamy fine sand, 0 to 3 percent slopes	10.7	2.0%
256B	Deerfield loamy fine sand, 3 to 8 percent slopes	43.2	7.9%
321B Birchwood sand, 3 to 8 percent slopes, very stony		0.2	0.0%
323B	Poquonock sand, 3 to 8 percent slopes, very stony	0.6	0.1%
437C Plymouth loamy coarse sand, 8 to 15 percent slopes, bouldery		0.0	0.0%
480C	Plymouth - Carver complex, 8 to 15 percent slopes	5.0	0.9%

USDA

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
481C Plymouth - Carver complex, 8 to 15 percent slopes, bouldery		1.5	0.3%
608	Water, ocean	0.3	0.1%
628B	Canton - Urban land complex, 0 to 8 percent slopes	3.8	0.7%
637B	Carver - Urban land complex, 0 to 8 percent slopes	26.4	4.9%
652E Udorthents, refuse substratum, 8 to 35 percent slopes		19.4	3.6%
656B Udorthents - Urban land complex, 0 to 8 percent slopes		18.0	3.3%
665B Udipsamments, 0 to 8 percent slopes		13.4	2.5%
700A Udipsamments, wet substratum, 0 to 3 percent slopes		2.6	0.5%
701A Rainberry coarse sand, 0 to 3 percent slope, sanded surface, inactive		14.3	2.6%
702C Udipsamments, 8 to 15 percent slopes		10.0	1.8%
704A	Freetown and Swansea coarse sands, 0 to 3 percent slopes, sanded surface and inactive	1.9	0.3%
Totals for Area of Interest		544.2	100.0%

Attachment 2 Pre-Development Hydrologic Analysis





PRE-DEVELOPMENT CONDITIONS HYDROLOGIC ANALYSIS

OBJECTIVE

To determine the pre-development peak rates of runoff from the site for the 2-, 10-, 25-, 50-, and 100-year storm events.

CONCLUSION

Peak Runoff Rates

The following numbers represent the peak rates of runoff from the site under the pre-development conditions:

Storm	2 Year	10 Year	25 Year	50 Year	100 Year
Event	Pre (cfs)				
DP-1	0.00	0.73	3.85	10.76	23.07
DP-2	0.00	0.00	0.03	0.10	0.49
DP-3	0.00	0.00	0.04	0.12	0.60
DP-4	0.00	0.01	0.07	0.23	0.98
DP-5	0.00	0.00	0.04	0.12	0.62
DP-6	0.00	0.01	0.13	0.43	1.84
DP-7	0.00	0.00	0.03	0.12	0.49

CALCULATION METHODS

- 1. Runoff curve numbers (CN), time-of-concentration (T_c), and runoff rates were calculated based on TR-55 methodology.
- 2. Autodesk Civil 3D 2019 computer program was utilized for digitizing ground cover areas.
- 3. Runoff rates computed using HydroCAD version 10.10.

ASSUMPTIONS

- 1. The ground cover types and boundaries were determined using the Topographic Plan, MassGIS aerial imagery, aerial imagery viewed on Google Earth, and hydrologic soil groups based on United States Department of Agriculture, NRCS Soil Survey map information.
- 2. The subcatchment limits were truncated at the property line, except for the northeastern portion of EDA-1/PDA-1.
 - This subcatchment expanded beyond the property line in order to include runoff that the Property receives from the abutting property owned by Wareham Little League Inc.

REV	CALC. BY	DATE	CHECKED BY	DATE	APPROVED BY	DATE
0	RFK	11/08/2021	KJP	11/12/2021	MC	11/17/2021

RFK/kjp/mc/1833109CS004A

Civil Engineering • Land Surveying • Landscape Architecture • Land Use Permitting • Environmental Planning • Wetland Science



SOURCES OF DATA/ EQUATIONS

- 1. NRCS Soil Map for Plymouth County, downloaded from Web Soil Survey on 4/15/2020.
- 2. Topographic Plan, prepared by Northeast Survey Consultants and B+T, dated 11/19/2021.
- 3. Pre-Development Conditions Hydrologic Areas Map, prepared by B+T, dated 11/08/2021.
- 4. Proposed Site Plan Design File, B+T File No. 1833109D076B.
- 5. Pre-Development Hydrologic Calculations, B+T File No. 1833109CS001, dated 05/22/2020.
- 6. TR-55 Urban Hydrology for Small Watersheds, SCS, 1986.
- 7. Massachusetts DEP Stormwater Management Handbook, February 2008.
- 8. Town of Wareham Rules & Regulations Governing the Subdivision of Land, March 2013.

LIST OF ATTACHMENTS

1. Pre-Development Conditions: Hydrologic Areas Map and HydroCAD Report

REV	CALC. BY	DATE	CHECKED BY	DATE	APPROVED BY	DATE
0	RFK	11/08/2021	KJP	11/12/2021	MC	11/17/2021

RFK/kjp/mc/1833109CS004A

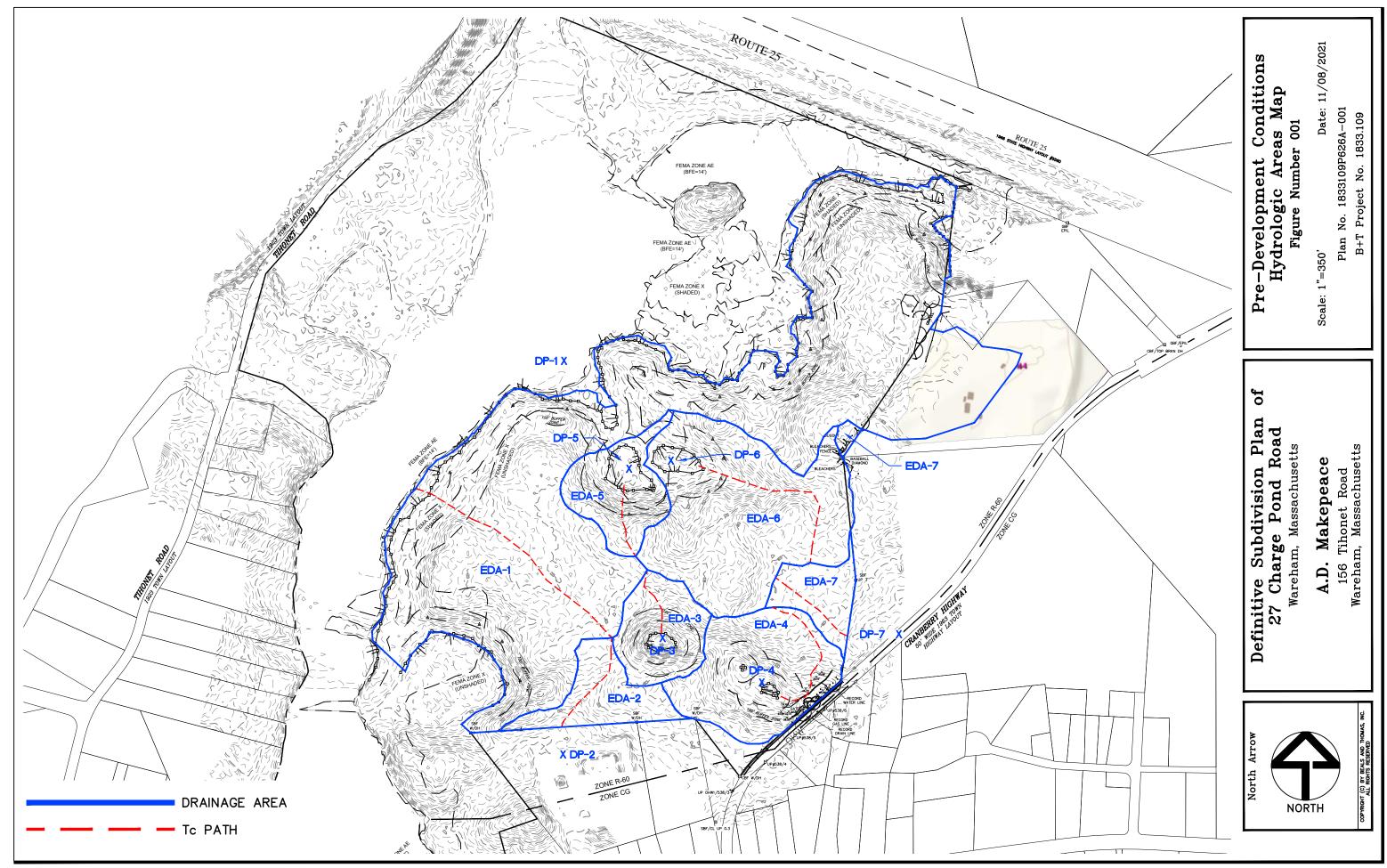
Civil Engineering • Land Surveying • Landscape Architecture • Land Use Permitting • Environmental Planning • Wetland Science

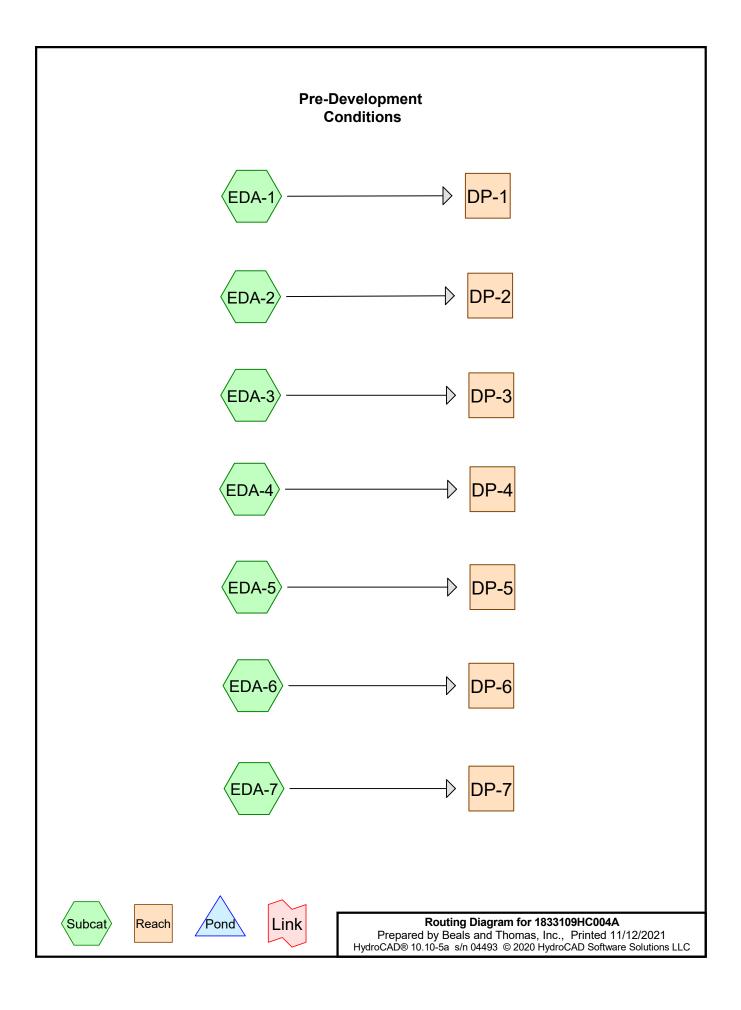
Attachment 1

Pre-Development Conditions: Hydrologic Areas Map and HydroCAD Report









Area Listing (all nodes)

Area	CN	Description
 (acres)		(subcatchment-numbers)
1.998	39	>75% Grass cover, Good, HSG A (EDA-1, EDA-4, EDA-6, EDA-7)
3.732	61	>75% Grass cover, Good, HSG B (EDA-1, EDA-7)
0.413	96	Gravel surface, HSG B (EDA-1)
0.004	98	Roofs, HSG A (EDA-7)
0.049	98	Roofs, HSG B (EDA-1)
60.945	30	Woods, Good, HSG A (EDA-1, EDA-2, EDA-3, EDA-4, EDA-5, EDA-6, EDA-7)
2.936	55	Woods, Good, HSG B (EDA-1)
0.998	77	Woods, Good, HSG D (EDA-1)
71.075	34	TOTAL AREA

1833109HC004A	Type III 24-hr Plymouth-002yr Rainfall=3.36"
Prepared by Beals and Thomas, Inc.	Printed 11/12/2021
HydroCAD® 10.10-5a s/n 04493 © 2020 HydroCAD Softwar	e Solutions LLC Page 3

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment EDA-1:	Runoff Area=42.430 ac 0.12% Impervious Runoff Depth=0.00" Flow Length=1,024' Tc=33.1 min CN=37 Runoff=0.00 cfs 0.000 af
Subcatchment EDA-2:	Runoff Area=2.708 ac 0.00% Impervious Runoff Depth=0.00" Flow Length=442' Tc=18.0 min CN=30 Runoff=0.00 cfs 0.000 af
Subcatchment EDA-3:	Runoff Area=3.078 ac 0.00% Impervious Runoff Depth=0.00" Flow Length=290' Tc=13.3 min CN=30 Runoff=0.00 cfs 0.000 af
Subcatchment EDA-4:	Runoff Area=6.130 ac 0.00% Impervious Runoff Depth=0.00" Flow Length=655' Tc=25.8 min CN=30 Runoff=0.00 cfs 0.000 af
Subcatchment EDA-5:	Runoff Area=3.277 ac 0.00% Impervious Runoff Depth=0.00" Flow Length=303' Tc=14.9 min CN=30 Runoff=0.00 cfs 0.000 af
Subcatchment EDA-6:	Runoff Area=11.348 ac 0.00% Impervious Runoff Depth=0.00" Flow Length=782' Tc=25.1 min CN=30 Runoff=0.00 cfs 0.000 af
Subcatchment EDA-7:	Runoff Area=2.104 ac 0.19% Impervious Runoff Depth=0.00" Flow Length=382' Tc=18.8 min CN=31 Runoff=0.00 cfs 0.000 af
Reach DP-1:	Inflow=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af
Reach DP-2:	Inflow=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af
Reach DP-3:	Inflow=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af
Reach DP-4:	Inflow=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af
Reach DP-5:	Inflow=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af
Reach DP-6:	Inflow=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af
Reach DP-7:	Inflow=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af

Total Runoff Area = 71.075 acRunoff Volume = 0.000 afAverage Runoff Depth = 0.00"99.93% Pervious = 71.022 ac0.07% Impervious = 0.053 ac

Summary for Subcatchment EDA-1:

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-002yr Rainfall=3.36"

Area	(ac)	CN	Desc	cription						
32.	525	30	Woods, Good, HSG A							
2.	936	55	Woo	/oods, Good, HSG B						
0.	998	77	Woo	ds, Good,	HSG D					
1.	793	39	>75%	6 Grass co	over, Good	, HSG A				
3.	716	61	>75%	6 Grass co	over, Good	, HSG B				
0.	413	96	Grav	el surface	, HSG B					
0.	049	98	Roof	s, HSG B						
42.	430	37	Weig	phted Aver	age					
42.	381		99.8	8% Pervio	us Area					
0.	049		0.12	% Impervi	ous Area					
Tc	Length	n S	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·				
11.2	50) 0.0	0300	0.07		Sheet Flow, Tc-1				
						Woods: Light underbrush n= 0.400 P2= 2.80"				
17.7	694	4 0.0	0170	0.65		Shallow Concentrated Flow, Tc-2				
						Woodland Kv= 5.0 fps				
4.2	280	0.0	0500	1.12		Shallow Concentrated Flow, Tc-3				
						Woodland Kv= 5.0 fps				
33.1	1,024	4 To	otal							

Summary for Subcatchment EDA-2:

Runoff	_	0.00 of a	0.00 hrs. Valume-	0.000 of Dooth- 0.00"
RUHUH	_	0.00 CIS (0)	0.00 hrs, Volume=	0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-002yr Rainfall=3.36"

_	Area	(ac) C	N Des	cription					
	2.708 30 Woods, Good, HSG A								
2.708 100.00% Pervious Area									
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
-	11.2	50	0.0300	0.07		Sheet Flow, Tc-1			
	6.8	392	0.0370	0.96		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps			
	18.0	442	Total						

Summary for Subcatchment EDA-3:

Page 5

Runoff 0.00 hrs, Volume= = 0.00 cfs @ 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-002yr Rainfall=3.36"

_	Area	(ac) C	N Dese	cription					
	3.078 30 Woods, Good, HSG A								
	3.	078	100.	00% Pervi	ous Area				
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
	10.0	50	0.0400	0.08		Sheet Flow, Tc-1			
	1.7	81	0.0250	0.79		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps			
	0.8	63	0.0630	1.25		Shallow Concentrated Flow, Tc-3			
	0.8	96	0.1560	1.97		Woodland Kv= 5.0 fps Shallow Concentrated Flow, Tc-4 Woodland Kv= 5.0 fps			
	13.3	290	Total						

Summary for Subcatchment EDA-4:

Runoff	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af, Depth= 0.00"
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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-002yr Rainfall=3.36"

Area	(ac) C	N Dese	cription					
6.	6.071 30 Woods, Good, HSG A							
0.	0.059 39 >75% Grass cover, Good, HSG A							
6.	6.130 30 Weighted Average							
6.130 100.00% Pervious Area								
Τ.	1 11.		\/.l!t	0	Description			
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
15.2	50	0.0140	0.05		Sheet Flow, Tc-1			
					Woods: Light underbrush n= 0.400 P2= 2.80"			
4.8	253	0.0310	0.88		Shallow Concentrated Flow, Tc-2			
					Woodland Kv= 5.0 fps			
2.2	123	0.0360	0.95		Shallow Concentrated Flow, Tc-3			
					Woodland Kv= 5.0 fps			
3.6	229	0.0460	1.07		Shallow Concentrated Flow, Tc-4			
					Woodland Kv= 5.0 fps			
25.8	655	Total						

Summary for Subcatchment EDA-5:

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-002yr Rainfall=3.36"

_	Area	(ac) C	N Des	cription					
	3.277 30 Woods, Good, HSG A								
	3.	277	100.	00% Pervi	ous Area				
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
	11.2	50	0.0300	0.07		Sheet Flow, Tc-1			
	2.0	70	0.0140	0.59		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps			
_	1.7	183	0.1260	1.77		Shallow Concentrated Flow, Tc-3 Woodland Kv= 5.0 fps			
	1/ 0	303	Total						

14.9 303 Total

Summary for Subcatchment EDA-6:

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-002yr Rainfall=3.36"

Area	(ac) C	N Dese	cription					
11.	.289 3	80 Woo	ds, Good,	HSG A				
0.	0.059 39 >75% Grass cover, Good, HSG A							
11.	11.348 30 Weighted Average							
11.348 100.00% Pervious Area								
-		01		0				
Tc	Length	Slope	Velocity	Capacity	Description			
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)				
11.2	50	0.0300	0.07		Sheet Flow, Tc-1			
					Woods: Light underbrush n= 0.400 P2= 2.80"			
7.1	339	0.0250	0.79		Shallow Concentrated Flow, Tc-2			
					Woodland Kv= 5.0 fps			
3.2	217	0.0510	1.13		Shallow Concentrated Flow, Tc-3			
					Woodland Kv= 5.0 fps			
3.6	176	0.0260	0.81		Shallow Concentrated Flow, Tc-4			
					Woodland Kv= 5.0 fps			
25.1	782	Total						

Summary for Subcatchment EDA-7:

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-002yr Rainfall=3.36"

_	Area	(ac) C	N Des	cription				
1.997 30 Woods, Good, HSG A								
	0.087 39 >75% Grass cover, Good, HSG A							
0.016 61 >75% Grass cover, Good, HSG B						, HSG B		
_	0.	004	98 Roo	fs, HSG A				
	2.104 31 Weighted Average							
	2.100 99.81% Pervious Area							
	0.	004	0.19	% Impervi	ous Area			
_	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
	11.2	50	0.0300	0.07		Sheet Flow, Tc-1		
	11.2 7.6	50 332	0.0300	0.07		Sheet Flow, Tc-1 Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps		

Summary for Reach DP-1:

Inflow Are	a =	42.430 ac,	0.12% Impervious, Inflow D	epth = 0.00" for Plymouth-002yr event
Inflow	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af
Outflow	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-2:

Inflow Area =	2.708 ac,	0.00% Impervious, Inflow D	Depth = 0.00" for Plymouth-002yr event
Inflow =	0.00 cfs @	0.00 hrs, Volume=	0.000 af
Outflow =	0.00 cfs @	0.00 hrs, Volume=	0.000 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-3:

Inflow Area =	3.078 ac,	0.00% Impervious, Inflow Dep	oth = 0.00" for Plymouth-002yr event
Inflow =	0.00 cfs @	0.00 hrs, Volume= 0).000 af
Outflow =	0.00 cfs @	0.00 hrs, Volume= 0).000 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-4:

Inflow Are	a =	6.130 ac,	0.00% Impervious, Inflow D	epth = 0.00" for F	lymouth-002yr event
Inflow	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af	
Outflow	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af, Atten= 0%	6, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-5:

Inflow Area	=	3.277 ac,	0.00% Impervious, Inflow E	Depth = 0.00"	for Plymouth-002yr event
Inflow =	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af	
Outflow =	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-6:

Inflow Area =	11.348 ac,	0.00% Impervious, Inflow	/ Depth = 0.00"	for Plymouth-002yr event
Inflow =	0.00 cfs @	0.00 hrs, Volume=	0.000 af	
Outflow =	0.00 cfs @	0.00 hrs, Volume=	0.000 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-7:

Inflow Are	a =	2.104 ac,	0.19% Impervious, Inflow D	epth = 0.00" for Plymouth-002yr ev	ent
Inflow	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af	
Outflow	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af, Atten= 0%, Lag= 0.0 min	

1833109HC004A	Type III 24-hr Plymouth-010yr Rainfall=4.95"
Prepared by Beals and Thomas, Inc.	Printed 11/12/2021
HydroCAD® 10.10-5a s/n 04493 © 2020 HydroCAD Softwar	re Solutions LLC Page 9

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment EDA-1:	Runoff Area=42.430 ac 0.12% Impervious Runoff Depth>0.13" Flow Length=1,024' Tc=33.1 min CN=37 Runoff=0.73 cfs 0.442 af
Subcatchment EDA-2:	Runoff Area=2.708 ac 0.00% Impervious Runoff Depth>0.00" Flow Length=442' Tc=18.0 min CN=30 Runoff=0.00 cfs 0.001 af
Subcatchment EDA-3:	Runoff Area=3.078 ac 0.00% Impervious Runoff Depth>0.00" Flow Length=290' Tc=13.3 min CN=30 Runoff=0.00 cfs 0.001 af
Subcatchment EDA-4:	Runoff Area=6.130 ac 0.00% Impervious Runoff Depth>0.00" Flow Length=655' Tc=25.8 min CN=30 Runoff=0.01 cfs 0.002 af
Subcatchment EDA-5:	Runoff Area=3.277 ac 0.00% Impervious Runoff Depth>0.00" Flow Length=303' Tc=14.9 min CN=30 Runoff=0.00 cfs 0.001 af
Subcatchment EDA-6:	Runoff Area=11.348 ac 0.00% Impervious Runoff Depth>0.00" Flow Length=782' Tc=25.1 min CN=30 Runoff=0.01 cfs 0.003 af
Subcatchment EDA-7:	Runoff Area=2.104 ac 0.19% Impervious Runoff Depth>0.01" Flow Length=382' Tc=18.8 min CN=31 Runoff=0.00 cfs 0.002 af
Reach DP-1:	Inflow=0.73 cfs 0.442 af Outflow=0.73 cfs 0.442 af
Reach DP-2:	Inflow=0.00 cfs 0.001 af Outflow=0.00 cfs 0.001 af
Reach DP-3:	Inflow=0.00 cfs 0.001 af Outflow=0.00 cfs 0.001 af
Reach DP-4:	Inflow=0.01 cfs 0.002 af Outflow=0.01 cfs 0.002 af
Reach DP-5:	Inflow=0.00 cfs 0.001 af Outflow=0.00 cfs 0.001 af
Reach DP-6:	Inflow=0.01 cfs 0.003 af Outflow=0.01 cfs 0.003 af
Reach DP-7:	Inflow=0.00 cfs 0.002 af Outflow=0.00 cfs 0.002 af

Total Runoff Area = 71.075 acRunoff Volume = 0.451 afAverage Runoff Depth = 0.08"99.93% Pervious = 71.022 ac0.07% Impervious = 0.053 ac

Summary for Subcatchment EDA-1:

Runoff = 0.73 cfs @ 15.05 hrs, Volume= 0.442 af, Depth> 0.13"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-010yr Rainfall=4.95"

Area	(ac)	CN	Desc	ription							
32.	525	30	Woo	ds, Good,	HSG A						
2.	936	55	Woo	ods, Good, HSG B							
0.	998			oods, Good, HSG D							
1.	793	39	>75%	6 Grass co	over, Good	, HSG A					
3.	716	61	>75%	6 Grass co	over, Good	, HSG B					
0.	413	96	Grav	el surface	, HSG B						
0.	049	98	Roof	s, HSG B							
42.	430	37	Weig	phted Aver	age						
42.	381		99.8	8% Pervio	us Area						
0.	049		0.12	% Impervi	ous Area						
Тс	Length		lope	Velocity	Capacity	Description					
(min)	(feet)) (1	ft/ft)	(ft/sec)	(cfs)						
11.2	50	0.0	300	0.07		Sheet Flow, Tc-1					
						Woods: Light underbrush n= 0.400 P2= 2.80"					
17.7	694	0.0	170	0.65		Shallow Concentrated Flow, Tc-2					
						Woodland Kv= 5.0 fps					
4.2	280	0.0	500	1.12		Shallow Concentrated Flow, Tc-3					
						Woodland Kv= 5.0 fps					
33.1	1,024	l Tot	tal								

Summary for Subcatchment EDA-2:

Runoff	=	0.00 cfs @	24.00 hrs,	Volume=	0.001 af, Depth> 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-010yr Rainfall=4.95"

_	Area	(ac) C	N Des	cription					
_	2.708 30 Woods, Good, HSG A								
	2.	708	100.	00% Pervi	ous Area				
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
-	11.2	50	0.0300	0.07		Sheet Flow, Tc-1			
	6.8	392	0.0370	0.96		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps			
-	18.0	442	Total						

Summary for Subcatchment EDA-3:

Runoff = 0.00 cfs @ 24.00 hrs, Volume= 0.001 af, Depth> 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-010yr Rainfall=4.95"

_	Area	(ac) C	N Desc	cription				
	3.	078 3	80 Woo	ds, Good,	HSG A			
3.078 100.00% Pervious Area								
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
_	10.0	50	0.0400	0.08		Sheet Flow, Tc-1		
	1.7	81	0.0250	0.79		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2		
	1.7	01	0.0200	0.70		Woodland Kv= 5.0 fps		
	0.8	63	0.0630	1.25		Shallow Concentrated Flow, Tc-3		
		~~~		4.07		Woodland Kv= 5.0 fps		
	0.8	96	0.1560	1.97		Shallow Concentrated Flow, Tc-4 Woodland Kv= 5.0 fps		
_	13.3	290	Total					

### Summary for Subcatchment EDA-4:

Runoff	=	0.01 cfs @	24.00 hrs, Volume=	0.002 af, Depth> 0.00"
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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-010yr Rainfall=4.95"

Area	(ac) C	N Desc	cription		
6.	071 3	80 Woo	ds, Good,	HSG A	
0.	059 3	<mark>89 &gt;75</mark> 9	% Grass co	over, Good,	, HSG A
6.	130 3		ghted Aver		
6.	130	100.	00% Pervi	ous Area	
Та	l a a a th	Clana	Volosity	Conseitu	Description
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
15.2	50	0.0140	0.05		Sheet Flow, Tc-1
					Woods: Light underbrush n= 0.400 P2= 2.80"
4.8	253	0.0310	0.88		Shallow Concentrated Flow, Tc-2
					Woodland Kv= 5.0 fps
2.2	123	0.0360	0.95		Shallow Concentrated Flow, Tc-3
					Woodland Kv= 5.0 fps
3.6	229	0.0460	1.07		Shallow Concentrated Flow, Tc-4
					Woodland Kv= 5.0 fps
25.8	655	Total			

#### Summary for Subcatchment EDA-5:

Runoff = 0.00 cfs @ 24.00 hrs, Volume= 0.001 af, Depth> 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-010yr Rainfall=4.95"

_	Area	(ac) C	N Des	cription		
	3.	277 3	30 Woo	ods, Good,	HSG A	
-	3.	277	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	11.2	50	0.0300	0.07		Sheet Flow, Tc-1
	2.0	70	0.0140	0.59		Woods: Light underbrush n= 0.400 P2= 2.80" <b>Shallow Concentrated Flow, Tc-2</b> Woodland Kv= 5.0 fps
	1.7	183	0.1260	1.77		Shallow Concentrated Flow, Tc-3 Woodland Kv= 5.0 fps
	110	202	Total			

14.9 303 Total

# Summary for Subcatchment EDA-6:

Runoff = 0.01 cfs @ 24.00 hrs, Volume= 0.003 af, Depth> 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-010yr Rainfall=4.95"

Area	(ac) C	N Dese	cription		
11.	.289 3	80 Woo	ds, Good,	HSG A	
0.	.059 3	<mark>89 &gt;75</mark> 9	% Grass co	over, Good	, HSG A
11.	.348 3	80 Weig	ghted Aver	age	
11.	.348	100.	00% Pervi	ous Area	
-		01		0	
Tc	Length	Slope	Velocity	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
11.2	50	0.0300	0.07		Sheet Flow, Tc-1
					Woods: Light underbrush n= 0.400 P2= 2.80"
7.1	339	0.0250	0.79		Shallow Concentrated Flow, Tc-2
					Woodland Kv= 5.0 fps
3.2	217	0.0510	1.13		Shallow Concentrated Flow, Tc-3
					Woodland Kv= 5.0 fps
3.6	176	0.0260	0.81		Shallow Concentrated Flow, Tc-4
					Woodland Kv= 5.0 fps
25.1	782	Total			

#### Summary for Subcatchment EDA-7:

Runoff = 0.00 cfs @ 22.87 hrs, Volume= 0.002 af, Depth> 0.01"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-010yr Rainfall=4.95"

 Area (	(ac) (	CN	Desc	ription		
1.997 30 Woods, Good, HSG A						
0.0	087	39	>75%	6 Grass co	over, Good	, HSG A
0.0	016	61	>75%	6 Grass co	over, Good	, HSG B
 0.0	004	98	Roof	s, HSG A		
2.	104	31	Weig	ghted Aver	age	
2.	100		99.8	1% Pervio	us Area	
0.0	004		0.19	% Impervi	ous Area	
 Tc (min)	Length (feet)		ope ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
 11.2	50	0.0	300	0.07		Sheet Flow, Tc-1
7.6	332	2 0.02	210	0.72		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps
18.8	382	. Tot	al			

#### Summary for Reach DP-1:

Inflow Area	a =	42.430 ac,	0.12% Impervious, Inflow D	Depth > 0.13" for Plymouth-010yr event
Inflow	=	0.73 cfs @	15.05 hrs, Volume=	0.442 af
Outflow	=	0.73 cfs @	15.05 hrs, Volume=	0.442 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

### Summary for Reach DP-2:

Inflow Are	a =	2.708 ac,	0.00% Impervious, Inflow De	epth > 0.00" for Plymouth-010yr event
Inflow	=	0.00 cfs @	24.00 hrs, Volume=	0.001 af
Outflow	=	0.00 cfs @	24.00 hrs, Volume=	0.001 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

### Summary for Reach DP-3:

Inflow Area	a =	3.078 ac,	0.00% Impervious, Inflow Depth > 0.00" for Plymouth-010yr even	ıt
Inflow	=	0.00 cfs @	24.00 hrs, Volume= 0.001 af	
Outflow	=	0.00 cfs @	24.00 hrs, Volume= 0.001 af, Atten= 0%, Lag= 0.0 min	

## Summary for Reach DP-4:

Inflow Are	a =	6.130 ac,	0.00% Impervious, Inflow Dep	pth > 0.00" for Plymouth-010yr event
Inflow	=	0.01 cfs @	24.00 hrs, Volume=	0.002 af
Outflow	=	0.01 cfs @	24.00 hrs, Volume= (	0.002 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

## Summary for Reach DP-5:

Inflow Area	a =	3.277 ac,	0.00% Impervious, Inflow D	epth > 0.00"	for Plymouth-010yr event
Inflow	=	0.00 cfs @	24.00 hrs, Volume=	0.001 af	
Outflow	=	0.00 cfs @	24.00 hrs, Volume=	0.001 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

### Summary for Reach DP-6:

Inflow Area =	11.348 ac,	0.00% Impervious, Inflow D	Depth > 0.00" for Plymouth-010yr event
Inflow =	0.01 cfs @	24.00 hrs, Volume=	0.003 af
Outflow =	0.01 cfs @	24.00 hrs, Volume=	0.003 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

#### Summary for Reach DP-7:

Inflow Are	a =	2.104 ac,	0.19% Impervious,	Inflow Depth > 0.01	for Plymouth-010yr event
Inflow	=	0.00 cfs @	22.87 hrs, Volume	= 0.002 af	
Outflow	=	0.00 cfs @	22.87 hrs, Volume	= 0.002 af, A	tten= 0%, Lag= 0.0 min

1833109HC004A	Type III 24-hr Plymouth-025yr Rainfall=6.18"
Prepared by Beals and Thomas, Inc.	Printed 11/12/2021
HydroCAD® 10.10-5a s/n 04493 © 2020 HydroCAD Softwar	re Solutions LLC Page 15

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment EDA-1:	Runoff Area=42.430 ac 0.12% Impervious Runoff Depth>0.38" Flow Length=1,024' Tc=33.1 min CN=37 Runoff=3.85 cfs 1.350 af
Subcatchment EDA-2:	Runoff Area=2.708 ac 0.00% Impervious Runoff Depth>0.09" Flow Length=442' Tc=18.0 min CN=30 Runoff=0.03 cfs 0.020 af
Subcatchment EDA-3:	Runoff Area=3.078 ac 0.00% Impervious Runoff Depth>0.09" Flow Length=290' Tc=13.3 min CN=30 Runoff=0.04 cfs 0.023 af
Subcatchment EDA-4:	Runoff Area=6.130 ac 0.00% Impervious Runoff Depth>0.09" Flow Length=655' Tc=25.8 min CN=30 Runoff=0.07 cfs 0.046 af
Subcatchment EDA-5:	Runoff Area=3.277 ac 0.00% Impervious Runoff Depth>0.09" Flow Length=303' Tc=14.9 min CN=30 Runoff=0.04 cfs 0.025 af
Subcatchment EDA-6:	Runoff Area=11.348 ac 0.00% Impervious Runoff Depth>0.09" Flow Length=782' Tc=25.1 min CN=30 Runoff=0.13 cfs 0.085 af
Subcatchment EDA-7:	Runoff Area=2.104 ac 0.19% Impervious Runoff Depth>0.12" Flow Length=382' Tc=18.8 min CN=31 Runoff=0.03 cfs 0.021 af
Reach DP-1:	Inflow=3.85 cfs 1.350 af Outflow=3.85 cfs 1.350 af
Reach DP-2:	Inflow=0.03 cfs 0.020 af Outflow=0.03 cfs 0.020 af
Reach DP-3:	Inflow=0.04 cfs 0.023 af Outflow=0.04 cfs 0.023 af
Reach DP-4:	Inflow=0.07 cfs 0.046 af Outflow=0.07 cfs 0.046 af
Reach DP-5:	Inflow=0.04 cfs 0.025 af Outflow=0.04 cfs 0.025 af
Reach DP-6:	Inflow=0.13 cfs 0.085 af Outflow=0.13 cfs 0.085 af
Reach DP-7:	Inflow=0.03 cfs 0.021 af Outflow=0.03 cfs 0.021 af

Total Runoff Area = 71.075 acRunoff Volume = 1.571 afAverage Runoff Depth = 0.27"99.93% Pervious = 71.022 ac0.07% Impervious = 0.053 ac

### Summary for Subcatchment EDA-1:

Runoff = 3.85 cfs @ 12.80 hrs, Volume= 1.350 af, Depth> 0.38"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-025yr Rainfall=6.18"

Area	(ac) C	N Des	cription		
32.	525	30 Woo	ods, Good,	HSG A	
2.	936	55 Woo	ods, Good,	HSG B	
0.	998	77 Woo	ods, Good,	HSG D	
1.	793	39 >75°	% Grass c	over, Good	, HSG A
3.	716	61 >75°	% Grass c	over, Good	, HSG B
0.	413	96 Grav	/el surface	, HSG B	
0.	049	98 Roo	fs, HSG B		
42.	430	37 Wei	ghted Avei	age	
42.	381	99.8	8% Pervio	us Area	
0.	049	0.12	% Impervi	ous Area	
Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
11.2	50	0.0300	0.07		Sheet Flow, Tc-1
					Woods: Light underbrush n= 0.400 P2= 2.80"
17.7	694	0.0170	0.65		Shallow Concentrated Flow, Tc-2
					Woodland Kv= 5.0 fps
4.2	280	0.0500	1.12		Shallow Concentrated Flow, Tc-3
					Woodland Kv= 5.0 fps
33.1	1,024	Total			

## Summary for Subcatchment EDA-2:

Runoff	=	0.03 cfs @	15.44 hrs,	Volume=	0.020 af, Depth> 0.09"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-025yr Rainfall=6.18"

_	Area	(ac) C	N Des	cription		
_	2.	708 3	30 Woo	ds, Good,	HSG A	
2.708 100.00% Pervious Area						
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	11.2	50	0.0300	0.07		Sheet Flow, Tc-1
	6.8	392	0.0370	0.96		Woods: Light underbrush n= 0.400 P2= 2.80" <b>Shallow Concentrated Flow, Tc-2</b> Woodland Kv= 5.0 fps
-	18.0	442	Total			

#### Summary for Subcatchment EDA-3:

Runoff = 0.04 cfs @ 15.39 hrs, Volume= 0.023 af, Depth> 0.09"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-025yr Rainfall=6.18"

_	Area	(ac) C	N Desc	cription		
	3.	078 3	80 Woo	ds, Good,	HSG A	
	3.	078	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	10.0	50	0.0400	0.08		Sheet Flow, Tc-1
	1.7	81	0.0250	0.79		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2
	1.7	01	0.0200	0.70		Woodland Kv= 5.0 fps
	0.8	63	0.0630	1.25		Shallow Concentrated Flow, Tc-3
		~~~		4.07		Woodland Kv= 5.0 fps
	0.8	96	0.1560	1.97		Shallow Concentrated Flow, Tc-4 Woodland Kv= 5.0 fps
_	13.3	290	Total			

Summary for Subcatchment EDA-4:

Runoff	=	0.07 cfs @	15.57 hrs, Volume	e= 0.046 af, Depth> 0.09"
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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-025yr Rainfall=6.18"

Area	(ac) C	N Dese	cription		
6.	.071 3	80 Woo	ds, Good,	HSG A	
0.	<u>.059 3</u>	<u>89 >759</u>	% Grass co	over, Good	, HSG A
6.	.130 3		ghted Aver		
6.	.130	100.	00% Pervi	ous Area	
-		01		0	
Tc	Length	Slope	Velocity	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
15.2	50	0.0140	0.05		Sheet Flow, Tc-1
					Woods: Light underbrush n= 0.400 P2= 2.80"
4.8	253	0.0310	0.88		Shallow Concentrated Flow, Tc-2
					Woodland Kv= 5.0 fps
2.2	123	0.0360	0.95		Shallow Concentrated Flow, Tc-3
					Woodland Kv= 5.0 fps
3.6	229	0.0460	1.07		Shallow Concentrated Flow, Tc-4
					Woodland Kv= 5.0 fps
25.8	655	Total			

Summary for Subcatchment EDA-5:

Runoff = 0.04 cfs @ 15.40 hrs, Volume= 0.025 af, Depth> 0.09"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-025yr Rainfall=6.18"

_	Area	(ac) C	N Des	cription		
	3.	277 3	30 Woo	ds, Good,	HSG A	
_	3.	277	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	11.2	50	0.0300	0.07		Sheet Flow, Tc-1
	2.0	70	0.0140	0.59		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps
	1.7	183	0.1260	1.77		Shallow Concentrated Flow, Tc-3 Woodland Kv= 5.0 fps
	14.0	202	Total			

14.9 303 Total

Summary for Subcatchment EDA-6:

Runoff = 0.13 cfs @ 15.57 hrs, Volume= 0.085 af, Depth> 0.09"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-025yr Rainfall=6.18"

Area	(ac) C	N Desc	cription		
11.	.289 3	80 Woo	ds, Good,	HSG A	
0.	.059 3	<mark>89 >75</mark> 9	% Grass co	over, Good	, HSG A
11.	.348 3		ghted Aver		
11.	.348	100.	00% Pervi	ous Area	
_				•	— • • •
Tc	Length	Slope	Velocity	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
11.2	50	0.0300	0.07		Sheet Flow, Tc-1
					Woods: Light underbrush n= 0.400 P2= 2.80"
7.1	339	0.0250	0.79		Shallow Concentrated Flow, Tc-2
					Woodland Kv= 5.0 fps
3.2	217	0.0510	1.13		Shallow Concentrated Flow, Tc-3
					Woodland Kv= 5.0 fps
3.6	176	0.0260	0.81		Shallow Concentrated Flow, Tc-4
					Woodland Kv= 5.0 fps
25.1	782	Total			

Summary for Subcatchment EDA-7:

Runoff = 0.03 cfs @ 15.14 hrs, Volume= 0.021 af, Depth> 0.12"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-025yr Rainfall=6.18"

	Area (ac) (CN De	escription				
	1.997 30 Woods, Good, HSG A							
	0.0)87	39 >7	'5% Grass c	over, Good	, HSG A		
	0.0	016	61 >7	'5% Grass c	over, Good	, HSG B		
	0.0	004	98 Ro	oofs, HSG A				
	2.1	104	31 W	eighted Ave	rage			
	2.1	100	99	.81% Pervic	ous Area			
	0.0	004	0.	19% Impervi	ous Area			
_(Tc min)	Length (feet)	Slop (ft/f		Capacity (cfs)	Description		
	11.2	50	0.030	0 0.07		Sheet Flow, Tc-1		
	7.6	332	0.021	0 0.72		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps		
	18.8	382	Total					

Summary for Reach DP-1:

Inflow Are	a =	42.430 ac,	0.12% Impervious,	Inflow Depth >	0.38" for l	Plymouth-025yr event
Inflow	=	3.85 cfs @	12.80 hrs, Volume	= 1.350 a	af	
Outflow	=	3.85 cfs @	12.80 hrs, Volume	e= 1.350 a	af, Atten= 0°	%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-2:

Inflow Area	a =	2.708 ac,	0.00% Impervious, Inflow De	epth > 0.09" for Plymouth-025yr event
Inflow	=	0.03 cfs @	15.44 hrs, Volume=	0.020 af
Outflow	=	0.03 cfs @	15.44 hrs, Volume=	0.020 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-3:

Inflow Area =	3.078 ac,	0.00% Impervious, Inflow Depth	> 0.09" for Plymouth-025yr event
Inflow =	0.04 cfs @	15.39 hrs, Volume= 0.02	23 af
Outflow =	0.04 cfs @	15.39 hrs, Volume= 0.02	23 af, Atten= 0%, Lag= 0.0 min

Summary for Reach DP-4:

Inflow Area	a =	6.130 ac,	0.00% Impervious, Inflow D	epth > 0.09"	for Plymouth-025yr event
Inflow	=	0.07 cfs @	15.57 hrs, Volume=	0.046 af	
Outflow	=	0.07 cfs @	15.57 hrs, Volume=	0.046 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-5:

Inflow Area =	=	3.277 ac,	0.00% Impervious, Inflow	Depth > 0.09 "	for Plymouth-025yr event
Inflow =		0.04 cfs @	15.40 hrs, Volume=	0.025 af	
Outflow =		0.04 cfs @	15.40 hrs, Volume=	0.025 af, Att	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-6:

Inflow Area	=	11.348 ac,	0.00% Impervious, Inflow Depth > 0.09" for Plymouth-025yr even	nt
Inflow	=	0.13 cfs @	15.57 hrs, Volume= 0.085 af	
Outflow	=	0.13 cfs @	15.57 hrs, Volume= 0.085 af, Atten= 0%, Lag= 0.0 min	

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-7:

Inflow Are	a =	2.104 ac,	0.19% Impervious, I	Inflow Depth > 0.12"	for Plymouth-025yr event
Inflow	=	0.03 cfs @	15.14 hrs, Volume=	0.021 af	
Outflow	=	0.03 cfs @	15.14 hrs, Volume=	e 0.021 af, At	ten= 0%, Lag= 0.0 min

1833109HC004A	Type III 24-hr Plymouth-050yr Rainfall=7.31"
Prepared by Beals and Thomas, Inc.	Printed 11/12/2021
HydroCAD® 10.10-5a s/n 04493 © 2020 HydroCAD Software	e Solutions LLC Page 21

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment EDA-1:	Runoff Area=42.430 ac 0.12% Impervious Runoff Depth>0.72" Flow Length=1,024' Tc=33.1 min CN=37 Runoff=10.76 cfs 2.538 af
Subcatchment EDA-2:	Runoff Area=2.708 ac 0.00% Impervious Runoff Depth>0.27" Flow Length=442' Tc=18.0 min CN=30 Runoff=0.10 cfs 0.060 af
Subcatchment EDA-3:	Runoff Area=3.078 ac 0.00% Impervious Runoff Depth>0.27" Flow Length=290' Tc=13.3 min CN=30 Runoff=0.12 cfs 0.068 af
Subcatchment EDA-4:	Runoff Area=6.130 ac 0.00% Impervious Runoff Depth>0.26" Flow Length=655' Tc=25.8 min CN=30 Runoff=0.23 cfs 0.135 af
Subcatchment EDA-5:	Runoff Area=3.277 ac 0.00% Impervious Runoff Depth>0.27" Flow Length=303' Tc=14.9 min CN=30 Runoff=0.12 cfs 0.073 af
Subcatchment EDA-6:	Runoff Area=11.348 ac 0.00% Impervious Runoff Depth>0.26" Flow Length=782' Tc=25.1 min CN=30 Runoff=0.43 cfs 0.250 af
Subcatchment EDA-7:	Runoff Area=2.104 ac 0.19% Impervious Runoff Depth>0.32" Flow Length=382' Tc=18.8 min CN=31 Runoff=0.12 cfs 0.056 af
Reach DP-1:	Inflow=10.76 cfs 2.538 af Outflow=10.76 cfs 2.538 af
Reach DP-2:	Inflow=0.10 cfs 0.060 af Outflow=0.10 cfs 0.060 af
Reach DP-3:	Inflow=0.12 cfs 0.068 af Outflow=0.12 cfs 0.068 af
Reach DP-4:	Inflow=0.23 cfs 0.135 af Outflow=0.23 cfs 0.135 af
Reach DP-5:	Inflow=0.12 cfs 0.073 af Outflow=0.12 cfs 0.073 af
Reach DP-6:	Inflow=0.43 cfs 0.250 af Outflow=0.43 cfs 0.250 af
Reach DP-7:	Inflow=0.12 cfs 0.056 af Outflow=0.12 cfs 0.056 af

Total Runoff Area = 71.075 acRunoff Volume = 3.181 afAverage Runoff Depth = 0.54"99.93% Pervious = 71.022 ac0.07% Impervious = 0.053 ac

Summary for Subcatchment EDA-1:

Runoff = 10.76 cfs @ 12.68 hrs, Volume= 2.538 af, Depth> 0.72"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-050yr Rainfall=7.31"

Area	(ac) (CN [Desc	ription						
32.	525	30 \	Noo	oods, Good, HSG A						
2.	936	55 \	Noo	oods, Good, HSG B						
0.	998	77 \	Noo	oods, Good, HSG D						
1.	793	39 >	>75%	6 Grass co	over, Good	, HSG A				
3.	716	61 >	>75%	6 Grass co	over, Good	, HSG B				
0.	413	96 (Grav	el surface	, HSG B					
0.	049	98 F	Roof	s, HSG B						
42.	430	37 \	Neig	hted Aver	age					
42.	381	ç	99.8	3% Pervio	us Area					
0.	049	().12º	% Impervi	ous Area					
Tc	Length	i Slo	pe	Velocity	Capacity	Description				
(min)	(feet)) (ft	t/ft)	(ft/sec)	(cfs)					
11.2	50	0.03	300	0.07		Sheet Flow, Tc-1				
						Woods: Light underbrush n= 0.400 P2= 2.80"				
17.7	694	0.01	170	0.65		Shallow Concentrated Flow, Tc-2				
						Woodland Kv= 5.0 fps				
4.2	280	0.05	500	1.12		Shallow Concentrated Flow, Tc-3				
						Woodland Kv= 5.0 fps				
33.1	1,024	- Tota	al							

Summary for Subcatchment EDA-2:

Runoff =	0.10 cfs @	13.78 hrs.	Volume=	0.060 af,	Depth>	0.27"
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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-050yr Rainfall=7.31"

Area	(ac) C	N Dese	cription						
2.	2.708 30 Woods, Good, HSG A								
2.	708	100.	00% Pervi	ous Area					
Tc (min)	5 1 5 1 5				Description				
11.2	50	0.0300	0.07		Sheet Flow, Tc-1				
6.8	392	0.0370	0.96		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps				
18.0	442	Total							

Summary for Subcatchment EDA-3:

Runoff = 0.12 cfs @ 13.71 hrs, Volume= 0.068 af, Depth> 0.27"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-050yr Rainfall=7.31"

			cription	N Desc	(ac) C	Area		
3.078 30 Woods, Good, HSG A								
		ous Area	00% Pervi	100.	.078	3.		
	1	Capacity (cfs)	Velocity (ft/sec)	Slope (ft/ft)	Length (feet)	Tc (min)		
	Sheet Flow, Tc-1		0.08	0.0400	50	10.0		
30"	Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2		0.79	0.0250	81	1.7		
	Woodland Kv= 5.0 fps		1 05	0.0620	62	0.0		
	Woodland Kv= 5.0 fps		1.25	0.0630	03	0.0		
	Shallow Concentrated Flow, Tc-4		1.97	0.1560	96	0.8		
	woodiand KV= 5.0 lps			Total	200	13.3		
-	Sheet Flow, Tc-1 Woods: Light underbrush n= 0.400 P2= 2.8 Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps Shallow Concentrated Flow, Tc-3 Woodland Kv= 5.0 fps		(ft/sec) 0.08 0.79 1.25	(ft/ft) 0.0400 0.0250 0.0630	(feet) 50 81 63	(min) 10.0 1.7 0.8		

Summary for Subcatchment EDA-4:

Runoff	=	0.23 cfs @	13.87 hrs, Volume=	0.135 af, Depth> 0.26"
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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-050yr Rainfall=7.31"

Area	(ac) C	N Dese	cription						
6.	6.071 30 Woods, Good, HSG A								
0.	0.059 39 >75% Grass cover, Good, HSG A								
6.	6.130 30 Weighted Average								
6.	6.130 100.00% Pervious Area								
_									
Tc	Length	Slope	Velocity	Capacity	Description				
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)					
15.2	50	0.0140	0.05		Sheet Flow, Tc-1				
					Woods: Light underbrush n= 0.400 P2= 2.80"				
4.8	253	0.0310	0.88		Shallow Concentrated Flow, Tc-2				
					Woodland Kv= 5.0 fps				
2.2	123	0.0360	0.95		Shallow Concentrated Flow, Tc-3				
					Woodland Kv= 5.0 fps				
3.6	229	0.0460	1.07		Shallow Concentrated Flow, Tc-4				
					Woodland Kv= 5.0 fps				
25.8	655	Total							

Summary for Subcatchment EDA-5:

Runoff = 0.12 cfs @ 13.73 hrs, Volume= 0.073 af, Depth> 0.27"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-050yr Rainfall=7.31"

_	Area	(ac) C	N Des	cription		
	3.	277 3	30 Woo	ods, Good,	HSG A	
	3.	277	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	11.2	50	0.0300	0.07		Sheet Flow, Tc-1
	2.0	70	0.0140	0.59		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps
	1.7	183	0.1260	1.77		Shallow Concentrated Flow, Tc-3 Woodland Kv= 5.0 fps
	110	202	Total			

14.9 303 Total

Summary for Subcatchment EDA-6:

Runoff = 0.43 cfs @ 13.86 hrs, Volume= 0.250 af, Depth> 0.26"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-050yr Rainfall=7.31"

Area	(ac) C	N Desc	cription		
11.	.289 3	80 Woo	ds, Good,	HSG A	
0.	.059 3	<mark>89 >75</mark> 9	% Grass co	over, Good	, HSG A
11.	.348 3		ghted Aver		
11.	.348	100.	00% Pervi	ous Area	
_				•	— • • •
Tc	Length	Slope	Velocity	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
11.2	50	0.0300	0.07		Sheet Flow, Tc-1
					Woods: Light underbrush n= 0.400 P2= 2.80"
7.1	339	0.0250	0.79		Shallow Concentrated Flow, Tc-2
					Woodland Kv= 5.0 fps
3.2	217	0.0510	1.13		Shallow Concentrated Flow, Tc-3
					Woodland Kv= 5.0 fps
3.6	176	0.0260	0.81		Shallow Concentrated Flow, Tc-4
					Woodland Kv= 5.0 fps
25.1	782	Total			

Summary for Subcatchment EDA-7:

Runoff 0.12 cfs @ 12.67 hrs, Volume= = 0.056 af, Depth> 0.32"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-050yr Rainfall=7.31"

	Area (ac)	CN	Desc	ription		
1.997 30 Woods, Good, HSG A							
	0.0	087	39	>75%	6 Grass co	over, Good	, HSG A
	0.0	016	61	>75%	6 Grass co	over, Good	, HSG B
	0.0	004	98	Roof	s, HSG A		
	2.	104	31	Weig	hted Aver	age	
	2.	100		99.8	1% Pervio	us Area	
	0.0	004		0.19	% Impervi	ous Area	
(Tc min)	Length (feet)		lope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	11.2	50	0.0	0300	0.07		Sheet Flow, Tc-1
	7.6	332	2 0.0	0210	0.72		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps
	18.8	382	2 To	tal			

382 Total

Summary for Reach DP-1:

Inflow Are	a =	42.430 ac,	0.12% Impervious, Inflow I	Depth > $0.72''$ for	Plymouth-050yr event
Inflow	=	10.76 cfs @	12.68 hrs, Volume=	2.538 af	
Outflow	=	10.76 cfs @	12.68 hrs, Volume=	2.538 af, Atten= 0	%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-2:

Inflow Area	a =	2.708 ac,	0.00% Impervious, Inflow	v Depth > 0.27"	for Plymouth-050yr event
Inflow	=	0.10 cfs @	13.78 hrs, Volume=	0.060 af	
Outflow	=	0.10 cfs @	13.78 hrs, Volume=	0.060 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-3:

Inflow Area =	3.078 ac,	0.00% Impervious, Inflow Depth	n > 0.27" for Plymouth-050yr event
Inflow =	0.12 cfs @	13.71 hrs, Volume= 0.0	068 af
Outflow =	0.12 cfs @	13.71 hrs, Volume= 0.0	068 af, Atten= 0%, Lag= 0.0 min

Summary for Reach DP-4:

Inflow Are	a =	6.130 ac,	0.00% Impervious, Inflow De	pth > 0.26"	for Plymouth-050yr event
Inflow	=	0.23 cfs @	13.87 hrs, Volume=	0.135 af	
Outflow	=	0.23 cfs @	13.87 hrs, Volume=	0.135 af, Atte	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-5:

Inflow Area	a =	3.277 ac,	0.00% Impervious, Inflow D	epth > 0.27"	for Plymouth-050yr event
Inflow	=	0.12 cfs @	13.73 hrs, Volume=	0.073 af	
Outflow	=	0.12 cfs @	13.73 hrs, Volume=	0.073 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-6:

Inflow Area	a =	11.348 ac,	0.00% Impervious, Inflow Depth > 0.26" for Plymouth-050yr event	Ĺ
Inflow	=	0.43 cfs @	13.86 hrs, Volume= 0.250 af	
Outflow	=	0.43 cfs @	13.86 hrs, Volume= 0.250 af, Atten= 0%, Lag= 0.0 min	

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-7:

Inflow Are	a =	2.104 ac,	0.19% Impervious, Inflow D	Depth > 0.32" for Plymouth-050yr event
Inflow	=	0.12 cfs @	12.67 hrs, Volume=	0.056 af
Outflow	=	0.12 cfs @	12.67 hrs, Volume=	0.056 af, Atten= 0%, Lag= 0.0 min

1833109HC004A	Type III 24-hr Plymouth-100yr Rainfall=8.65"
Prepared by Beals and Thomas, Inc.	Printed 11/12/2021
HydroCAD® 10.10-5a s/n 04493 © 2020 HydroCAD Software	e Solutions LLC Page 27

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment EDA-1:	Runoff Area=42.430 ac 0.12% Impervious Runoff Depth>1.22" Flow Length=1,024' Tc=33.1 min CN=37 Runoff=23.07 cfs 4.312 af
Subcatchment EDA-2:	Runoff Area=2.708 ac 0.00% Impervious Runoff Depth>0.58" Flow Length=442' Tc=18.0 min CN=30 Runoff=0.49 cfs 0.130 af
Subcatchment EDA-3:	Runoff Area=3.078 ac 0.00% Impervious Runoff Depth>0.58" Flow Length=290' Tc=13.3 min CN=30 Runoff=0.60 cfs 0.148 af
Subcatchment EDA-4:	Runoff Area=6.130 ac 0.00% Impervious Runoff Depth>0.57" Flow Length=655' Tc=25.8 min CN=30 Runoff=0.98 cfs 0.293 af
Subcatchment EDA-5:	Runoff Area=3.277 ac 0.00% Impervious Runoff Depth>0.58" Flow Length=303' Tc=14.9 min CN=30 Runoff=0.62 cfs 0.157 af
Subcatchment EDA-6:	Runoff Area=11.348 ac 0.00% Impervious Runoff Depth>0.57" Flow Length=782' Tc=25.1 min CN=30 Runoff=1.84 cfs 0.542 af
Subcatchment EDA-7:	Runoff Area=2.104 ac 0.19% Impervious Runoff Depth>0.66" Flow Length=382' Tc=18.8 min CN=31 Runoff=0.49 cfs 0.116 af
Reach DP-1:	Inflow=23.07 cfs 4.312 af Outflow=23.07 cfs 4.312 af
Reach DP-2:	Inflow=0.49 cfs 0.130 af Outflow=0.49 cfs 0.130 af
Reach DP-3:	Inflow=0.60 cfs 0.148 af Outflow=0.60 cfs 0.148 af
Reach DP-4:	Inflow=0.98 cfs 0.293 af Outflow=0.98 cfs 0.293 af
Reach DP-5:	Inflow=0.62 cfs 0.157 af Outflow=0.62 cfs 0.157 af
Reach DP-6:	Inflow=1.84 cfs 0.542 af Outflow=1.84 cfs 0.542 af
Reach DP-7:	Inflow=0.49 cfs 0.116 af Outflow=0.49 cfs 0.116 af

Total Runoff Area = 71.075 acRunoff Volume = 5.699 afAverage Runoff Depth = 0.96"99.93% Pervious = 71.022 ac0.07% Impervious = 0.053 ac

Summary for Subcatchment EDA-1:

Runoff = 23.07 cfs @ 12.60 hrs, Volume= 4.312 af, Depth> 1.22"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-100yr Rainfall=8.65"

Area	(ac) (CN De	scription		
32.	.525	30 Wo	ods, Good,	HSG A	
2.	.936	55 Wc	ods, Good,	HSG B	
0.	.998	77 Wc	ods, Good,	HSG D	
1.	.793	39 >75	5% Grass c	over, Good	, HSG A
3.	.716	61 >75	5% Grass c	over, Good	, HSG B
0.	.413	96 Gra	vel surface	, HSG B	
0.	.049	98 Ro	ofs, HSG B		
42.	.430	37 We	ighted Ave	rage	
42.	.381	99.	88% Pervic	us Area	
0.	.049	0.1	2% Impervi	ous Area	
Tc	Length			Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
11.2	50	0.0300	0.07		Sheet Flow, Tc-1
					Woods: Light underbrush n= 0.400 P2= 2.80"
17.7	694	0.0170	0.65		Shallow Concentrated Flow, Tc-2
					Woodland Kv= 5.0 fps
4.2	280	0.0500	1.12		Shallow Concentrated Flow, Tc-3
					Woodland Kv= 5.0 fps
33.1	1,024	Total			

Summary for Subcatchment EDA-2:

Runoff = 0.49 cfs @ 12.55 hrs, Volume= 0.130 af, Depth> 0.58"	Runoff	=	0.49 cfs @	12.55 hrs.	Volume=	0.130 af, Depth> 0.58"
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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-100yr Rainfall=8.65"

Area	(ac) C	N Dese	cription		
2.	.708 3	30 Woo	ds, Good,	HSG A	
2.	.708	100.	00% Pervi	ous Area	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
11.2	50	0.0300	0.07		Sheet Flow, Tc-1
6.8	392	0.0370	0.96		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps
18.0	442	Total			

Summary for Subcatchment EDA-3:

Runoff = 0.60 cfs @ 12.48 hrs, Volume= 0.148 af, Depth> 0.58"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-100yr Rainfall=8.65"

_	Area	(ac) C	N Des	cription		
	3.	078 3	30 Woo	ods, Good,	HSG A	
-	3.	078	100.	00% Pervi	ous Area	
_	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	10.0	50	0.0400	0.08		Sheet Flow, Tc-1
	1.7	81	0.0250	0.79		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps
	0.8	63	0.0630	1.25		Shallow Concentrated Flow, Tc-3
	0.8	96	0.1560	1.97		Woodland Kv= 5.0 fps Shallow Concentrated Flow, Tc-4 Woodland Kv= 5.0 fps
-	12.2	200	Total			

13.3 290 Total

Summary for Subcatchment EDA-4:

Runoff	=	0.98 cfs @	12.66 hrs, Volume=	0.293 af, Depth> 0.57"
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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-100yr Rainfall=8.65"

Area	(ac) C	N Desc	cription		
6.	.071 3	80 Woo	ds, Good,	HSG A	
0.	<u>.059 3</u>	<u>89 >759</u>	% Grass co	over, Good	, HSG A
6.	130 3	30 Weig	ghted Aver	age	
6.	130	100.	00% Pervi	ous Area	
_				.	-
Tc	Length	Slope	Velocity	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
15.2	50	0.0140	0.05		Sheet Flow, Tc-1
					Woods: Light underbrush n= 0.400 P2= 2.80"
4.8	253	0.0310	0.88		Shallow Concentrated Flow, Tc-2
					Woodland Kv= 5.0 fps
2.2	123	0.0360	0.95		Shallow Concentrated Flow, Tc-3
					Woodland Kv= 5.0 fps
3.6	229	0.0460	1.07		Shallow Concentrated Flow, Tc-4
					Woodland Kv= 5.0 fps
25.8	655	Total			

Summary for Subcatchment EDA-5:

Runoff = 0.62 cfs @ 12.50 hrs, Volume= 0.157 af, Depth> 0.58"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-100yr Rainfall=8.65"

_	Area	(ac) C	N Des	cription		
	3.	277 3	30 Woo	ds, Good,	HSG A	
_	3.	277	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	11.2	50	0.0300	0.07		Sheet Flow, Tc-1
	2.0	70	0.0140	0.59		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps
	1.7	183	0.1260	1.77		Shallow Concentrated Flow, Tc-3 Woodland Kv= 5.0 fps
-	110	202	Total			

14.9 303 Total

Summary for Subcatchment EDA-6:

Runoff = 1.84 cfs @ 12.65 hrs, Volume= 0.542 af, Depth> 0.57"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-100yr Rainfall=8.65"

Area	(ac) C	N Dese	cription		
11.	.289 3	80 Woo	ds, Good,	HSG A	
0.	.059 3	<mark>89 >75</mark> 9	% Grass co	over, Good	, HSG A
11.	.348 3	80 Weig	ghted Aver	age	
11.	.348	100.	00% Pervi	ous Area	
-		01		0	
Tc	Length	Slope	Velocity	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
11.2	50	0.0300	0.07		Sheet Flow, Tc-1
					Woods: Light underbrush n= 0.400 P2= 2.80"
7.1	339	0.0250	0.79		Shallow Concentrated Flow, Tc-2
					Woodland Kv= 5.0 fps
3.2	217	0.0510	1.13		Shallow Concentrated Flow, Tc-3
					Woodland Kv= 5.0 fps
3.6	176	0.0260	0.81		Shallow Concentrated Flow, Tc-4
					Woodland Kv= 5.0 fps
25.1	782	Total			

Summary for Subcatchment EDA-7:

Runoff = 0.49 cfs @ 12.53 hrs, Volume= 0.116 af, Depth> 0.66"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-100yr Rainfall=8.65"

 Area ((ac) (CN	Desc	ription		
1.9	997	30	Woo	ds, Good,	HSG A	
0.0	087	39	>75%	6 Grass co	over, Good	, HSG A
0.0	016	61	>75%	6 Grass co	over, Good	, HSG B
 0.0	004	98	Roof	s, HSG A		
2.	104	31	Weig	ghted Aver	age	
2.	100		99.8	1% Pervio	us Area	
0.0	004		0.19	% Impervi	ous Area	
 Tc (min)	Length (feet)		ope ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
 11.2	50	0.0	300	0.07		Sheet Flow, Tc-1
7.6	332	2 0.02	210	0.72		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps
18.8	382	. Tot	al			

Summary for Reach DP-1:

Inflow Are	a =	42.430 ac,	0.12% Impervious, Inflow	Depth > 1.22"	for Plymouth-100yr event
Inflow	=	23.07 cfs @	12.60 hrs, Volume=	4.312 af	
Outflow	=	23.07 cfs @	12.60 hrs, Volume=	4.312 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-2:

Inflow Area	a =	2.708 ac,	0.00% Impervious, Inflow	Depth > 0.58"	for Plymouth-100yr event
Inflow	=	0.49 cfs @	12.55 hrs, Volume=	0.130 af	
Outflow	=	0.49 cfs @	12.55 hrs, Volume=	0.130 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-3:

Inflow Area =	3.078 ac,	0.00% Impervious, Inflow Dep	oth > 0.58" for Plymouth-100yr event
Inflow =	0.60 cfs @	12.48 hrs, Volume= 0).148 af
Outflow =	0.60 cfs @	12.48 hrs, Volume= 0).148 af, Atten= 0%, Lag= 0.0 min

Summary for Reach DP-4:

Inflow Are	a =	6.130 ac,	0.00% Impervious, Inflow De	oth > 0.57" fo	r Plymouth-100yr event
Inflow	=	0.98 cfs @	12.66 hrs, Volume=	0.293 af	
Outflow	=	0.98 cfs @	12.66 hrs, Volume=	0.293 af, Atten=	0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-5:

Inflow Area	a =	3.277 ac,	0.00% Impervious, Inflow E	Depth > 0.58"	for Plymouth-100yr event
Inflow	=	0.62 cfs @	12.50 hrs, Volume=	0.157 af	
Outflow	=	0.62 cfs @	12.50 hrs, Volume=	0.157 af, Att	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-6:

Inflow Area =	11.348 ac,	0.00% Impervious, Inflow D	Depth > 0.57"	for Plymouth-100yr event
Inflow =	1.84 cfs @	12.65 hrs, Volume=	0.542 af	
Outflow =	1.84 cfs @	12.65 hrs, Volume=	0.542 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-7:

Inflow Are	a =	2.104 ac,	0.19% Impervious, Ir	nflow Depth > 0.66"	for Plymouth-100yr event
Inflow	=	0.49 cfs @	12.53 hrs, Volume=	0.116 af	
Outflow	=	0.49 cfs @	12.53 hrs, Volume=	0.116 af, Att	en= 0%, Lag= 0.0 min

Attachment 3 Post-Development Hydrologic Analysis





POST-DEVELOPMENT CONDITIONS HYDROLOGIC ANALYSIS

OBJECTIVE

To determine the post-development peak rates of runoff from the site for the 2-, 10-, 25-, 50-, and 100-year storm events.

CONCLUSION

Peak Runoff Rates

The following numbers represent the peak rates of runoff from the site under the post-development conditions:

Storm	2 Year	10 Year	25 Year	50 Year	100 Year
Event	Post (cfs)				
DP-1	0.00	0.73	3.85	10.76	23.07
DP-2	0.00	0.00	0.03	0.10	0.49
DP-3	0.00	0.00	0.04	0.12	0.60
DP-4	0.00	0.01	0.06	0.22	0.96
DP-5	0.00	0.00	0.04	0.12	0.62
DP-6	0.00	0.01	0.13	0.43	1.84
DP-7	0.00	0.00	0.03	0.12	0.49

In accordance with the MassDEP Stormwater Handbook, post-development peak runoff rates are less than or equal to pre-development peak runoff rates under the 2-, 10-, 25-, 50-, and 100-year storm events.

CALCULATION METHODS

- 1. Runoff curve numbers (CN), time-of-concentration (T_c), and runoff rates were calculated based on TR-55 methodology.
- 2. Autodesk Civil 3D 2019 computer program was utilized for digitizing ground cover areas.
- 3. Runoff rates computed using HydroCAD version 10.10.

ASSUMPTIONS

- 1. The ground cover types and boundaries were determined using the Topographic Plan, MassGIS aerial imagery, aerial imagery viewed on Google Earth, and hydrologic soil groups based on United States Department of Agriculture, NRCS Soil Survey map information.
- 2. The subcatchment limits were truncated at the property line, except for the northeastern portion of EDA-1/PDA-1.
 - This subcatchment expanded beyond the property line in order to include runoff that the Property receives from the abutting property owned by Wareham Little League Inc.

REV	CALC. BY	DATE	CHECKED BY	DATE	APPROVED BY	DATE
0	RFK	11/08/2021	KJP	11/12/2021	MC	11/17/2021

RFK/kjp/mc/1833109CS005A

Civil Engineering • Land Surveying • Landscape Architecture • Land Use Permitting • Environmental Planning • Wetland Science



SOURCES OF DATA/ EQUATIONS

- 1. NRCS Soil Map for Plymouth County, downloaded from Web Soil Survey on 4/15/2020.
- 2. Topographic Plan, prepared by Northeast Survey Consultants and B+T, dated 11/19/2021.
- 3. Post-Development Conditions Hydrologic Areas Map, prepared by B+T, dated 11/08/2021.
- 4. Proposed Site Plan Design File, B+T File No. 1833109D076B.
- 5. Pre-Development Hydrologic Calculations, B+T File No. 1833109CS001, dated 05/22/2020.
- 6. TR-55 Urban Hydrology for Small Watersheds, SCS, 1986.
- 7. Massachusetts DEP Stormwater Management Handbook, February 2008.
- 8. Town of Wareham Rules & Regulations Governing the Subdivision of Land, March 2013.

LIST OF ATTACHMENTS

1. Post-Development Conditions: Hydrologic Areas Map and HydroCAD Report

REV	CALC. BY	DATE	CHECKED BY	DATE	APPROVED BY	DATE
0	RFK	11/08/2021	KJP	11/12/2021	MC	11/17/2021

RFK/kjp/mc/1833109CS005A

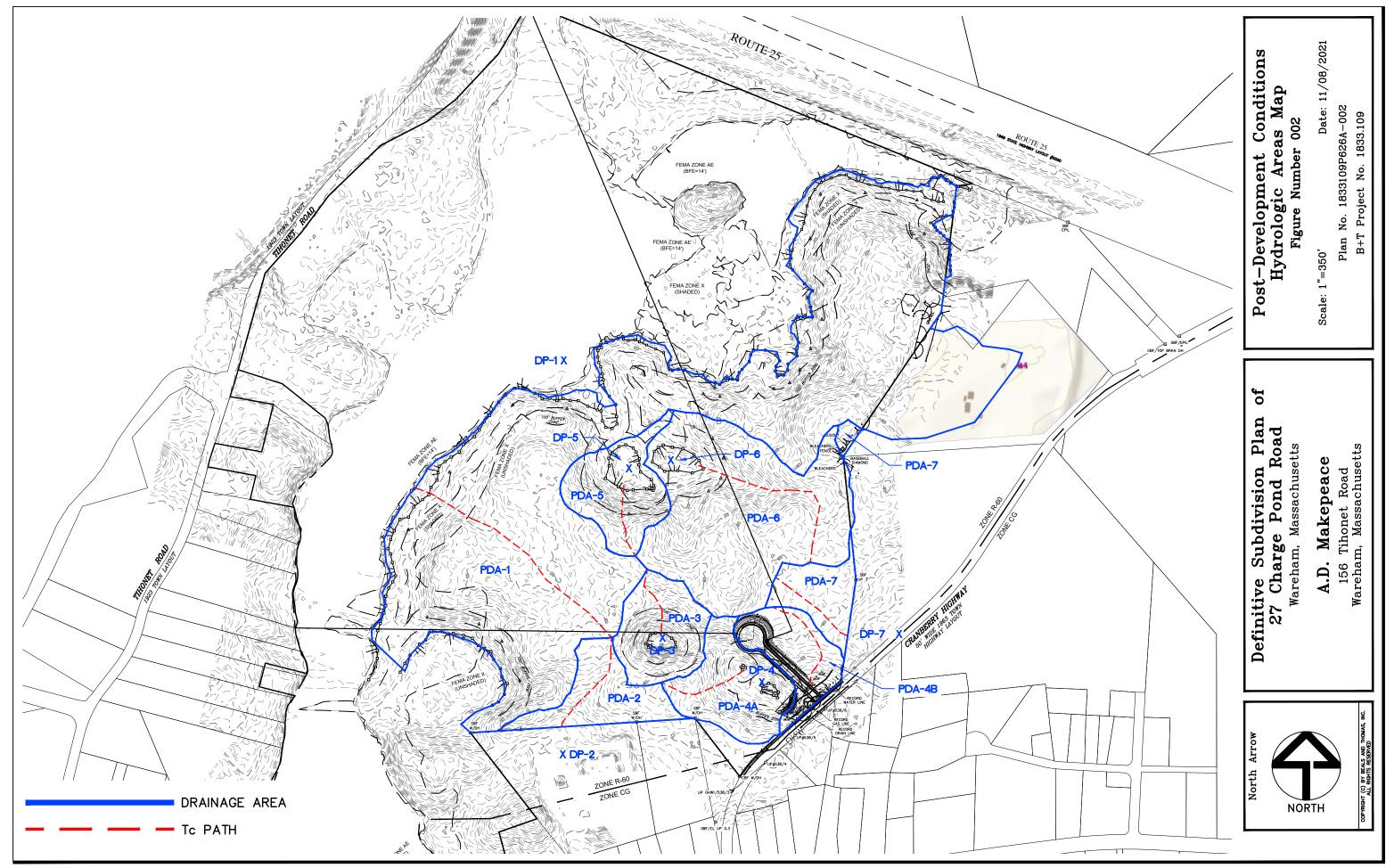
Civil Engineering • Land Surveying • Landscape Architecture • Land Use Permitting • Environmental Planning • Wetland Science

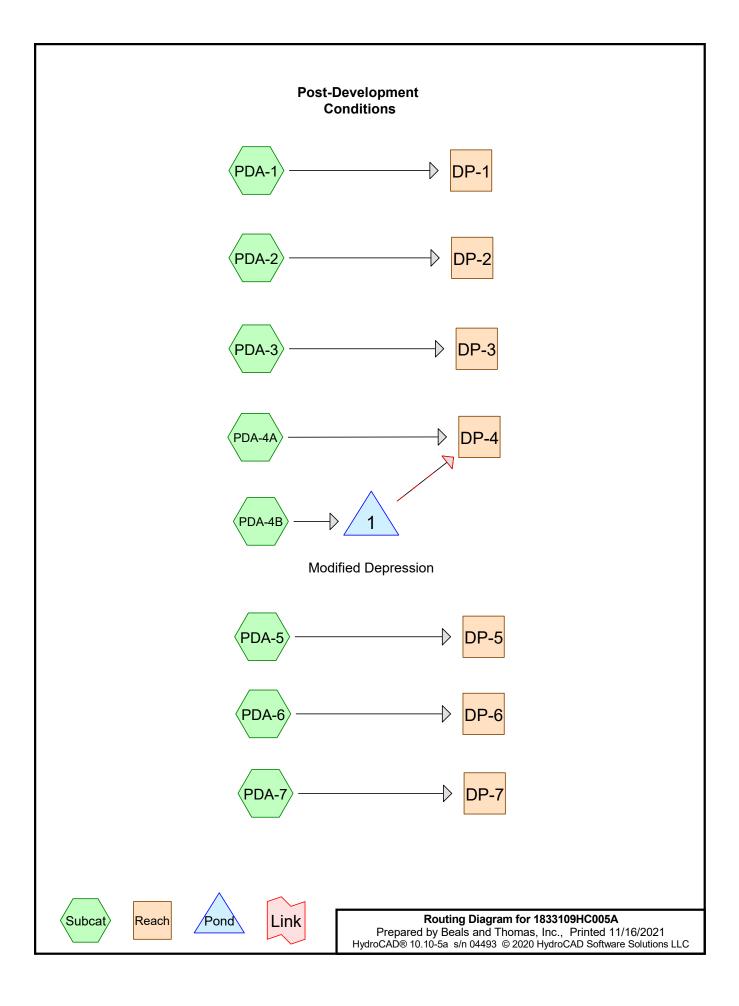
Attachment 1

Post-Development Conditions: Hydrologic Areas Map and HydroCAD Report









Area Listing (all nodes)

	Area	CN	Description
((acres)		(subcatchment-numbers)
	2.943	39	>75% Grass cover, Good, HSG A (PDA-1, PDA-4A, PDA-4B, PDA-6, PDA-7)
	3.732	61	>75% Grass cover, Good, HSG B (PDA-1, PDA-7)
	0.413	96	Gravel surface, HSG B (PDA-1)
	0.404	98	Paved parking, HSG A (PDA-4B)
	0.004	98	Roofs, HSG A (PDA-7)
	0.049	98	Roofs, HSG B (PDA-1)
Ę	59.596	30	Woods, Good, HSG A (PDA-1, PDA-2, PDA-3, PDA-4A, PDA-4B, PDA-5, PDA-6,
			PDA-7)
	2.936	55	Woods, Good, HSG B (PDA-1)
	0.998	77	Woods, Good, HSG D (PDA-1)
	71.075	35	TOTAL AREA

1833109HC005A	Type III 24-hr Plymouth-002yr Rainfall=3.36"
Prepared by Beals and Thomas, Inc.	Printed 11/16/2021
HydroCAD® 10.10-5a s/n 04493 © 2020 HydroCAD Softward	re Solutions LLC Page 3

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment PDA-1:	Runoff Area=42.430 ac 0.12% Impervious Runoff Depth=0.00" Flow Length=1,024' Tc=33.1 min CN=37 Runoff=0.00 cfs 0.000 af
Subcatchment PDA-2:	Runoff Area=2.708 ac 0.00% Impervious Runoff Depth=0.00"
	Flow Length=442' Tc=18.0 min CN=30 Runoff=0.00 cfs 0.000 af
Subcatchment PDA-3:	Runoff Area=3.078 ac 0.00% Impervious Runoff Depth=0.00" Flow Length=290' Tc=13.3 min CN=30 Runoff=0.00 cfs 0.000 af
Subcatchment PDA-4A:	Runoff Area=3.613 ac 0.00% Impervious Runoff Depth=0.00" Flow Length=367' Tc=15.6 min CN=31 Runoff=0.00 cfs 0.000 af
Subcatchment PDA-4B:	Runoff Area=2.517 ac 16.05% Impervious Runoff Depth>0.05" Flow Length=424' Tc=20.9 min CN=44 Runoff=0.02 cfs 0.010 af
Subcatchment PDA-5:	Runoff Area=3.277 ac 0.00% Impervious Runoff Depth=0.00" Flow Length=303' Tc=14.9 min CN=30 Runoff=0.00 cfs 0.000 af
Subcatchment PDA-6:	Runoff Area=11.348 ac 0.00% Impervious Runoff Depth=0.00" Flow Length=782' Tc=25.1 min CN=30 Runoff=0.00 cfs 0.000 af
Subcatchment PDA-7:	Runoff Area=2.104 ac 0.19% Impervious Runoff Depth=0.00" Flow Length=382' Tc=18.8 min CN=31 Runoff=0.00 cfs 0.000 af
Reach DP-1:	Inflow=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af
Reach DP-2:	Inflow=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af
Reach DP-3:	Inflow=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af
Reach DP-4:	Inflow=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af
Reach DP-5:	Inflow=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af
Reach DP-6:	Inflow=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af
Reach DP-7:	Inflow=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af

Pond 1: Modified DepressionPeak Elev=22.01'Storage=11 cfInflow=0.02 cfs0.010 afDiscarded=0.02 cfs0.010 afPrimary=0.00 cfs0.000 afSecondary=0.00 cfs0.000 afOutflow=0.02 cfs0.010 af

Total Runoff Area = 71.075 acRunoff Volume = 0.010 afAverage Runoff Depth = 0.00"99.36% Pervious = 70.618 ac0.64% Impervious = 0.457 ac

Summary for Subcatchment PDA-1:

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-002yr Rainfall=3.36"

Area	(ac)	CN	Desc	cription		
32.	525	30	Woo	ds, Good,	HSG A	
2.	936	55	Woo	ds, Good,	HSG B	
0.	998	77	Woo	ds, Good,	HSG D	
1.	793	39	>75%	6 Grass co	over, Good	, HSG A
3.	716	61	>75%	6 Grass co	over, Good	, HSG B
0.	413	96	Grav	el surface	, HSG B	
0.	049	98	Roof	s, HSG B		
42.	430	37	Weig	phted Aver	age	
42.	381		99.8	8% Pervio	us Area	
0.	049		0.12	% Impervi	ous Area	
Tc	Length	n S	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·
11.2	50	0.0	0300	0.07		Sheet Flow, Tc-1
						Woods: Light underbrush n= 0.400 P2= 2.80"
17.7	694	4 0.0	0170	0.65		Shallow Concentrated Flow, Tc-2
						Woodland Kv= 5.0 fps
4.2	280	0.0	0500	1.12		Shallow Concentrated Flow, Tc-3
						Woodland Kv= 5.0 fps
33.1	1,024	4 To	otal			

Summary for Subcatchment PDA-2:

Runoff	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-002yr Rainfall=3.36"

_	Area	(ac) C	N Des	cription		
2.708 30 Woods, Good, HSG A					HSG A	
	2.708 100.00% Pervious Area				ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	11.2	50	0.0300	0.07		Sheet Flow, Tc-1
	6.8	392	0.0370	0.96		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps
-	18.0	442	Total			

Summary for Subcatchment PDA-3:

Page 6

Runoff 0.00 hrs, Volume= = 0.00 cfs @ 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-002yr Rainfall=3.36"

_	Area	(ac) C	N Dese	cription		
	3.078 30 Woods, Good, HSG A			ds, Good,	HSG A	
	3.078 100.00% Pervious Area				ous Area	
_	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	10.0	50	0.0400	0.08		Sheet Flow, Tc-1
	1.7	81	0.0250	0.79		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps
	0.8	63	0.0630	1.25		Shallow Concentrated Flow, Tc-3
						Woodland Kv= 5.0 fps
	0.8	96	0.1560	1.97		Shallow Concentrated Flow, Tc-4
_						Woodland Kv= 5.0 fps
	13.3	290	Total			

Summary for Subcatchment PDA-4A:

Runoff	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af, Depth= 0.00"
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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-002yr Rainfall=3.36"

Area	(ac) C	N Des	cription		
3.374 30 Woods, Good, HSG A			, , ,		
0.239 39 >75% Grass cover, Good, HSG A					, HSG A
3.613 31 Weighted Average					
3.	3.613 100.00% Pervious Area			ous Area	
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
11.2	50	0.0300	0.07		Sheet Flow, Tc-1
					Woods: Light underbrush n= 0.400 P2= 2.80"
1.6	99	0.0400	1.00		Shallow Concentrated Flow, Tc-2
					Woodland Kv= 5.0 fps
2.7	218	0.0730	1.35		Shallow Concentrated Flow, Tc-3
					Woodland Kv= 5.0 fps
15.6	367	Total			

Summary for Subcatchment PDA-4B:

Runoff 0.02 cfs @ 15.52 hrs, Volume= 0.010 af, Depth> 0.05" =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-002yr Rainfall=3.36"

Area	(ac) C	N Des	cription		
1.	357 3	30 Woo	ods, Good,	HSG A	
0.	756 3	39 >75	% Grass co	over, Good	, HSG A
0.	404 9	98 Pave	ed parking	, HSG A	
2.	517 4	14 Wei	ghted Aver	age	
2.	113	83.9	5% Pervio	us Area	
0.	404	16.0	5% Imper	ious Area	
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
15.2	50	0.0140	0.05		Sheet Flow, Tc-1
					Woods: Light underbrush n= 0.400 P2= 2.80"
4.8	253	0.0310	0.88		Shallow Concentrated Flow, Tc-2
					Woodland Kv= 5.0 fps
0.7	61	0.0740	1.36		Shallow Concentrated Flow, Tc-3
					Woodland Kv= 5.0 fps
0.2	60	0.1250	5.30		Shallow Concentrated Flow, Tc-4
					Grassed Waterway Kv= 15.0 fps
20.9	424	Total			

Summary for Subcatchment PDA-5:

Runoff	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af, Depth= 0.00"
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 Area	(ac) C	N Dese	cription		
3.	277 3	30 Woo	ds, Good,	HSG A	
3.	277	100.	00% Pervi	ous Area	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
 11.2	50	0.0300	0.07		Sheet Flow, Tc-1
2.0	70	0.0140	0.59		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps
1.7	183	0.1260	1.77		Shallow Concentrated Flow, Tc-3 Woodland Kv= 5.0 fps
14.9	303	Total			

Summary for Subcatchment PDA-6:

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-002yr Rainfall=3.36"

Area	(ac) C	N Desc	cription			
11.	.280 3	0 Woo	ds, Good,	HSG A		
0.	.068 3	9 >759	% Grass co	over, Good	, HSG A	
11.	11.348 30 Weighted Average					
11.	.348	100.	00% Pervi	ous Area		
-		0		0		
Tc	Length	Slope	Velocity	Capacity	Description	
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)		
11.2	50	0.0300	0.07		Sheet Flow, Tc-1	
					Woods: Light underbrush n= 0.400 P2= 2.80"	
7.1	339	0.0250	0.79		Shallow Concentrated Flow, Tc-2	
					Woodland Kv= 5.0 fps	
3.2	217	0.0510	1.13		Shallow Concentrated Flow, Tc-3	
					Woodland Kv= 5.0 fps	
3.6	176	0.0260	0.81		Shallow Concentrated Flow, Tc-4	
					Woodland Kv= 5.0 fps	
25.1	782	Total				

Summary for Subcatchment PDA-7:

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Area (a	ic) C	N Desc	cription		
1.99	97 3	0 Woo	ds, Good,	HSG A	
30.0	87 3	9 >75%	% Grass co	over, Good	, HSG A
0.01	16 6	1 >75%	% Grass co	over, Good	, HSG B
0.00	04 9	8 Roof	s, HSG A		
2.10	04 3	1 Weig	ghted Aver	age	
2.10	00	99.8	1% Pervio	us Area	
0.00	04	0.19	% Impervi	ous Area	
Tc L (min)	_ength (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
11.2	50	0.0300	0.07		Sheet Flow, Tc-1
7.6	332	0.0210	0.72		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps
18.8	382	Total			

Summary for Reach DP-1:

Inflow Area	a =	42.430 ac,	0.12% Impervious, Inflow D	epth = 0.00" for Plymouth-0	02yr event
Inflow	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af	-
Outflow	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af, Atten= 0%, Lag= 0.	0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-2:

Inflow Are	a =	2.708 ac,	0.00% Impervious, Inflow D	epth = 0.00"	for Plymouth-002yr event
Inflow	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af	
Outflow	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-3:

Inflow Area =	3.078 ac,	0.00% Impervious, Inflow Depth = 0.00" for Plymouth-002yr event
Inflow =	0.00 cfs @	0.00 hrs, Volume= 0.000 af
Outflow =	0.00 cfs @	0.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-4:

Inflow Are	a =	6.130 ac,	6.59% Impervious, Inflow D	epth = 0.00"	for Plymouth-002yr event
Inflow	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af	
Outflow	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-5:

Inflow Area =	3.277 ac,	0.00% Impervious, Inflow D	Depth = 0.00" for Plymouth-002yr event
Inflow =	0.00 cfs @	0.00 hrs, Volume=	0.000 af
Outflow =	0.00 cfs @	0.00 hrs, Volume=	0.000 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-6:

Inflow Area	a =	11.348 ac,	0.00% Impervious, Inflow Depth = 0.00" for Plymouth-002yr event
Inflow	=	0.00 cfs @	0.00 hrs, Volume= 0.000 af
Outflow	=	0.00 cfs @	0.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-7:

Inflow Are	a =	2.104 ac,	0.19% Impervious, Inflow D	epth = 0.00"	for Plymouth-002yr event
Inflow	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af	
Outflow	=	0.00 cfs @	0.00 hrs, Volume=	0.000 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Pond 1: Modified Depression

Inflow Area =	2.517 ac, 16.05% Impervious, Inflow De	pth > 0.05" for Plymouth-002yr event
Inflow =	0.02 cfs @ 15.52 hrs, Volume=	0.010 af
Outflow =	0.02 cfs @ 15.72 hrs, Volume=	0.010 af, Atten= 1%, Lag= 12.0 min
Discarded =	0.02 cfs @ 15.72 hrs, Volume=	0.010 af
Primary =	0.00 cfs @ 0.00 hrs, Volume=	0.000 af
Secondary =	0.00 cfs $\overline{@}$ 0.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 22.01' @ 15.72 hrs Surf.Area= 929 sf Storage= 11 cf

Plug-Flow detention time= 11.6 min calculated for 0.010 af (98% of inflow) Center-of-Mass det. time= 6.9 min (1,115.2 - 1,108.4)

Volume	Invert	Avail.Sto	rage Storage	e Description	
#1	22.00'	13,98	35 cf Custon	n Stage Data (Pr	ismatic) Listed below (Recalc)
Elevatio (fee		ırf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
22.0 23.0 24.0 25.0 26.0	00 00 00 00	915 2,091 3,267 4,879 6,581	0 1,503 2,679 4,073 5,730	0 1,503 4,182 8,255 13,985	
Device	Routing	Invert	Outlet Device	es	
#1 #2 #3	Discarded Primary Secondary	22.00' 24.20' 25.00'	12.0" Round L= 19.0' CP Inlet / Outlet n= 0.013 Co 20.0' long x Head (feet)	PP, projecting, no Invert= 24.20' / 2 prrugated PE, sm	b headwall, Ke= 0.900 24.00' S= 0.0105 '/' Cc= 0.900 booth interior, Flow Area= 0.79 sf bad-Crested Rectangular Weir 0.80 1.00

Discarded OutFlow Max=0.05 cfs @ 15.72 hrs HW=22.01' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.05 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=22.00' (Free Discharge) ←2=Culvert (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=22.00' (Free Discharge) —3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

1833109HC005A	Type III 24-hr Plymouth-010yr Rainfall=4.95"
Prepared by Beals and Thomas, Inc.	Printed 11/16/2021
HydroCAD® 10.10-5a s/n 04493 © 2020 HydroCAD Softwar	e Solutions LLC Page 12

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment PDA-1:	Runoff Area=42.430 ac 0.12% Impervious Runoff Depth>0.13" Flow Length=1,024' Tc=33.1 min CN=37 Runoff=0.73 cfs 0.442 af
Subcatchment PDA-2:	Runoff Area=2.708 ac 0.00% Impervious Runoff Depth>0.00" Flow Length=442' Tc=18.0 min CN=30 Runoff=0.00 cfs 0.001 af
Subcatchment PDA-3:	Runoff Area=3.078 ac 0.00% Impervious Runoff Depth>0.00" Flow Length=290' Tc=13.3 min CN=30 Runoff=0.00 cfs 0.001 af
Subcatchment PDA-4A:	Runoff Area=3.613 ac 0.00% Impervious Runoff Depth>0.01" Flow Length=367' Tc=15.6 min CN=31 Runoff=0.01 cfs 0.003 af
Subcatchment PDA-4B:	Runoff Area=2.517 ac 16.05% Impervious Runoff Depth>0.38" Flow Length=424' Tc=20.9 min CN=44 Runoff=0.33 cfs 0.079 af
Subcatchment PDA-5:	Runoff Area=3.277 ac 0.00% Impervious Runoff Depth>0.00" Flow Length=303' Tc=14.9 min CN=30 Runoff=0.00 cfs 0.001 af
Subcatchment PDA-6:	Runoff Area=11.348 ac 0.00% Impervious Runoff Depth>0.00" Flow Length=782' Tc=25.1 min CN=30 Runoff=0.01 cfs 0.003 af
Subcatchment PDA-7:	Runoff Area=2.104 ac 0.19% Impervious Runoff Depth>0.01" Flow Length=382' Tc=18.8 min CN=31 Runoff=0.00 cfs 0.002 af
Reach DP-1:	Inflow=0.73 cfs 0.442 af Outflow=0.73 cfs 0.442 af
Reach DP-2:	Inflow=0.00 cfs 0.001 af Outflow=0.00 cfs 0.001 af
Reach DP-3:	Inflow=0.00 cfs 0.001 af Outflow=0.00 cfs 0.001 af
Reach DP-4:	Inflow=0.01 cfs 0.003 af Outflow=0.01 cfs 0.003 af
Reach DP-5:	Inflow=0.00 cfs 0.001 af Outflow=0.00 cfs 0.001 af
Reach DP-6:	Inflow=0.01 cfs 0.003 af Outflow=0.01 cfs 0.003 af
Reach DP-7:	Inflow=0.00 cfs 0.002 af Outflow=0.00 cfs 0.002 af

Pond 1: Modified DepressionPeak Elev=22.67' Storage=870 cfInflow=0.33 cfs0.079 afDiscarded=0.09 cfs0.078 afPrimary=0.00 cfs0.000 afSecondary=0.00 cfs0.000 afOutflow=0.09 cfs0.078 af

Total Runoff Area = 71.075 acRunoff Volume = 0.532 afAverage Runoff Depth = 0.09"99.36% Pervious = 70.618 ac0.64% Impervious = 0.457 ac

Summary for Subcatchment PDA-1:

Runoff = 0.73 cfs @ 15.05 hrs, Volume= 0.442 af, Depth> 0.13"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-010yr Rainfall=4.95"

Area	(ac) (CN De	scription		
32.	.525	30 Wo	ods, Good,	HSG A	
2.	.936	55 Wc	ods, Good,	HSG B	
0.	.998	77 Wc	ods, Good,	HSG D	
1.	.793	39 >75	5% Grass c	over, Good	, HSG A
3.	.716	61 >75	5% Grass c	over, Good	, HSG B
0.	.413	96 Gra	vel surface	, HSG B	
0.	.049	98 Ro	ofs, HSG B		
42.	.430	37 We	ighted Ave	rage	
42.	.381	99.	88% Pervic	us Area	
0.	.049	0.1	2% Impervi	ous Area	
Tc	Length			Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
11.2	50	0.0300	0.07		Sheet Flow, Tc-1
					Woods: Light underbrush n= 0.400 P2= 2.80"
17.7	694	0.0170	0.65		Shallow Concentrated Flow, Tc-2
					Woodland Kv= 5.0 fps
4.2	280	0.0500	1.12		Shallow Concentrated Flow, Tc-3
					Woodland Kv= 5.0 fps
33.1	1,024	Total			

Summary for Subcatchment PDA-2:

Runoff	=	0.00 cfs @	24.00 hrs.	Volume=	0.001 af, Depth> 0.00"

_	Area	(ac) C	N Des	cription		
_	2.	708 3	30 Woo	ds, Good,	HSG A	
2.708 100.00% Pervious Area						
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	11.2	50	0.0300	0.07		Sheet Flow, Tc-1
	6.8	392	0.0370	0.96		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps
-	18.0	442	Total			

Summary for Subcatchment PDA-3:

Runoff = 0.00 cfs @ 24.00 hrs, Volume= 0.001 af, Depth> 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-010yr Rainfall=4.95"

_	Area	(ac) C	N Desc	cription		
_	3.	078 3	80 Woo	ds, Good,	HSG A	
	3.	078	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	10.0	50	0.0400	0.08		Sheet Flow, Tc-1
	1.7	81	0.0250	0.79		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps
	0.8	63	0.0630	1.25		Shallow Concentrated Flow, Tc-3
						Woodland Kv= 5.0 fps
	0.8	96	0.1560	1.97		Shallow Concentrated Flow, Tc-4
_						Woodland Kv= 5.0 fps
	13.3	290	Total			

Summary for Subcatchment PDA-4A:

Runoff	=	0.01 cfs @	22.84 hrs, Volume=	0.003 af, Depth> 0.01"
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Area	(ac) C	N Dese	cription		
-			ds, Good,		
0.	<u>239</u> 3	<u>89 >759</u>	<u>% Grass co</u>	over, Good	, HSG A
3.	613 3	31 Weig	ghted Aver	age	
3.	613	100.	00% Pervi	ous Area	
Тс	Length	Slope	Velocity	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
11.2	50	0.0300	0.07		Sheet Flow, Tc-1
					Woods: Light underbrush n= 0.400 P2= 2.80"
1.6	99	0.0400	1.00		Shallow Concentrated Flow, Tc-2
					Woodland Kv= 5.0 fps
2.7	218	0.0730	1.35		Shallow Concentrated Flow, Tc-3
					Woodland Kv= 5.0 fps
15.6	367	Total			

Summary for Subcatchment PDA-4B:

Runoff = 0.33 cfs @ 12.56 hrs, Volume= 0.079 af, Depth> 0.38"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-010yr Rainfall=4.95"

Area	(ac) C	N Dese	cription					
1.	1.357 30 Woods, Good, HSG A							
0.	756 3	39 >759	% Grass co	over, Good	, HSG A			
0.	404 9	8 Pave	ed parking	, HSG A				
2.	517 4	4 Wei	phted Aver	age				
2.	113	•	5% Pervio	0				
0.	404	16.0	5% Imper	ious Area				
			•					
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
15.2	50	0.0140	0.05		Sheet Flow, Tc-1			
					Woods: Light underbrush n= 0.400 P2= 2.80"			
4.8	253	0.0310	0.88		Shallow Concentrated Flow, Tc-2			
					Woodland Kv= 5.0 fps			
0.7	61	0.0740	1.36		Shallow Concentrated Flow, Tc-3			
					Woodland Kv= 5.0 fps			
0.2	60	0.1250	5.30		Shallow Concentrated Flow, Tc-4			
					Grassed Waterway Kv= 15.0 fps			
20.9	424	Total						

Summary for Subcatchment PDA-5:

Runoff	=	0.00 cfs @	24.00 hrs.	Volume=	0.001 af,	Depth>	0.00"
runon		0.00 010 @	24.00 110,	Volumo	0.001 ui,	Dopur	0.00

Area	(ac) C	N Desc	cription		
3	.277 3	30 Woo	ds, Good,	HSG A	
3	.277	100.	00% Pervi	ous Area	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
11.2	50	0.0300	0.07		Sheet Flow, Tc-1
2.0	70	0.0140	0.59		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps
1.7	183	0.1260	1.77		Shallow Concentrated Flow, Tc-3 Woodland Kv= 5.0 fps
14.9	303	Total			

Summary for Subcatchment PDA-6:

Runoff = 0.01 cfs @ 24.00 hrs, Volume= 0.003 af, Depth> 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-010yr Rainfall=4.95"

Area	(ac) C	N Desc	cription				
11.	.280 3	80 Woo	ds, Good,	HSG A			
0.	.068 3	<mark>89 >75</mark> 9	% Grass co	over, Good	, HSG A		
11.	11.348 30 Weighted Average						
11.	11.348 100.00% Pervious Area						
т	1		\/.l!t	0	Description		
Tc	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
11.2	50	0.0300	0.07		Sheet Flow, Tc-1		
					Woods: Light underbrush n= 0.400 P2= 2.80"		
7.1	339	0.0250	0.79		Shallow Concentrated Flow, Tc-2		
					Woodland Kv= 5.0 fps		
3.2	217	0.0510	1.13		Shallow Concentrated Flow, Tc-3		
					Woodland Kv= 5.0 fps		
3.6	176	0.0260	0.81		Shallow Concentrated Flow, Tc-4		
					Woodland Kv= 5.0 fps		
25.1	782	Total					

Summary for Subcatchment PDA-7:

Runoff = 0.00 cfs @ 22.87 hrs, Volume= 0.002 af, Depth> 0.01"

Area (a	ac) C	N Desc	cription					
1.9	97 3	0 Woo	/oods, Good, HSG A					
0.0	87 3	9 > 759	% Grass co	over, Good	, HSG A			
0.0	16 6	51 >759	% Grass co	over, Good	, HSG B			
0.0	04 9	8 Root	s, HSG A					
2.1	04 3	1 Weig	ghted Aver	age				
2.1	00	99.8	1% Pervio	us Area				
0.0	04	0.19	% Impervi	ous Area				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
11.2	50	0.0300	0.07		Sheet Flow, Tc-1			
7.6	332	0.0210	0.72		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps			
18.8	382	Total						

Summary for Reach DP-1:

Inflow Are	a =	42.430 ac,	0.12% Impervious, Inflow D	epth > 0.13"	for Plymouth-010yr event
Inflow	=	0.73 cfs @	15.05 hrs, Volume=	0.442 af	
Outflow	=	0.73 cfs @	15.05 hrs, Volume=	0.442 af, Atter	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-2:

Inflow Area	a =	2.708 ac,	0.00% Impervious, Inflow D	epth > 0.00"	for Plymouth-010yr event
Inflow	=	0.00 cfs @	24.00 hrs, Volume=	0.001 af	
Outflow	=	0.00 cfs @	24.00 hrs, Volume=	0.001 af, Att	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-3:

Inflow Area	a =	3.078 ac,	0.00% Impervious, Inflow Depth > 0.00" for Plymouth-010yr even	ıt
Inflow	=	0.00 cfs @	24.00 hrs, Volume= 0.001 af	
Outflow	=	0.00 cfs @	24.00 hrs, Volume= 0.001 af, Atten= 0%, Lag= 0.0 min	

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-4:

Inflow Are	a =	6.130 ac,	6.59% Impervious, Inflow D	epth > 0.01"	for Plymouth-010yr event
Inflow	=	0.01 cfs @	22.84 hrs, Volume=	0.003 af	
Outflow	=	0.01 cfs @	22.84 hrs, Volume=	0.003 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-5:

Inflow Area	a =	3.277 ac,	0.00% Impervious, Inflow De	epth > 0.00" for Plymouth-010yr event
Inflow	=	0.00 cfs @	24.00 hrs, Volume=	0.001 af
Outflow	=	0.00 cfs @	24.00 hrs, Volume=	0.001 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-6:

Inflow Area	a =	11.348 ac,	0.00% Impervious, Inflow Depth > 0.00" for Plymouth-010yr event
Inflow	=	0.01 cfs @	24.00 hrs, Volume= 0.003 af
Outflow	=	0.01 cfs @	24.00 hrs, Volume= 0.003 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-7:

Inflow Area	a =	2.104 ac,	0.19% Impervious, Inflow De	epth > 0.01" fo	or Plymouth-010yr event
Inflow	=	0.00 cfs @	22.87 hrs, Volume=	0.002 af	
Outflow	=	0.00 cfs @	22.87 hrs, Volume=	0.002 af, Atten=	= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Pond 1: Modified Depression

Inflow Area =	2.517 ac, 16.05% Impervious, Inflow	Depth > 0.38" for Plymouth-010yr event
Inflow =	0.33 cfs @ 12.56 hrs, Volume=	0.079 af
Outflow =	0.09 cfs @ 15.69 hrs, Volume=	0.078 af, Atten= 71%, Lag= 187.8 min
Discarded =	0.09 cfs @ 15.69 hrs, Volume=	0.078 af
Primary =	0.00 cfs @ 0.00 hrs, Volume=	0.000 af
Secondary =	0.00 cfs $\overline{@}$ 0.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 22.67' @ 15.69 hrs Surf.Area= 1,698 sf Storage= 870 cf

Plug-Flow detention time= 112.0 min calculated for 0.078 af (98% of inflow) Center-of-Mass det. time= 102.5 min (1,068.1 - 965.6)

Volume	Invert	Avail.Sto	rage Storage	Description	
#1	22.00'	13,98	35 cf Custom	n Stage Data (Pr	ismatic) Listed below (Recalc)
Elevatio (fee		rf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
22.0 23.0 24.0 25.0 26.0)0)0)0)0	915 2,091 3,267 4,879 6,581	0 1,503 2,679 4,073 5,730	0 1,503 4,182 8,255 13,985	
Device	Routing	Invert	Outlet Device		
#1 #2 #3	#1 Discarded 22.00' #2 Primary 24.20'		12.0" Round L= 19.0' CPI Inlet / Outlet I n= 0.013 Coi 20.0' long x Head (feet) 0	P, projecting, no Invert= 24.20' / 2 rrugated PE, smo	headwall, Ke= 0.900 4.00' S= 0.0105 '/' Cc= 0.900 ooth interior, Flow Area= 0.79 sf oad-Crested Rectangular Weir 0.80 1.00

Discarded OutFlow Max=0.09 cfs @ 15.69 hrs HW=22.67' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.09 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=22.00' (Free Discharge) ←2=Culvert (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=22.00' (Free Discharge) —3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

1833109HC005A	Type III 24-hr Plymouth-025yr Rainfall=6.18
Prepared by Beals and Thomas, Inc.	Printed 11/16/2021
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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment PDA-1:	Runoff Area=42.430 ac 0.12% Impervious Runoff Depth>0.38" Flow Length=1,024' Tc=33.1 min CN=37 Runoff=3.85 cfs 1.350 af
Subcatchment PDA-2:	Runoff Area=2.708 ac 0.00% Impervious Runoff Depth>0.09" Flow Length=442' Tc=18.0 min CN=30 Runoff=0.03 cfs 0.020 af
Subcatchment PDA-3:	Runoff Area=3.078 ac 0.00% Impervious Runoff Depth>0.09" Flow Length=290' Tc=13.3 min CN=30 Runoff=0.04 cfs 0.023 af
Subcatchment PDA-4A:	Runoff Area=3.613 ac 0.00% Impervious Runoff Depth>0.12" Flow Length=367' Tc=15.6 min CN=31 Runoff=0.06 cfs 0.037 af
Subcatchment PDA-4B:	Runoff Area=2.517 ac 16.05% Impervious Runoff Depth>0.80" Flow Length=424' Tc=20.9 min CN=44 Runoff=1.00 cfs 0.168 af
Subcatchment PDA-5:	Runoff Area=3.277 ac 0.00% Impervious Runoff Depth>0.09" Flow Length=303' Tc=14.9 min CN=30 Runoff=0.04 cfs 0.025 af
Subcatchment PDA-6:	Runoff Area=11.348 ac 0.00% Impervious Runoff Depth>0.09" Flow Length=782' Tc=25.1 min CN=30 Runoff=0.13 cfs 0.085 af
Subcatchment PDA-7:	Runoff Area=2.104 ac 0.19% Impervious Runoff Depth>0.12" Flow Length=382' Tc=18.8 min CN=31 Runoff=0.03 cfs 0.021 af
Reach DP-1:	Inflow=3.85 cfs 1.350 af Outflow=3.85 cfs 1.350 af
Reach DP-2:	Inflow=0.03 cfs 0.020 af Outflow=0.03 cfs 0.020 af
Reach DP-3:	Inflow=0.04 cfs 0.023 af Outflow=0.04 cfs 0.023 af
Reach DP-4:	Inflow=0.06 cfs 0.037 af Outflow=0.06 cfs 0.037 af
Reach DP-5:	Inflow=0.04 cfs 0.025 af Outflow=0.04 cfs 0.025 af
Reach DP-6:	Inflow=0.13 cfs 0.085 af
Reach DP-7:	Outflow=0.13 cfs 0.085 af Inflow=0.03 cfs 0.021 af Outflow=0.03 cfs 0.021 af

Pond 1: Modified DepressionPeak Elev=23.58' Storage=2,925 cfInflow=1.00 cfs0.168 afDiscarded=0.15 cfs0.135 afPrimary=0.00 cfs0.000 afSecondary=0.00 cfs0.000 afOutflow=0.15 cfs0.135 af

Total Runoff Area = 71.075 acRunoff Volume = 1.730 afAverage Runoff Depth = 0.29"99.36% Pervious = 70.618 ac0.64% Impervious = 0.457 ac

Summary for Subcatchment PDA-1:

Runoff = 3.85 cfs @ 12.80 hrs, Volume= 1.350 af, Depth> 0.38"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-025yr Rainfall=6.18"

Area	(ac) C	N Des	cription							
32.	525 3	30 Woo	/oods, Good, HSG A							
2.	936	55 Woo	ods, Good,	HSG B						
0.	998	77 Woo	ods, Good,	HSG D						
1.	793 🗧	39 >75°	% Grass c	over, Good	, HSG A					
3.	716 (61 >75°	% Grass c	over, Good	, HSG B					
0.	413	96 Grav	/el surface	, HSG B						
0.	049 9	98 Roo	fs, HSG B							
42.	430 🗧	37 Wei	ghted Avei	age						
42.	381	99.8	8% Pervio	us Area						
0.	049	0.12	% Impervi	ous Area						
_				_						
Tc	Length	Slope	Velocity	Capacity	Description					
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
11.2	50	0.0300	0.07		Sheet Flow, Tc-1					
					Woods: Light underbrush n= 0.400 P2= 2.80"					
17.7	694	0.0170	0.65		Shallow Concentrated Flow, Tc-2					
					Woodland Kv= 5.0 fps					
4.2	280	0.0500	1.12		Shallow Concentrated Flow, Tc-3					
					Woodland Kv= 5.0 fps					
33.1	1,024	Total								

Summary for Subcatchment PDA-2:

Runoff	=	0.03 cfs @	15.44 hrs.	Volume=	0.020 af, Depth> 0.09"

_	Area	(ac) C	N Des	cription		
_	2.	708 3	30 Woo	ds, Good,	HSG A	
	2.	708	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	11.2	50	0.0300	0.07		Sheet Flow, Tc-1
	6.8	392	0.0370	0.96		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps
-	18.0	442	Total			

Summary for Subcatchment PDA-3:

Runoff = 0.04 cfs @ 15.39 hrs, Volume= 0.023 af, Depth> 0.09"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-025yr Rainfall=6.18"

_	Area	(ac) C	N Des	cription		
	3.	078 3	30 Woo	ds, Good,	HSG A	
-	3.	078	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	10.0	50	0.0400	0.08		Sheet Flow, Tc-1
	1.7	81	0.0250	0.79		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps
	0.8	63	0.0630	1.25		Shallow Concentrated Flow, Tc-3
	0.8	96	0.1560	1.97		Woodland Kv= 5.0 fps Shallow Concentrated Flow, Tc-4 Woodland Kv= 5.0 fps
	12.2	200	Total			

13.3 290 Total

Summary for Subcatchment PDA-4A:

Runoff	=	0.06 cfs @	15.07 hrs,	Volume=	0.037 af, Depth> 0.12"
--------	---	------------	------------	---------	------------------------

Area	(ac) C	N Des	cription		
-			ds, Good,		
0.	<u>239</u> 3	<u>89 >759</u>	<u>% Grass co</u>	over, Good	, HSG A
3.	613 3	31 Wei	ghted Aver	age	
3.	613	100.	00% Pervi	ous Area	
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
11.2	50	0.0300	0.07		Sheet Flow, Tc-1
					Woods: Light underbrush n= 0.400 P2= 2.80"
1.6	99	0.0400	1.00		Shallow Concentrated Flow, Tc-2
					Woodland Kv= 5.0 fps
2.7	218	0.0730	1.35		Shallow Concentrated Flow, Tc-3
					Woodland Kv= 5.0 fps
15.6	367	Total			

Type III 24-hr Plymouth-025yr Rainfall=6.18"Printed 11/16/2021re Solutions LLCPage 25

Summary for Subcatchment PDA-4B:

Runoff = 1.00 cfs @ 12.43 hrs, Volume= 0.168 af, Depth> 0.80"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-025yr Rainfall=6.18"

Area	(ac) C	N Des	cription		
1.	357 3	30 Woo	ods, Good,	HSG A	
0.	756	39 >75°	% Grass c	over, Good	, HSG A
0.	404	98 Pave	ed parking	, HSG A	
2.	517 4	44 Wei	ghted Aver	rage	
2.	113	83.9	5% Pervio	us Area	
0.	404	16.0	5% Imperv	/ious Area	
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
15.2	50	0.0140	0.05		Sheet Flow, Tc-1
					Woods: Light underbrush n= 0.400 P2= 2.80"
4.8	253	0.0310	0.88		Shallow Concentrated Flow, Tc-2
					Woodland Kv= 5.0 fps
0.7	61	0.0740	1.36		Shallow Concentrated Flow, Tc-3
					Woodland Kv= 5.0 fps
0.2	60	0.1250	5.30		Shallow Concentrated Flow, Tc-4
					Grassed Waterway Kv= 15.0 fps
20.9	424	Total			

Summary for Subcatchment PDA-5:

Runoff	=	0.04 cfs @	15.40 hrs.	Volume=	0.025 af.	Depth>	0.09"
runon		0.04 013 @	10.401113,	V Olume=	0.020 al,	Depuis	0.00

Area	(ac) C	N Desc	cription		
3	.277 3	30 Woo	ds, Good,	HSG A	
3	.277	100.	00% Pervi	ous Area	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
11.2	50	0.0300	0.07		Sheet Flow, Tc-1
2.0	70	0.0140	0.59		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps
1.7	183	0.1260	1.77		Shallow Concentrated Flow, Tc-3 Woodland Kv= 5.0 fps
14.9	303	Total			

Summary for Subcatchment PDA-6:

Runoff = 0.13 cfs @ 15.57 hrs, Volume= 0.085 af, Depth> 0.09"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-025yr Rainfall=6.18"

Area	(ac) C	N Desc	cription		
11.	.280 3	0 Woo	ds, Good,	HSG A	
0.	.068 3	9 > 759	% Grass co	over, Good	, HSG A
11.	.348 3		ghted Aver		
11.	.348	100.	00% Pervi	ous Area	
т.	1	01	\/_l!t	O	Description
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
11.2	50	0.0300	0.07		Sheet Flow, Tc-1
					Woods: Light underbrush n= 0.400 P2= 2.80"
7.1	339	0.0250	0.79		Shallow Concentrated Flow, Tc-2
					Woodland Kv= 5.0 fps
3.2	217	0.0510	1.13		Shallow Concentrated Flow, Tc-3
					Woodland Kv= 5.0 fps
3.6	176	0.0260	0.81		Shallow Concentrated Flow, Tc-4
					Woodland Kv= 5.0 fps
25.1	782	Total			

Summary for Subcatchment PDA-7:

Runoff = 0.03 cfs @ 15.14 hrs, Volume= 0.021 af, Depth> 0.12"

Area (a	ic) C	N Desc	cription			
1.99	97 3	0 Woo	oods, Good, HSG A			
30.0	87 3	9 >75%	% Grass co	over, Good	, HSG A	
0.01	16 6	1 >75%	% Grass co	over, Good	, HSG B	
0.00	04 9	8 Roof	s, HSG A			
2.10	04 3	1 Weig	ghted Aver	age		
2.10	00	99.8	1% Pervio	us Area		
0.00	04	0.19	% Impervi	ous Area		
Tc L (min)	_ength (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
11.2	50	0.0300	0.07		Sheet Flow, Tc-1	
7.6	332	0.0210	0.72		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps	
18.8	382	Total				

Summary for Reach DP-1:

Inflow Are	a =	42.430 ac,	0.12% Impervious, Inflow D	Depth > 0.38"	for Plymouth-025yr event
Inflow	=	3.85 cfs @	12.80 hrs, Volume=	1.350 af	
Outflow	=	3.85 cfs @	12.80 hrs, Volume=	1.350 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-2:

Inflow Area	=	2.708 ac,	0.00% Impervious, Inflow	Depth > 0.09"	for Plymouth-025yr event
Inflow =	=	0.03 cfs @	15.44 hrs, Volume=	0.020 af	
Outflow =	=	0.03 cfs @	15.44 hrs, Volume=	0.020 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-3:

Inflow Area	a =	3.078 ac,	0.00% Impervious, Inflo	w Depth > 0.09"	for Plymouth-025yr event
Inflow	=	0.04 cfs @	15.39 hrs, Volume=	0.023 af	
Outflow	=	0.04 cfs @	15.39 hrs, Volume=	0.023 af, Att	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-4:

Inflow Are	a =	6.130 ac,	6.59% Impervious, Inflow D	Depth > 0.07"	for Plymouth-025yr event
Inflow	=	0.06 cfs @	15.07 hrs, Volume=	0.037 af	
Outflow	=	0.06 cfs @	15.07 hrs, Volume=	0.037 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-5:

Inflow Are	a =	3.277 ac,	0.00% Impervious, Inflow De	epth > 0.09"	for Plymouth-025yr event
Inflow	=	0.04 cfs @	15.40 hrs, Volume=	0.025 af	
Outflow	=	0.04 cfs @	15.40 hrs, Volume=	0.025 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-6:

Inflow Area =	11.348 ac,	0.00% Impervious, Inflow Dept	th > 0.09" for Plymouth-025yr event
Inflow =	0.13 cfs @	15.57 hrs, Volume= 0.	.085 af
Outflow =	0.13 cfs @	15.57 hrs, Volume= 0.	.085 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-7:

Inflow Are	a =	2.104 ac,	0.19% Impervious, Inflow De	epth > 0.12"	for Plymouth-025yr event
Inflow	=	0.03 cfs @	15.14 hrs, Volume=	0.021 af	
Outflow	=	0.03 cfs @	15.14 hrs, Volume=	0.021 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Pond 1: Modified Depression

Inflow Area =	2.517 ac, 16.05% Impervious, Inflow	Depth > 0.80" for Plymouth-025yr event
Inflow =	1.00 cfs @ 12.43 hrs, Volume=	0.168 af
Outflow =	0.15 cfs @ 16.02 hrs, Volume=	0.135 af, Atten= 84%, Lag= 214.9 min
Discarded =	0.15 cfs @ 16.02 hrs, Volume=	0.135 af
Primary =	0.00 cfs @ 0.00 hrs, Volume=	0.000 af
Secondary =	0.00 cfs $\overline{@}$ 0.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 23.58' @ 16.02 hrs Surf.Area= 2,778 sf Storage= 2,925 cf

Plug-Flow detention time= 231.7 min calculated for 0.135 af (81% of inflow) Center-of-Mass det. time= 151.1 min (1,079.6 - 928.5)

Volume	Invert	Avail.Sto	rage Storage	Description	
#1	22.00'	13,98	35 cf Custom	n Stage Data (Pr	ismatic) Listed below (Recalc)
Elevatio (fee		ırf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
22.0 23.0 24.0 25.0 26.0)0)0)0)0	915 2,091 3,267 4,879 6,581	0 1,503 2,679 4,073 5,730	0 1,503 4,182 8,255 13,985	
Device	Routing	Invert	Outlet Device	es	
#1 #2 #3	Discarded Primary Secondary	22.00' 24.20' 25.00'	12.0" Round L= 19.0' CP Inlet / Outlet I n= 0.013 Col 20.0' long x Head (feet) (P, projecting, no Invert= 24.20' / 2 rrugated PE, sm	headwall, Ke= 0.900 4.00' S= 0.0105 '/' Cc= 0.900 ooth interior, Flow Area= 0.79 sf oad-Crested Rectangular Weir 0.80 1.00

Discarded OutFlow Max=0.15 cfs @ 16.02 hrs HW=23.58' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.15 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=22.00' (Free Discharge) ←2=Culvert (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=22.00' (Free Discharge) —3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

1833109HC005A	Type III 24-hr Plymouth-050yr Rainfall=7.31"
Prepared by Beals and Thomas, Inc.	Printed 11/16/2021
HydroCAD® 10.10-5a s/n 04493 © 2020 HydroCAD Softwar	e Solutions LLC Page 30

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment PDA-1:	Runoff Area=42.430 ac 0.12% Impervious Runoff Depth>0.72" Flow Length=1,024' Tc=33.1 min CN=37 Runoff=10.76 cfs 2.538 af
Subcatchment PDA-2:	Runoff Area=2.708 ac 0.00% Impervious Runoff Depth>0.27" Flow Length=442' Tc=18.0 min CN=30 Runoff=0.10 cfs 0.060 af
Subcatchment PDA-3:	Runoff Area=3.078 ac 0.00% Impervious Runoff Depth>0.27" Flow Length=290' Tc=13.3 min CN=30 Runoff=0.12 cfs 0.068 af
Subcatchment PDA-4A:	Runoff Area=3.613 ac 0.00% Impervious Runoff Depth>0.32" Flow Length=367' Tc=15.6 min CN=31 Runoff=0.22 cfs 0.097 af
Subcatchment PDA-4B:	Runoff Area=2.517 ac 16.05% Impervious Runoff Depth>1.29" Flow Length=424' Tc=20.9 min CN=44 Runoff=1.93 cfs 0.270 af
Subcatchment PDA-5:	Runoff Area=3.277 ac 0.00% Impervious Runoff Depth>0.27" Flow Length=303' Tc=14.9 min CN=30 Runoff=0.12 cfs 0.073 af
Subcatchment PDA-6:	Runoff Area=11.348 ac 0.00% Impervious Runoff Depth>0.26" Flow Length=782' Tc=25.1 min CN=30 Runoff=0.43 cfs 0.250 af
Subcatchment PDA-7:	Runoff Area=2.104 ac 0.19% Impervious Runoff Depth>0.32" Flow Length=382' Tc=18.8 min CN=31 Runoff=0.12 cfs 0.056 af
Reach DP-1:	Inflow=10.76 cfs 2.538 af Outflow=10.76 cfs 2.538 af
Reach DP-2:	Inflow=0.10 cfs 0.060 af Outflow=0.10 cfs 0.060 af
Reach DP-3:	Inflow=0.12 cfs 0.068 af Outflow=0.12 cfs 0.068 af
Reach DP-4:	Inflow=0.22 cfs 0.107 af Outflow=0.22 cfs 0.107 af
Reach DP-5:	Inflow=0.12 cfs 0.073 af Outflow=0.12 cfs 0.073 af
Reach DP-6:	Inflow=0.43 cfs 0.250 af Outflow=0.43 cfs 0.250 af
Reach DP-7:	Inflow=0.12 cfs 0.056 af Outflow=0.12 cfs 0.056 af

Pond 1: Modified DepressionPeak Elev=24.33' Storage=5,332 cfInflow=1.93 cfs0.270 afDiscarded=0.21 cfs0.186 afPrimary=0.06 cfs0.010 afSecondary=0.00 cfs0.000 afOutflow=0.27 cfs0.196 af

Total Runoff Area = 71.075 acRunoff Volume = 3.413 afAverage Runoff Depth = 0.58"99.36% Pervious = 70.618 ac0.64% Impervious = 0.457 ac

Summary for Subcatchment PDA-1:

Runoff = 10.76 cfs @ 12.68 hrs, Volume= 2.538 af, Depth> 0.72"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-050yr Rainfall=7.31"

Area	(ac) (CN [Desc	ription		
32.	525	30 \	Noo	ds, Good,	HSG A	
2.	936	55 \	Noo	ds, Good,	HSG B	
0.	998	77 \	Noo	ds, Good,	HSG D	
1.	793	39 >	>75%	6 Grass co	over, Good	, HSG A
3.	716	61 >	>75%	6 Grass co	over, Good	, HSG B
0.	413	96 (Grav	el surface	, HSG B	
0.	049	98 F	Roof	s, HSG B		
42.	430	37 \	Neig	hted Aver	age	
42.	381	ç	99.8	3% Pervio	us Area	
0.	049	().12º	% Impervi	ous Area	
Tc	Length	i Slo	pe	Velocity	Capacity	Description
(min)	(feet)) (ft	t/ft)	(ft/sec)	(cfs)	
11.2	50	0.03	300	0.07		Sheet Flow, Tc-1
						Woods: Light underbrush n= 0.400 P2= 2.80"
17.7	694	0.01	170	0.65		Shallow Concentrated Flow, Tc-2
						Woodland Kv= 5.0 fps
4.2	280	0.05	500	1.12		Shallow Concentrated Flow, Tc-3
						Woodland Kv= 5.0 fps
33.1	1,024	- Tota	al			

Summary for Subcatchment PDA-2:

						_	
Runoff	=	0.10 cfs @	13.78 hrs.	Volume=	0.060 af,	Depth>	0.27"

_	Area	(ac) C	N Des	cription		
_	2.	708 3	30 Woo	ds, Good,	HSG A	
	2.	708	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	11.2	50	0.0300	0.07		Sheet Flow, Tc-1
	6.8	392	0.0370	0.96		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps
-	18.0	442	Total			

Summary for Subcatchment PDA-3:

Runoff = 0.12 cfs @ 13.71 hrs, Volume= 0.068 af, Depth> 0.27"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-050yr Rainfall=7.31"

_	Area	(ac) C	N Dese	cription		
-	3.	078 3	30 Woo	ods, Good,	HSG A	
-	3.	078	100.	00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	10.0	50	0.0400	0.08		Sheet Flow, Tc-1
	1.7	81	0.0250	0.79		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps
	0.8	63	0.0630	1.25		Shallow Concentrated Flow, Tc-3
	0.8	96	0.1560	1.97		Woodland Kv= 5.0 fps Shallow Concentrated Flow, Tc-4 Woodland Kv= 5.0 fps
	12.2	200	Total			

13.3 290 Total

Summary for Subcatchment PDA-4A:

Runoff	=	0.22 cfs @	12.61 hrs,	Volume=	0.097 af, De	pth> 0.32"
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Area	(ac) C	N Des	cription		
-			ds, Good,		
0.	<u>239</u> 3	<u>89</u> >759	<u>% Grass co</u>	over, Good	, HSG A
3.	613 3	31 Wei	ghted Aver	age	
3.	613	100.	00% Pervi	ous Area	
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
11.2	50	0.0300	0.07		Sheet Flow, Tc-1
					Woods: Light underbrush n= 0.400 P2= 2.80"
1.6	99	0.0400	1.00		Shallow Concentrated Flow, Tc-2
					Woodland Kv= 5.0 fps
2.7	218	0.0730	1.35		Shallow Concentrated Flow, Tc-3
					Woodland Kv= 5.0 fps
15.6	367	Total			

Summary for Subcatchment PDA-4B:

1.93 cfs @ 12.37 hrs, Volume= Runoff = 0.270 af, Depth> 1.29"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-050yr Rainfall=7.31"

Area	(ac) C	N Dese	cription				
1.	357 3	30 Woo	ds, Good,	HSG A			
0.	756 3	39 >759	% Grass co	over, Good	, HSG A		
0.	0.404 98 Paved parking, HSG A						
2.	517 4	4 Weig	ghted Aver	age			
2.	113	83.9	5% Pervio	us Area			
0.	404	16.0	5% Imperv	vious Area			
			•				
Tc	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·		
15.2	50	0.0140	0.05		Sheet Flow, Tc-1		
					Woods: Light underbrush n= 0.400 P2= 2.80"		
4.8	253	0.0310	0.88		Shallow Concentrated Flow, Tc-2		
					Woodland Kv= 5.0 fps		
0.7	61	0.0740	1.36		Shallow Concentrated Flow, Tc-3		
					Woodland Kv= 5.0 fps		
0.2	60	0.1250	5.30		Shallow Concentrated Flow, Tc-4		
					Grassed Waterway Kv= 15.0 fps		
20.9	424	Total					

Summary for Subcatchment PDA-5:

Runoff	=	0.12 cfs @	13.73 hrs.	Volume=	0.073 af.	Depth> 0.27"
runon		0.12 010 @	10.701110,	Volumo	0.070 ul,	

 Area	(ac) C	N Dese	cription		
3.	277 3	30 Woo	ds, Good,	HSG A	
3.	277	100.	00% Pervi	ous Area	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
 11.2	50	0.0300	0.07		Sheet Flow, Tc-1
2.0	70	0.0140	0.59		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps
1.7	183	0.1260	1.77		Shallow Concentrated Flow, Tc-3 Woodland Kv= 5.0 fps
14.9	303	Total			

Summary for Subcatchment PDA-6:

Runoff = 0.43 cfs @ 13.86 hrs, Volume= 0.250 af, Depth> 0.26"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-050yr Rainfall=7.31"

Area	(ac) C	N Desc	cription					
11.	.280 3	80 Woo	ds, Good,	HSG A				
0.	0.068 39 >75% Grass cover, Good, HSG A							
11.	11.348 30 Weighted Average							
11.	11.348 100.00% Pervious Area							
-		01		0				
Tc	Length	Slope	Velocity	Capacity	Description			
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)				
11.2	50	0.0300	0.07		Sheet Flow, Tc-1			
					Woods: Light underbrush n= 0.400 P2= 2.80"			
7.1	339	0.0250	0.79		Shallow Concentrated Flow, Tc-2			
					Woodland Kv= 5.0 fps			
3.2	217	0.0510	1.13		Shallow Concentrated Flow, Tc-3			
					Woodland Kv= 5.0 fps			
3.6	176	0.0260	0.81		Shallow Concentrated Flow, Tc-4			
					Woodland Kv= 5.0 fps			
25.1	782	Total						

Summary for Subcatchment PDA-7:

Runoff = 0.12 cfs @ 12.67 hrs, Volume= 0.056 af, Depth> 0.32"

Area (a	ac) C	N Desc	cription							
1.9	97 3	0 Woo	pods, Good, HSG A							
0.0	87 3	9 > 759	% Grass co	over, Good	, HSG A					
0.0	16 6	51 >759	% Grass co	over, Good	, HSG B					
0.0	04 9	8 Root	s, HSG A							
2.1	04 3	1 Weig	ghted Aver	age						
2.1	00	99.8	1% Pervio	us Area						
0.0	04	0.19	% Impervi	ous Area						
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description					
11.2	50	0.0300	0.07		Sheet Flow, Tc-1					
7.6	332	0.0210	0.72		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps					
18.8	382	Total								

Summary for Reach DP-1:

Inflow Are	a =	42.430 ac,	0.12% Impervious, Inflow E	Depth > 0.72"	for Plymouth-050yr event
Inflow	=	10.76 cfs @	12.68 hrs, Volume=	2.538 af	
Outflow	=	10.76 cfs @	12.68 hrs, Volume=	2.538 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-2:

Inflow Area	a =	2.708 ac,	0.00% Impervious, Inflow D	epth > 0.27"	for Plymouth-050yr event
Inflow	=	0.10 cfs @	13.78 hrs, Volume=	0.060 af	
Outflow	=	0.10 cfs @	13.78 hrs, Volume=	0.060 af, Att	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-3:

Inflow Area	a =	3.078 ac,	0.00% Impervious, Inflow De	epth > 0.27" for Plymouth-050yr event
Inflow	=	0.12 cfs @	13.71 hrs, Volume=	0.068 af
Outflow	=	0.12 cfs @	13.71 hrs, Volume=	0.068 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-4:

Inflow Are	a =	6.130 ac,	6.59% Impervious, Infle	Depth > 0.21"	for Plymouth-050yr event
Inflow	=	0.22 cfs @	12.61 hrs, Volume=	0.107 af	
Outflow	=	0.22 cfs @	12.61 hrs, Volume=	0.107 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-5:

Inflow Area	a =	3.277 ac,	0.00% Impervious, Inflow D	epth > 0.27"	for Plymouth-050yr event
Inflow	=	0.12 cfs @	13.73 hrs, Volume=	0.073 af	
Outflow	=	0.12 cfs @	13.73 hrs, Volume=	0.073 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-6:

Inflow Area =	11.348 ac,	0.00% Impervious, Inflow Dep	oth > 0.26"	for Plymouth-050yr event
Inflow =	0.43 cfs @	13.86 hrs, Volume=).250 af	
Outflow =	0.43 cfs @	13.86 hrs, Volume= (.250 af, Atter	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-7:

Inflow Are	a =	2.104 ac,	0.19% Impervious, Inflow [Depth > 0.32"	for Plymouth-050yr event
Inflow	=	0.12 cfs @	12.67 hrs, Volume=	0.056 af	
Outflow	=	0.12 cfs @	12.67 hrs, Volume=	0.056 af, Att	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Pond 1: Modified Depression

Inflow Area =	2.517 ac, 16.05% Impervious, Inflow	Depth > 1.29" for Plymouth-050yr event
Inflow =	1.93 cfs @ 12.37 hrs, Volume=	0.270 af
Outflow =	0.27 cfs @ 15.48 hrs, Volume=	0.196 af, Atten= 86%, Lag= 186.5 min
Discarded =	0.21 cfs @ 15.48 hrs, Volume=	0.186 af
Primary =	0.06 cfs @ 15.48 hrs, Volume=	0.010 af
Secondary =	0.00 cfs $\overline{@}$ 0.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 24.33' @ 15.48 hrs Surf.Area= 3,792 sf Storage= 5,332 cf

Plug-Flow detention time= 266.7 min calculated for 0.196 af (72% of inflow) Center-of-Mass det. time= 163.7 min (1,072.6 - 908.9)

Volume	Invert	Avail.Sto	rage Storage	Description	
#1	22.00'	13,98	35 cf Custom	n Stage Data (Pr	ismatic) Listed below (Recalc)
Elevatio (fee		ırf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
22.0 23.0 24.0 25.0 26.0)0)0)0)0	915 2,091 3,267 4,879 6,581	0 1,503 2,679 4,073 5,730	0 1,503 4,182 8,255 13,985	
Device	Routing	Invert	Outlet Device	es	
#1 #2 #3	Discarded Primary Secondary	22.00' 24.20' 25.00'	12.0" Round L= 19.0' CP Inlet / Outlet I n= 0.013 Col 20.0' long x Head (feet) (P, projecting, no Invert= 24.20' / 2 rrugated PE, sm	headwall, Ke= 0.900 4.00' S= 0.0105 '/' Cc= 0.900 ooth interior, Flow Area= 0.79 sf oad-Crested Rectangular Weir 0.80 1.00

Discarded OutFlow Max=0.21 cfs @ 15.48 hrs HW=24.33' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.21 cfs)

Primary OutFlow Max=0.05 cfs @ 15.48 hrs HW=24.33' (Free Discharge) ←2=Culvert (Inlet Controls 0.05 cfs @ 0.95 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=22.00' (Free Discharge) —3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

1833109HC005A	Type III 24-hr Plymouth-100yr Rainfall=8.65"
Prepared by Beals and Thomas, Inc.	Printed 11/16/2021
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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment PDA-1:	Runoff Area=42.430 ac 0.12% Impervious Runoff Depth>1.22" Flow Length=1,024' Tc=33.1 min CN=37 Runoff=23.07 cfs 4.312 af
Subcatchment PDA-2:	Runoff Area=2.708 ac 0.00% Impervious Runoff Depth>0.58" Flow Length=442' Tc=18.0 min CN=30 Runoff=0.49 cfs 0.130 af
Subcatchment PDA-3:	Runoff Area=3.078 ac 0.00% Impervious Runoff Depth>0.58" Flow Length=290' Tc=13.3 min CN=30 Runoff=0.60 cfs 0.148 af
Subcatchment PDA-4A:	Runoff Area=3.613 ac 0.00% Impervious Runoff Depth>0.66" Flow Length=367' Tc=15.6 min CN=31 Runoff=0.88 cfs 0.199 af
Subcatchment PDA-4B:	Runoff Area=2.517 ac 16.05% Impervious Runoff Depth>1.97" Flow Length=424' Tc=20.9 min CN=44 Runoff=3.28 cfs 0.413 af
Subcatchment PDA-5:	Runoff Area=3.277 ac 0.00% Impervious Runoff Depth>0.58" Flow Length=303' Tc=14.9 min CN=30 Runoff=0.62 cfs 0.157 af
Subcatchment PDA-6:	Runoff Area=11.348 ac 0.00% Impervious Runoff Depth>0.57" Flow Length=782' Tc=25.1 min CN=30 Runoff=1.84 cfs 0.542 af
Subcatchment PDA-7:	Runoff Area=2.104 ac 0.19% Impervious Runoff Depth>0.66" Flow Length=382' Tc=18.8 min CN=31 Runoff=0.49 cfs 0.116 af
Reach DP-1:	Inflow=23.07 cfs 4.312 af Outflow=23.07 cfs 4.312 af
Reach DP-2:	Inflow=0.49 cfs 0.130 af Outflow=0.49 cfs 0.130 af
Reach DP-3:	Inflow=0.60 cfs 0.148 af Outflow=0.60 cfs 0.148 af
Reach DP-4:	Inflow=0.96 cfs 0.315 af Outflow=0.96 cfs 0.315 af
Reach DP-5:	Inflow=0.62 cfs 0.157 af Outflow=0.62 cfs 0.157 af
Reach DP-6:	Inflow=1.84 cfs 0.542 af Outflow=1.84 cfs 0.542 af
Reach DP-7:	Inflow=0.49 cfs 0.116 af Outflow=0.49 cfs 0.116 af

Pond 1: Modified DepressionPeak Elev=24.62' Storage=6,529 cfInflow=3.28 cfs0.413 afDiscarded=0.24 cfs0.205 afPrimary=0.55 cfs0.115 afSecondary=0.00 cfs0.000 afOutflow=0.79 cfs0.320 af

Total Runoff Area = 71.075 acRunoff Volume = 6.018 afAverage Runoff Depth = 1.02"99.36% Pervious = 70.618 ac0.64% Impervious = 0.457 ac

Summary for Subcatchment PDA-1:

Runoff = 23.07 cfs @ 12.60 hrs, Volume= 4.312 af, Depth> 1.22"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-100yr Rainfall=8.65"

Area	(ac) (CN Des	cription		
32.	525	30 Wo	ods, Good,	HSG A	
2.	936	55 Wo	ods, Good,	HSG B	
0.	998	77 Wo	ods, Good,	HSG D	
1.	793	39 >75	% Grass c	over, Good	, HSG A
3.	716	61 >75	% Grass c	over, Good	, HSG B
0.	413	96 Gra	vel surface	e, HSG B	
0.	049	<u>98 Roc</u>	fs, HSG B		
42.	430	37 We	ghted Avei	rage	
42.	381	99.8	88% Pervio	us Area	
0.	049	0.12	2% Impervi	ous Area	
Тс	Length		Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
11.2	50	0.0300	0.07		Sheet Flow, Tc-1
					Woods: Light underbrush n= 0.400 P2= 2.80"
17.7	694	0.0170	0.65		Shallow Concentrated Flow, Tc-2
					Woodland Kv= 5.0 fps
4.2	280	0.0500	1.12		Shallow Concentrated Flow, Tc-3
					Woodland Kv= 5.0 fps
33.1	1,024	Total			

Summary for Subcatchment PDA-2:

Runoff = 0.49 cfs @ 12.55 hrs, Volume= 0.130 af, De	Depth> 0.58"
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_	Area	(ac) C	N Dese	cription		
	2.708 30 Woods, Good, HSG A				HSG A	
	2.708 100.00% Pervious Area			00% Pervi	ous Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	11.2	50	0.0300	0.07		Sheet Flow, Tc-1
	6.8	392	0.0370	0.96		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps
-	18.0	442	Total			

Summary for Subcatchment PDA-3:

Runoff = 0.60 cfs @ 12.48 hrs, Volume= 0.148 af, Depth> 0.58"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-100yr Rainfall=8.65"

_	Area	(ac) C	N Dese	cription		
_	3.078 30 Woods, Good, HSG A				HSG A	
-	3.078 100.00% Pervious Area					
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	10.0	50	0.0400	0.08		Sheet Flow, Tc-1
	1.7	81	0.0250	0.79		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps
	0.8	63	0.0630	1.25		Shallow Concentrated Flow, Tc-3
	0.8	96	0.1560	1.97		Woodland Kv= 5.0 fps Shallow Concentrated Flow, Tc-4
_	0.0	90	0.1500	1.97		Woodland Kv= 5.0 fps
	12 2	200	Total			

13.3 290 Total

Summary for Subcatchment PDA-4A:

Runoff	=	0.88 cfs @	12.49 hrs,	Volume=	0.199 af, Depth> 0.66"
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Area	(ac) C	N Dese	cription		
3.374 30 Woods, Good, HSG A		HSG A			
0.239 39 >75% Grass cover, Good, HSG A					, HSG A
3.613 31 Weighted Average					
3.613 100.00% Pervious Area					
Tc	Length	Slope	Velocity	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
11.2	50	0.0300	0.07		Sheet Flow, Tc-1
					Woods: Light underbrush n= 0.400 P2= 2.80"
1.6	99	0.0400	1.00		Shallow Concentrated Flow, Tc-2
					Woodland Kv= 5.0 fps
2.7	218	0.0730	1.35		Shallow Concentrated Flow, Tc-3
					Woodland Kv= 5.0 fps
15.6	367	Total			

Summary for Subcatchment PDA-4B:

Runoff = 3.28 cfs @ 12.34 hrs, Volume= 0.413 af, Depth> 1.97"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-100yr Rainfall=8.65"

Area	(ac) C	N Dese	cription		
1.	357 3	30 Woo	ds, Good,	HSG A	
0.	756 3	39 >759	% Grass co	over, Good	, HSG A
0.	404 9	8 Pave	ed parking	, HSG A	
2.	517 4	4 Wei	phted Aver	age	
2.	113	•	5% Pervio	0	
0.	404	16.0	5% Imper	ious Area	
			•		
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
15.2	50	0.0140	0.05		Sheet Flow, Tc-1
					Woods: Light underbrush n= 0.400 P2= 2.80"
4.8	253	0.0310	0.88		Shallow Concentrated Flow, Tc-2
					Woodland Kv= 5.0 fps
0.7	61	0.0740	1.36		Shallow Concentrated Flow, Tc-3
					Woodland Kv= 5.0 fps
0.2	60	0.1250	5.30		Shallow Concentrated Flow, Tc-4
					Grassed Waterway Kv= 15.0 fps
20.9	424	Total			

Summary for Subcatchment PDA-5:

Runoff	=	0.62 cfs @	12.50 hrs, Volume=	0.157 af, Depth> 0.58"
1 turion		0.02 010 @	12.00 110, 1000110	

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-100yr Rainfall=8.65"

 Area	(ac) C	N Dese	cription		
3.	277 3	30 Woo	ds, Good,	HSG A	
3.	277	100.	00% Pervi	ous Area	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
 11.2	50	0.0300	0.07		Sheet Flow, Tc-1
2.0	70	0.0140	0.59		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps
1.7	183	0.1260	1.77		Shallow Concentrated Flow, Tc-3 Woodland Kv= 5.0 fps
14.9	303	Total			

Summary for Subcatchment PDA-6:

Runoff = 1.84 cfs @ 12.65 hrs, Volume= 0.542 af, Depth> 0.57"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-100yr Rainfall=8.65"

Area	(ac) C	N Desc	cription		
11.	.280 3	80 Woo	ds, Good,	HSG A	
0.	.068 3	89 > 759	% Grass co	over, Good	, HSG A
11.	.348 3		ghted Aver		
11.	.348	100.	00% Pervi	ous Area	
-		01		0	
Tc	Length	Slope	Velocity	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
11.2	50	0.0300	0.07		Sheet Flow, Tc-1
					Woods: Light underbrush n= 0.400 P2= 2.80"
7.1	339	0.0250	0.79		Shallow Concentrated Flow, Tc-2
					Woodland Kv= 5.0 fps
3.2	217	0.0510	1.13		Shallow Concentrated Flow, Tc-3
					Woodland Kv= 5.0 fps
3.6	176	0.0260	0.81		Shallow Concentrated Flow, Tc-4
					Woodland Kv= 5.0 fps
25.1	782	Total			

Summary for Subcatchment PDA-7:

Runoff = 0.49 cfs @ 12.53 hrs, Volume= 0.116 af, Depth> 0.66"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr Plymouth-100yr Rainfall=8.65"

Area (ac) C	N Dese	cription		
1.9	997 3	30 Woo	ds, Good,	HSG A	
0.0)87 3	39 >759	% Grass co	over, Good	, HSG A
0.0	016 6	61 >759	% Grass co	over, Good	, HSG B
0.0	004 9	8 Root	fs, HSG A		
2.1	104 3	31 Weig	ghted Aver	age	
2.1	100	99.8	1% Pervio	us Area	
0.0)04	0.19	% Impervi	ous Area	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
11.2	50	0.0300	0.07		Sheet Flow, Tc-1
7.6	332	0.0210	0.72		Woods: Light underbrush n= 0.400 P2= 2.80" Shallow Concentrated Flow, Tc-2 Woodland Kv= 5.0 fps
18.8	382	Total			

Summary for Reach DP-1:

Inflow Are	a =	42.430 ac,	0.12% Impervious, Infle	ow Depth > 1.22"	for Plymouth-100yr event
Inflow	=	23.07 cfs @	12.60 hrs, Volume=	4.312 af	
Outflow	=	23.07 cfs @	12.60 hrs, Volume=	4.312 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-2:

Inflow Area =	2.708 ac,	0.00% Impervious, Inflow	Depth > 0.58"	for Plymouth-100yr event
Inflow =	0.49 cfs @	12.55 hrs, Volume=	0.130 af	
Outflow =	0.49 cfs @	12.55 hrs, Volume=	0.130 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-3:

Inflow Area	a =	3.078 ac,	0.00% Impervious, Inflo	w Depth > 0.58"	for Plymouth-100yr event
Inflow	=	0.60 cfs @	12.48 hrs, Volume=	0.148 af	
Outflow	=	0.60 cfs @	12.48 hrs, Volume=	0.148 af, Att	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-4:

Inflow Are	a =	6.130 ac,	6.59% Impervious, Inflow I	Depth > 0.62"	for Plymouth-100yr event
Inflow	=	0.96 cfs @	13.05 hrs, Volume=	0.315 af	
Outflow	=	0.96 cfs @	13.05 hrs, Volume=	0.315 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-5:

Inflow Are	a =	3.277 ac,	0.00% Impervious, Inflow D	epth > 0.58"	for Plymouth-100yr event
Inflow	=	0.62 cfs @	12.50 hrs, Volume=	0.157 af	
Outflow	=	0.62 cfs @	12.50 hrs, Volume=	0.157 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-6:

Inflow Area =	11.348 ac,	0.00% Impervious, Inflow De	epth > 0.57"	for Plymouth-100yr event
Inflow =	1.84 cfs @	12.65 hrs, Volume=	0.542 af	
Outflow =	1.84 cfs @	12.65 hrs, Volume=	0.542 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Reach DP-7:

Inflow Are	a =	2.104 ac,	0.19% Impervious, Inflow I	Depth > 0.66"	for Plymouth-100yr event
Inflow	=	0.49 cfs @	12.53 hrs, Volume=	0.116 af	
Outflow	=	0.49 cfs @	12.53 hrs, Volume=	0.116 af, Att	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Summary for Pond 1: Modified Depression

Inflow Area =	2.517 ac, 16.05% Impervious, Inflow Depth > 1.97" for Plymouth-100yr even	t
Inflow =	3.28 cfs @ 12.34 hrs, Volume= 0.413 af	
Outflow =	0.79 cfs @ 13.20 hrs, Volume= 0.320 af, Atten= 76%, Lag= 51.2 min	
Discarded =	0.24 cfs @ 13.20 hrs, Volume= 0.205 af	
Primary =	0.55 cfs @ 13.20 hrs, Volume= 0.115 af	
Secondary =	0.00 cfs $\bar{@}$ 0.00 hrs, Volume= 0.000 af	

Routing by Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Peak Elev= 24.62' @ 13.20 hrs Surf.Area= 4,271 sf Storage= 6,529 cf

Plug-Flow detention time= 193.5 min calculated for 0.319 af (77% of inflow) Center-of-Mass det. time= 105.8 min (999.4 - 893.6)

Volume	Invert	Avail.Sto	rage Storage	Description	
#1	22.00'	13,98	35 cf Custom	n Stage Data (Pr	ismatic) Listed below (Recalc)
Elevatio (fee		rf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
22.0 23.0 24.0 25.0 26.0)0)0)0)0	915 2,091 3,267 4,879 6,581	0 1,503 2,679 4,073 5,730	0 1,503 4,182 8,255 13,985	
Device	Routing	Invert	Outlet Device		
#1 #2 #3	Discarded Primary Secondary	22.00' 24.20' 25.00'	12.0" Round L= 19.0' CPI Inlet / Outlet I n= 0.013 Coi 20.0' long x Head (feet) 0	P, projecting, no Invert= 24.20' / 2 rrugated PE, smo	headwall, Ke= 0.900 4.00' S= 0.0105 '/' Cc= 0.900 ooth interior, Flow Area= 0.79 sf oad-Crested Rectangular Weir 0.80 1.00

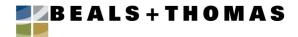
Discarded OutFlow Max=0.24 cfs @ 13.20 hrs HW=24.62' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.24 cfs)

Primary OutFlow Max=0.55 cfs @ 13.20 hrs HW=24.62' (Free Discharge) ←2=Culvert (Inlet Controls 0.55 cfs @ 1.75 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=22.00' (Free Discharge) —3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Attachment 4 Hydraulic Calculations





HYDRAULIC CALCULATIONS

OBJECTIVE

To size pipes to adequately convey flows from the proposed project and to meet the design standards of the Massachusetts DEP Stormwater Handbook for inlet capacity, pipe flow, and scour.

CONCLUSION

- The proposed pipes will adequately convey the 50-year storm event runoff rates.
- The proposed stormwater management design has been reviewed for compliance with the stormwater management standards described in the Massachusetts DEP Stormwater Management Handbook.

CALCULATION METHODS

• The pipes are designed using the Rational Formula, based on a 50-year storm event for the Town of Barnstable (see attached IDF curve).

ASSUMPTIONS

- Runoff coefficient C=0.3 for pervious areas and C=0.9 for impervious areas.
- Manning's n=0.012 for HDPE pipe.
- The times of concentration (T_c) for contributing subcatchments are approximately 19.5 minutes for flows to AD-1, and 6 minutes for flows to CB-1, CB-2, CB-3, and CB-4.
- The minimum full-flow (scour) velocity is 2 feet per second.
- The maximum full-flow (scour) velocity is 10 feet per second.

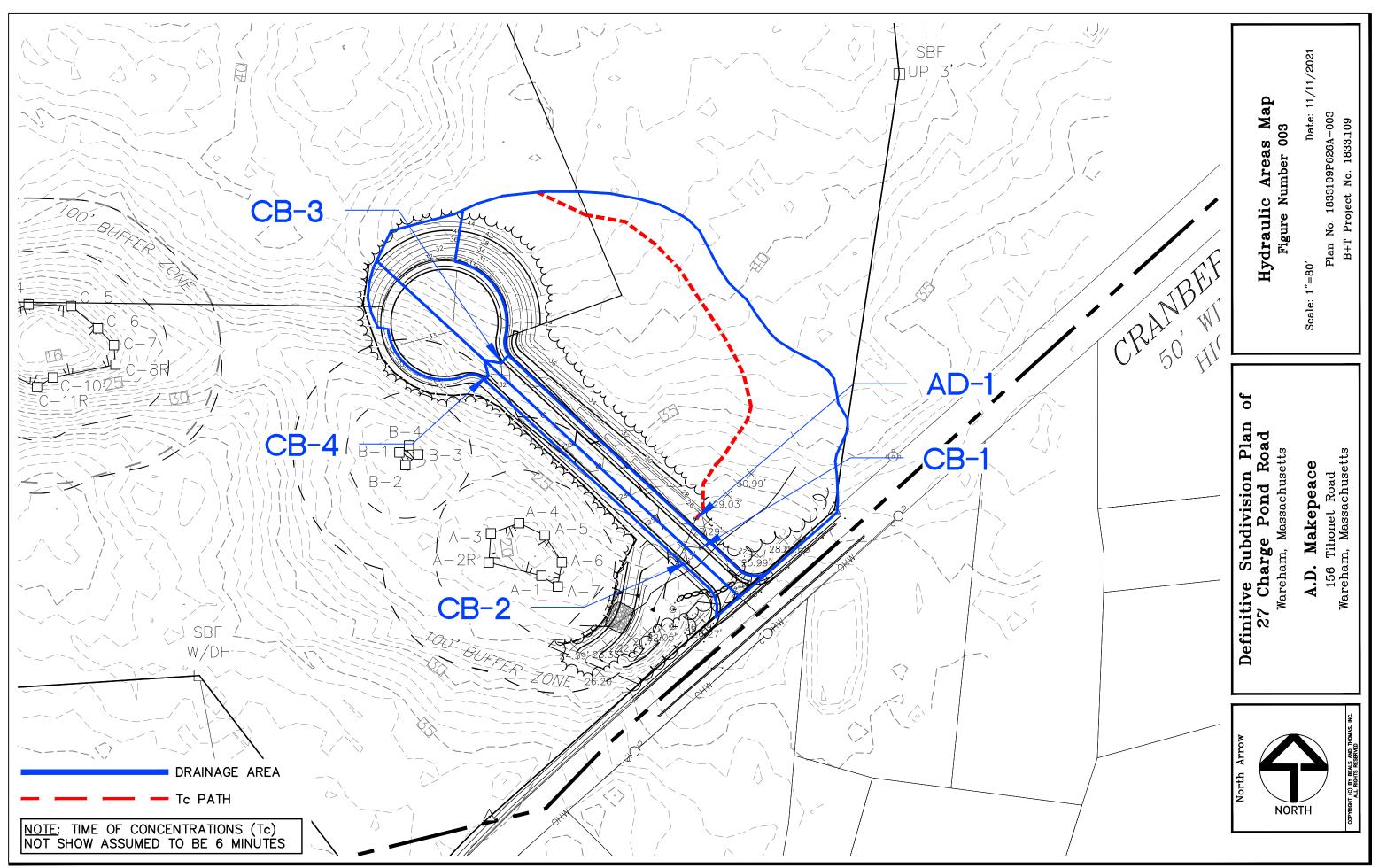
SOURCES OF DATA/ EQUATIONS

- 1. Rational Method (Q=CiA) was used to calculate peak runoff rates tributary to AD-1, CB-1, CB-2, CB-3, and CB-4.
- 2. Manning's Equation was used to determine pipe capacities.
- 3. 50-year storm intensity obtained from the Intensity/Duration rainfall curve for Barnstable, MA in S.C.S Technical Report No. 40.
- 4. Massachusetts DEP Stormwater Management Handbook, February 2008.

REV	CALC. BY	DATE	CHECKED BY	DATE	APPROVED BY	DATE
0	RFK	11/11/2021	KJP	11/12/2021	MC	11/17/2021

RFK/kjp/mc/1833109CS006A

Civil Engineering • Land Surveying • Landscape Architecture • Land Use Permitting • Environmental Planning • Wetland Science



🗾 B E A L S + T H O M A S

BEALS AND THOMAS, INC.

PAVED GRASSED PAVED GRASSED	AREA 0 1.69 AREA 0.116 0.022	C 0.9 0.3 C 0.9 0.3 C	Tc= TOTAL AREA= WEIGHTED C= DA- Tc= TOTAL AREA= WEIGHTED C=	6 1.69 0.30 CB-1 6 0.138 0.80	MIN ACRES MIN ACRES
PAVED	AREA 0.116 0.022 AREA	C 0.9 0.3	WEIGHTED C= DA- Tc= TOTAL AREA=	0.30 CB-1 6 0.138	MIN
	0.116 0.022 AREA	0.9 0.3	DA- Tc= TOTAL AREA=	CB-1 6 0.138	
	0.116 0.022 AREA	0.9 0.3	Tc= TOTAL AREA=	6 0.138	
	0.116 0.022 AREA	0.9 0.3	TOTAL AREA=	0.138	
	0.022 AREA	0.3	TOTAL AREA=	0.138	
		C	WEIGHTED C=	0.80	
		C			
		U	DA-	CB-2	
PAVED	0.079	0.9	Tc=	6	MIN
GRASSED	0.022	0.3	TOTAL AREA=	0.101	ACRES
			WEIGHTED C=	0.77	
		_	DA-	CB-3	
PAVED	AREA 0.116	C 0.9	Tc=	6	MIN
GRASSED	0.079	0.3	TOTAL AREA=	0.195	ACRES
			WEIGHTED C=	0.66	
			DA-	CB-4	
PAVED	AREA 0.095	C 0.9	Tc=	6	MIN
GRASSED	0.095	0.3	TOTAL AREA=	0.132	ACRES
			WEIGHTED C=	0.73	
			DA-	DMH-2	
PAVED	AREA 0.211	C 0.9	Tc=	6	MIN
GRASSED	0.211	0.3	TOTAL AREA=	0.327	ACRES
-			WEIGHTED C=	0.69	-
			DA-	DMH-1	
PAVED	AREA 0.406	C 0.9	Tc=	6	MIN
GRASSED	0.406 1.85	0.9 0.3	TOTAL AREA=	6 2.256	ACRES
	1.00	0.0	WEIGHTED C=	0.41	NONEO
			DA-	WQS-1	
PAVED	AREA 0.406	C 0.9	Tc=	6	MIN
GRASSED	1.85	0.3	TOTAL AREA=	2.256	ACRES
			WEIGHTED C=	0.41	
JOB NO. 1833.10)	COMPUTED BY RFK	CHECKED BY KJP		
	je Pond Road	DATE 11/11/202			



Using the Rational Method:

Q = CIA

Where:

Q = flow (cfs)

C = Runoff Coefficient

I = Rainfall Intensity, 50-year storm (in/hr) (from Barnstable, MA IDF curve, see attached A = Contributing Area (acres)

Assumptions: - Coefficient of runoff for Gravel Surfaces = 0.9

- Coefficient of runoff for Pervious Surfaces = 0.3

Inlet	Contributing Area (Acres)	Weighted Average Rational Coefficients	Rainfall Intensity for Barnstable (in/hr)	Contributing Flow (cfs)
AD-1	1.690	0.30	4.25	2.15
CB-1	0.138	0.80	6.60	0.73
CB-2	0.101	0.77	6.60	0.51
CB-3	0.195	0.66	6.60	0.85
CB-4	0.132	0.73	6.60	0.64
DHM-2	0.327	0.69	6.60	1.49
DHM-1	2.256	0.41	6.60	6.10
WQS-1	2.256	0.41	6.60	6.10

JOB NO. 1833.109	COMPUTED BY	RFK	CHECKED BY	KJP
FILE 27 Charge Pond Road	DATE	11/11/2021	DATE	11/12/2021



Using the Manning Equation to Verify Pipe Capacities Versus Pipe Flows:

$$Q = \frac{1.49}{n} A R^{\frac{2}{3}} S^{\frac{1}{2}}$$

Where:

Q = flow (cfs) n = Manning's roughness coefficient A = Cross Sectional Area (sf) R = Hydraulic Radius (ft) S = Pipe Slope

Assumptions: n = 0.012 for HDPE pipe Pipe velocity shall be between 2.0 ft/sec and 10 ft/sec

Pipe Connection	Contributing Flow-50 Year Storm(cfs)	Proposed Pipe Size and Material	Proposed Pipe Slope (rise/run)	Full-Flow Capacity of Pipe from Manning Equation (cfs)	Adequate	Full Flow Velocity (ft/sec)
AD-1 to DMH-1	2.15	12" HDPE	0.0035	2.29	ОК	6.7
CB-1 to DMH-1	0.73	12" HDPE	0.0064	3.10	OK	9.0
CB-2 to DMH-1	0.51	12" HDPE	0.0064	3.10	OK	3.9
CB-3 to DMH-2	0.85	12" HDPE	0.0050	2.74	OK	3.5
CB-4 to DHM-2	0.64	12" HDPE	0.0050	2.74	OK	3.5
DMH-2 to DMH-1	1.49	12" HDPE	0.0219	5.73	OK	7.3
DMH-1 to WQS-1	6.10	18" HDPE	0.0083	10.40	ОК	7.4
WQS-1 to FE-1	6.10	18" HDPE	0.0057	8.61	OK	6.2

JOB NO. 1833.109	COMPUTED BY	RFK	CHECKED BY	KJP
27 Charge Pond	_			
FILE Road	DATE	11/11/2021	DATE	11/12/2021



CB #	50-YEAR STORM DESIGN FLOW (CFS)	HEAD (ft) Lebaron LF248-2 (Single grate) A= 1.5625 SF	HEAD (ft) Lebaron LV2448-2 (Double grate) A= 3.125 SF	RECOMMENDED GRATE
		1.5025 51	7- 3.123 51	
CB-1	0.73	0.009414934	0.0023537	Single
CB-2	0.51	0.00459528	0.0011488	Single
CB-3	0.85	0.012764665	0.0031912	Single
CB-4	0.64	0.007236549	0.0018091	Single

Note: Capacity based on Orifice Flow (ponded condition).

b no. 1833.109	COMPUTED BY:	RFK	CHECKED BY:	KJP
FILE: 27 Charge Pond Road	DATE:	11/11/21	DATE:	11/12/2021

JOB

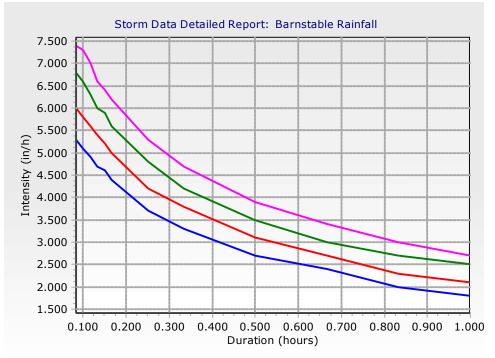
Element Details					
ID		30	Notes		
Label	E	Barnstable Rainfall			
Duration (hours)	10 Year (in/h)	25 Year (in/h)	50 Year (in/h)	100 Year (in/h)	
0.083	5.300	6.000	6.800	7.400	
0.100	5.100	5.800	6.600	7.300	
0.117	4.900	5.600	6.300	7.000	
0.133	4.700	5.400	6.000	6.600	
0.150	4.600	5.200	5.900	6.400	
0.167	4.400	5.000	5.600	6.200	
0.250	3.700	4.200	4.800	5.300	
0.333	3.300	3.800	4.200	4.700	
0.500	2.700	3.100	3.500	3.900	
0.667	2.400	2.700	3.000	3.400	
0.833	2.000	2.300	2.700	3.000	
1.000	1.800	2.100	2.500	2.700	

Storm Data Detailed Report: Barnstable Rainfall

Library Status Summary

	Synchronization Details
ID	30
Label	Barnstable Rainfall
Modified Date	6/25/2019 9:03:03 AM
Library Source	G:\Corp-Data\Qags\StormCAD\8 XM\Rainfall .xml
Library Modified Date	10/16/2008 3:19:18 PM
Synchronization Status	Synchronize to Library
Engineering Reference Guid	686ed606-a18a-4e03-9cab- f4a1ec6f02ac

Untitled1.stsw 6/25/2019 Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 Bentley StormCAD CONNECT Edition [10.01.01.04] Page 1 of 2



Storm Data Detailed Report: Barnstable Rainfall

Untitled1.stsw 6/25/2019 Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 Bentley StormCAD CONNECT Edition [10.01.01.04] Page 2 of 2 Attachment 5 Groundwater Recharge, Drawdown, Water Quality Volume, Proprietary Water Quality Inlet Sizing, TSS Removal, and Riprap Apron Sizing





Groundwater Recharge Volume Required:

Rv = F x Impervious Area, where:

- **Rv** = Required Recharge Volume [Ac-ft]
- **F** = Target Depth Factor associated with each Hydrologic Soil Group (HSG) [in]

Impervious Area = Total Pavement and Rooftop Area under Post-development Conditions [Ac]

			Increased Impervious Area [Acres]	Required Recharge Volume [Ac-ft]	
HSG "A", use F =	0.6	in	0.406	0.020	
HSG "B", use F =	0.35	in	0.000	0.000	
HSG "C", use F =	0.25	in	0.000	0.000	
HSG "D", use F =	0.1	in	0.000	0.000	
Total R	equire	0.020	Ac-ft		

Capture Area Adjustment:	(Ref: DEP Handbook V.3 Ch.1 P.27-28)

Total Increased Site Impervious Area (Total)=	0.406 Acres
Impervious Area Draining to Infiltrative BMPs (infil) =	0.406 Acres

Capture Area Adjustment Factor = (Total)/(Infil) = Ca =	1.00
Adjusted Required Recharge Volume = Ca x Rv	0.020 Ac-ft

Groundwater Recharge Volume Provided :

ВМР	Provided Recharge Volume [Ac-ft]	
Modified Depression	0.112	_
Total Provided Recharge Volume =	0.112	Ac-ft

PROVIDED GROUNDWATER RECHARGE VOLUME IS GREATER THAN OR EQUAL TO THE REQUIRED RECHARGE VOLUME, THEREFORE PROPOSED STORMWATER MANAGEMENT DESIGN IS IN COMPLIANCE WITH STANDARD 3.

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JOB: 27 Charge Pond Road	DATE:	11/11/21	DATE:	11/12/2021



Drawdown Time =			where:	Rv = Storage Volume Below Outlet [Ac-ft]
	(K) (Bottom Area)		where:	K= Infiltration Rate [in/hr]
				Bottom Area= Bottom Area of Recharge System [Ac]
Modified Depression	n			
	Rv =	0.112 A	Ac-ft	
	K =	2.410 i	n/hr	
Bot	tom Area =	0.008 A	Acres	
Drawdo	own Time =	69.710 H	lours	< 72 Hours, Design is in compliance with the standard.

Note:

1. The infiltration BMPs have been designed to fully drain within 72 hours, therefore the proposed stormwater management design is in compliance with Standard 3.

2. Infiltration Rate based on Volume 3, Chapter 1, Table 2.3.3 *Rawls Rates* from the 2008 MA DEP Stormwater Management Handbook.

JOB NO. 1833.109	COMPUTED BY:	NBB	CHECKED BY:	RFK
JOB: 27 Charge Pond Road	DATE:	11/11/21	DATE:	11/12/2021

Stage-Area-Storage for Pond 1: Modified Depression

	_	_		_	
Elevation	Surface	Storage	Elevation	Surface	Storage
(feet)	(acres)	(acre-feet)	(feet)	(acres)	(acre-feet)
22.00	0.021	0.000	24.60	0.097	0.148
22.05	0.022	0.001	24.65	0.099	0.153
22.10	0.024	0.002	24.70	0.101	0.158
22.15	0.025	0.003	24.75	0.103	0.163
22.20	0.026	0.005	24.80	0.105	0.168
22.25	0.028	0.006	24.85	0.106	0.173
22.30	0.029	0.008	24.90	0.108	0.178
22.35	0.030	0.009	24.95	0.110	0.184
22.40	0.032	0.011	25.00	0.112	0.190
22.45	0.033	0.012	25.05	0.114	0.195
22.50	0.035	0.014	25.10	0.116	0.201
22.55	0.036	0.016	25.15	0.118	0.207
22.60	0.037	0.017	25.20	0.120	0.213
22.65 22.70	0.039 0.040	0.019 0.021	25.25 25.30	0.122 0.124	0.219 0.225
22.70	0.040	0.021	25.30	0.124	0.225
22.75	0.041	0.025	25.33	0.120	0.231
22.85	0.043	0.023	25.40	0.120	0.244
22.00	0.045	0.020	25.50	0.132	0.250
22.95	0.043	0.032	25.55	0.132	0.257
23.00	0.048	0.035	25.60	0.135	0.264
23.05	0.049	0.037	25.65	0.137	0.271
23.10	0.051	0.039	25.70	0.139	0.277
23.15	0.052	0.042	25.75	0.141	0.285
23.20	0.053	0.045	25.80	0.143	0.292
23.25	0.055	0.047	25.85	0.145	0.299
23.30	0.056	0.050	25.90	0.147	0.306
23.35	0.057	0.053	25.95	0.149	0.314
23.40	0.059	0.056	26.00	0.151	0.321
23.45	0.060	0.059			
23.50	0.062	0.062			
23.55	0.063	0.065			
23.60	0.064	0.068			
23.65	0.066	0.071			
23.70	0.067	0.075			
23.75	0.068	0.078			
23.80	0.070	0.082			
23.85	0.071	0.085			
23.90	0.072	0.089			
23.95	0.074	0.092			
24.00	0.075	0.096			
24.05 24.10	0.077 0.079	0.100 0.104			
24.10	0.079	0.104			
24.13 24.20	0.081 0.082	0.108 0.112			
24.20	0.082	0.112			
24.20	0.086	0.120			
24.35	0.088	0.120			
24.40	0.090	0.129			
24.45	0.092	0.120			
24.50	0.094	0.138			
24.55	0.095	0.143			



$V_{WQ} = (D_{WQ} / 12 \text{ in/ft}) \times (A_{IMP} \times 43,560 \text{ SF/Ac}) \text{ where:}$

V_{wq} = Required Water Quality Volume [CF]

 \mathbf{D}_{WQ} = Water Quality Depth : 1-inch for discharges within a Zone II or Interim Wellhead Protection Area, to or near critical areas, runoff from LUHPPL, or exfiltration to soil with infiltration rate 2.4 in/hr or greater; $\frac{1}{2}$ -inch for discharges to other areas.

A_{IMP} = Post-development Impervious Area; may exclude roof top areas [Ac]

Required Water Quality Volume:

Drainage Area/	New A _{IMP}	Dwq	V _{wq} Requ	ired
Treatment Train	[Ac]	[in]	[CF]	
PDA-4B	0.406	1	1,474	
Total Required W	ater Quality	Volume:	1,474	Cubic Feet
				0.034 Ac-ft

Provided Water Quality Volume:

Drainage Area/		Water Quality	
Treatment Train	BMP	Volume Provided	
		[CF]	_
PDA-4B	Modified Depression	4,868	_
Total Provided \	Nater Quality Volume:	4,868	Cubic Feet

WATER QUALITY VOLUME PROVIDED IS GREATER THAN OR EQUAL TO THE REQUIRED WATER QUALITY VOLUME, THEREFORE PROPOSED STORMWATER MANAGEMENT DESIGN IS IN COMPLIANCE WITH STANDARD 4.

JOB NO. 1833.109	COMPUTED BY:	NBB	CHECKED BY:	RFK
JOB: 27 Charge Pond Road	DATE:	11/11/21	DATE:	11/12/2021

Stage-Area-Storage for Pond 1: Modified Depression

Elevation	Surface	Storage	Elevation	Surface	Storage
(feet)	(sq-ft)	(cubic-feet)	(feet)	(sq-ft)	(cubic-feet)
22.00	915	0	24.60	4,234	6,432
22.05	974	47	24.65	4,315	6,646
22.10	1,033	97	24.70	4,395	6,864
22.15	1,091	150	24.75	4,476	7,086
22.20	1,150	207	24.80	4,557	7,311
22.25	1,209	266	24.85	4,637	7,541
22.20	1,268	327	24.90	4,718	7,341
22.30	1,327	392	24.90	4,798	8,013
22.33	1,385	460	25.00	4,798	
22.40	1,444	531	25.00	4,964	8,255
22.43	1,503	605	25.05	5,049	8,501 8,751
	1,562	681		5,134	
22.55			25.15		9,006
22.60	1,621	761	25.20	5,219	9,265
22.65	1,679	843	25.25	5,305	9,528
22.70	1,738	929	25.30	5,390	9,795
22.75	1,797	1,017	25.35	5,475	10,067
22.80	1,856	1,108	25.40	5,560	10,343
22.85	1,915	1,203	25.45	5,645	10,623
22.90	1,973	1,300	25.50	5,730	10,907
22.95	2,032	1,400	25.55	5,815	11,196
23.00	2,091	1,503	25.60	5,900	11,489
23.05	2,150	1,609	25.65	5,985	11,786
23.10	2,209	1,718	25.70	6,070	12,087
23.15	2,267	1,830	25.75	6,156	12,393
23.20	2,326	1,945	25.80	6,241	12,703
23.25	2,385	2,063	25.85	6,326	13,017
23.30	2,444	2,183	25.90	6,411	13,335
23.35	2,503	2,307	25.95	6,496	13,658
23.40	2,561	2,433	26.00	6,581	13,985
23.45	2,620	2,563			
23.50	2,679	2,696			
23.55	2,738	2,831			
23.60	2,797	2,969			
23.65	2,855	3,111			
23.70	2,914	3,255			
23.75	2,973	3,402			
23.80	3,032	3,552			
23.85	3,091	3,705			
23.90	3,149	3,861			
23.95	3,208	4,020			
24.00	3,267	4,182			
24.05	3,348	4,347			
24.10	3,428	4,517			
24.15	3,509	4,690			
<mark>24.20</mark>	<mark>3,589</mark>	<mark>4,868</mark>			
24.25	3,670	5,049			
24.30	3,751	5,235			
24.35	3,831	5,424			
24.40	3,912	5,618			
24.45	3,992	5,815			
24.50	4,073	6,017			
24.55	4,154	6,223			
		-			



Step 1: Define Minimum Flow Rate per Water Quality Inlet to Treat Desired Water Quality Volume

Water quality inlets are sized based on flow rate; therefore expressing Water Quality Volume as a flow rate based on the percentage of cumulative average volume captured ensures systems are sized to achieve the desired Water Quality treatment level.

 $Q = (q_u)(A)(WQV)$ where:

Q = peak flow rate associated with first 1.0-inch of runoff [CFS]

 q_u = The Peak Discharge [CFS/mi²/in] Massachusetts DEP Standard Method to Convert Required Water Quality Volume to a Discharge Rate for Sizing Flow Based Manufactured Proprietary Stormwater Treatment Practices
 A = Contributing Drainage Area, Impervious Surface Only [Ac]

WQV = The Water Quality Treatment Depth [In]

WQI No.	А	Тс	WQV	q _u	Q
WQI NO.	(Ac)	(Min)	(in)	(csm/in)	(cfs)
WQS-1	0.406	6.0	1.0	774	0.49
Total	0.406	Acres			

Step 2: Size Water Quality Inlet as recommended by Manufacturer

See attached Sizing Report(s) for recommended model(s).

Step 3: Water Quality Volume Provided by WQIunit(s)

Total Impervious Area Treated by WQI u	ınit(s):		0.406 Acres 17,685 SF	
Treated Water Quality Depth :			1.0 inches	
(accounted for by Average Water Quality	ty Flow Rate)			
Total Water Quality Volume provided b	oy Water Qualit	y Inlets	1,474 CF	
JOB NO. 1833.109	COMPUTED BY:	NBB	CHECKED BY:	RFK
JOB: 27 Charge Pond Road	DATE:	11/11/21	DATE:	11/11/2021





CDS ESTIMATED NET ANNUAL SOLIDS LOAD REDUCTION **BASED ON THE RATIONAL RAINFALL METHOD 27 CHARGE POND ROAD** WAREHAM, MA 0.41 ac Unit Site Designation **WQS-1** Area 0.9 Rainfall Station # Weighted C 66 6 min t_c CDS Model 1515-3 **CDS** Treatment Capacity 1.0 cfs Rainfall Percent Rainfall Cumulative Total Flowrate **Treated Flowrate** Incremental Intensity¹ Volume¹ **Rainfall Volume** Removal (%) (cfs) (cfs) (in/hr) 0.08 35.3% 35.3% 0.03 0.03 33.6 0.06 0.06 0.16 23.8% 59.1% 22.2 0.24 12.9% 72.0% 0.09 0.09 11.8 0.32 7.8% 79.8% 0.12 0.12 7.0 0.40 4.9% 84.7% 0.15 0.15 4.3 0.48 3.5% 88.3% 0.18 0.18 3.0 1.7% 0.56 90.0% 0.20 0.20 1.4 0.64 1.8% 91.8% 0.23 0.23 1.5 0.72 1.9% 93.7% 0.26 0.26 1.5 0.80 0.9% 94.6% 0.29 0.29 0.7 1.00 2.3% 96.9% 0.37 0.37 1.7 2.00 2.9% 0.73 0.73 99.8% 1.4 3.00 0.2% 100.0% 1.10 1.00 0.1 0.00 0.0% 100.0% 0.00 0.00 0.0 0.00 0.0% 100.0% 0.00 0.00 0.0 0.00 0.0% 100.0% 0.00 0.00 0.0 0.00 0.0% 100.0% 0.00 0.00 0.0 0.00 0.0% 100.0% 0.00 0.00 0.0 0.00 0.0% 100.0% 0.00 0.00 0.0 100.0% 0.00 0.0 0.00 0.0% 0.00 0.00 0.0% 100.0% 0.00 0.00 0.0 90.0 Removal Efficiency Adjustment² = 0.0% Predicted % Annual Rainfall Treated = 100.0% Predicted Net Annual Load Removal Efficiency = 90.0% 1 - Based on 14 years of 15 minute precipitation data from NCDC station 3821, Hyannis, in Barnstable County, MA 2 - Reduction due to use of 60-minute data for a site that has a time of concentration less than 30-minutes.



Median Stone Sizing:

$$D_{50} = 0.2 D_0 \left(\frac{Q}{\sqrt{g D_0}^{2.5}} \right)^{\frac{4}{3}} \left(\frac{D_0}{TW} \right)$$

Where: D₀ = Maximum Inside Pipe Diameter (ft)

 D_{50} = Median Riprap Diameter (ft)

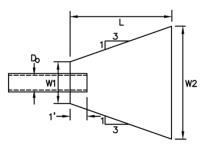
Q = Peak Discharge Rate from Hydraulic Design (cfs)

TW = Tailwater Depth (ft); (Use $0.4D_0$ if TW is unknown, max $1.0D_0$)

g = Gravitational Acceleration Constant = 32.2 ft/s^2

Apron Sizing:

D ₅₀ [In]	Apron Length (L) [ft}	Apron Depth [In]	Apron Width At Beginning	Apron Width At End	
5	4D ₀	3.5D ₅₀	3D ₀	3D ₀ +⅔L	₽₀
6	4D ₀	3.3D ₅₀	3D ₀	3D₀+3⁄L	F
10	5D ₀	2.4D ₅₀	3D ₀	3D₀+3⁄L	LW1
14	6D ₀	2.2D ₅₀	3D ₀	3D ₀ +⅔L	1'-+
20	7D ₀	2.0D ₅₀	3D ₀	3D ₀ +⅔L	11
22	8D ₀	2.0D ₅₀	3D ₀	3D ₀ +⅔L	



FLARED END SECTION	PIPE DIAMETER (D ₀) (FEET)	100-YEAR STORM FLOW (Q) (CFS)	TAILWATER (TW) [ft]	MEDIAN STONE DIAMETER (D ₅₀) (INCHES)	APRON LENGTH (L) (FEET)	APRON DEPTH [In]	APRON WIDTH AT BEGINING (W ₁) [ft]	APRON WIDTH AT END (W ₂) [ft]
FE-03	1.0	0.55	0.4	5	4.00	17.5	3.0	5.7

<u>Notes</u>

[1] Calculations performed in accordance with Hydraulic Engineering Circular No. 14, Third Edition; Hydraulic Design of Energy Dissipaters for Culverts and Channels, dated July 2006.

[2] Pipe shall extend 1 foot into riprap.

[3] For maximum pipe size of 60".

[4] FE-03 flow taken from 100-year storm flow in HydroCAD

JOB NO. 1833.109	COMPUTED BY:	NBB	CHECKED BY:	RFK
JOB: 27 Charge Pond Road	DATE: 11	./15/21	DATE:	11/16/2021

Attachment 6 Site Owner's Manual



Site Owner's Manual

Definitive Subdivision Plan of 27 Charge Pond Road

27 Charge Pond Road Wareham, Massachusetts

Prepared for: A.D. Makepeace Company 158 Tihonet Road Wareham, MA 02571

Prepared by:



November 19, 2021

1833109RP005A

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REFER TO THE APPROVED DEFINITIVE SUBDIVISION PLANS

APPENDICES

Appendix A: Operation and Maintenance Log Appendix B: List of Emergency Contacts Appendix C: Proprietary Separator Technical Manual



1.0 INTRODUCTION

The Site Owner's Manual complies with the Long-Term Pollution Prevention Plan (Standard 4) and the Long-Term Operation and Maintenance Plan (Standard 9) requirements of the 2008 Massachusetts Department of Environmental Protection (DEP) Stormwater Handbook. The Manual outlines source control and pollution prevention measures and maintenance requirements of stormwater best management practices (BMPs) associated with the proposed development.



2.0 SITE OWNER'S AGREEMENT

2.1 Operation and Maintenance Compliance Statement

Site Owner:	A.D. Makepeace Company
	158 Tihonet Road
	Wareham, MA 02571

Responsible Party: A.D. Makepeace Company

A.D. Makepeace Company or their successors shall maintain ownership of the on-site stormwater management system as well as the responsibility for operation and maintenance during the post-development stages of the project. The site has been inspected for erosion and appropriate measures have been taken to permanently stabilize any eroded areas. All aspects of stormwater best management practices (BMPs) have been inspected for damage, wear and malfunction, and appropriate steps have been taken to repair or replace the system or portions of the system so that the stormwater at the site may be managed in accordance with the Stormwater Management Standards. Future responsible parties shall be notified of their continuing legal responsibility to operate and maintain the BMPs. The operation and maintenance plan for the stormwater BMPs is being implemented.

Responsible Party Signature

Date

2.2 Stormwater Maintenance Easements

There are no off-site areas utilized for stormwater control, therefore no stormwater management easements are required. The Site Owner will have access to all stormwater practices for inspection and maintenance, including direct maintenance access by heavy equipment to structures requiring regular maintenance.

2.3 Record Keeping

The Site Owner shall maintain a rolling log in which all inspections and maintenance activities for the past three years shall be recorded. The Operation and Maintenance Log includes information pertaining to inspections, repairs, and disposal relevant to the project's stormwater management system. The Log is located in Appendix A.

The Operation and Maintenance Log shall be made available to the Conservation Commission and the DEP upon request. The Conservation Commission and the DEP shall be allowed to enter and inspect the premises to evaluate and ensure that the responsible party complies with the maintenance requirements for each BMP.



2.4 Training

Employees involved in grounds maintenance and emergency response will be educated on the general concepts of stormwater management and groundwater protection. The Site Owner's Manual will be reviewed with the maintenance staff. The staff will be trained on the proper course of action for specific events expected to be incurred during routine maintenance or emergency situations.



3.0 LONG-TERM POLLUTION PREVENTION PLAN

In compliance with Standard 4 of the 2008 DEP Stormwater Management Handbook, this section outlines source control and pollution prevention measures to be employed on-site after construction.

3.1 Storage of Materials and Waste

The site shall be kept clear of trash and debris at all times. Certain materials and waste products shall be stored inside or outside upon an impervious surface and covered, as required by local and state regulations.

3.2 Vehicle Washing

No commercial vehicle washing shall take place on site.

3.3 Routine Inspections and Maintenance of Stormwater BMPs

See Section 4.0 Long-Term Operation and Maintenance Plan, for routine inspection and maintenance requirements for all proposed stormwater BMPs.

3.4 Spill Prevention and Response

A contingency plan shall be implemented to address the spill or release of petroleum products and hazardous materials and will include the following measures:

- Equipment necessary to quickly attend to inadvertent spills or leaks shall be stored on-site in a secure but accessible location. Such equipment shall include but not be limited to the following: safety goggles, chemically resistant gloves and overshoe boots, water and chemical fire extinguishers, sand and shovels, suitable absorbent materials, storage containers and first aid equipment (i.e. Indian Valley Industries, Inc. 55-gallon Spill Containment kit or approved equivalent).
- 2. Spills or leaks shall be treated properly according to material type, volume of spillage and location of spill. Mitigation shall include preventing further spillage, containing the spilled material in the smallest practical area, removing spilled material in a safe and environmentally-friendly manner, and remediation of any damage to the environment.
- 3. For large spills, Massachusetts DEP Hazardous Waste Incident Response Group shall be notified immediately at 888-304-1133 and an emergency response contractor shall be consulted.



3.5 Maintenance of Lawns, Gardens, and other Landscaped Areas

Lawns, gardens, and other landscaped areas shall be maintained regularly by the site owner. Vegetated and landscaped BMPs will be maintained as outlined in Section 4.0.

3.6 Storage and Use of Fertilizers, Herbicides, and Pesticides

All fertilizers, herbicides, and pesticides shall be stored in accordance with local, state, and federal regulations. The application rate and use of fertilizers, herbicides, and pesticides on the site shall at no time exceed local, state, or federal specifications.

3.7 Pet Waste Management

Pet owners shall be required to pick up after their animals and dispose of waste in the trash.

3.8 Snow and Deicing Chemical Management

Snow removal and use of deicing chemicals at the proposed development shall comply with the following requirements:

- Plowed snow shall be placed in the areas outside of wetland boundaries and stormwater best management practices. The following maintenance measures shall be undertaken at all snow disposal sites:
 - Debris shall be cleared from an area prior to using it for snow disposal.
 - Debris and accumulated sediments shall be cleared from the site and properly disposed of at the end of the snow season and no later than May 15.
- In accordance with the Massachusetts General Laws, Chapter 85, Section 7A, salt and other de-icing chemicals will be stored at an indoor location. Salt and other deicing chemicals shall be stored in accordance with Massachusetts General Law.
- Sand piles shall be contained and stabilized to prevent the discharge of sand to wetlands or water bodies, and, where feasible, covered.
- Salt storage piles shall be located outside of the 100-year floodplain.
- The application of salt on the proposed roadway shall at no time exceed state or local requirements.
- The use of deicing materials and sand shall not be used at the proposed project site to protect off-site areas.



4.0 LONG-TERM OPERATION AND MAINTENANCE PLAN

This section outlines the stormwater best management practices (BMPs) associated with the proposed stormwater management system and identifies the long-term inspection and maintenance requirements for each BMP.

4.1 Stormwater Management System Components

The following table outlines the type and quantity of the BMPs and their general location. All basins are accessible for maintenance from the development driveway.

BMP Type	Quantity	Location
Catch Basins	4	Throughout Parker Mills Road.
Area Drain	1	Off of Parker Mills Road.
Proprietary Separator/Water Quality Structure	1	Off of Parker Mills Road.
Modified Depression	1	Within Lot 1, south of Parker Mills Road.
Stormwater Outfall	3	Within Lot 1, south of Parker Mills Road.

4.2 Inspection and Maintenance Schedules

4.2.1 General Maintenance for Mosquito Control

If necessary to minimize mosquito breeding, a licensed pesticide applicator shall apply larvicides, such as Bacillus sphaericus (Bs) to all catch basins sumps, and water quality inlets. Larvicides shall be applied in compliance with all pesticide label requirements, and will be applied during or immediately after wet weather, unless the product used can withstand extended dry periods. Ensure all manhole covers, and inspection ports are secure to reduce the likelihood of mosquitoes laying eggs in standing water.

4.2.2 Deep Sump and Hooded Catch Basins

Catch basins shall be inspected four times per year, including after the foliage season. Other inspection and maintenance requirements include:

- Units shall be cleaned (organic material, sediment and hydrocarbons removed) four times per year or whenever the depth of deposits is greater than or equal to one half the depth from the bottom of the invert of the lowest pipe in the basin.
 - Cleanout shall always occur after street sweeping.



- If any evidence of hydrocarbons is found during inspection, the material shall be immediately removed using absorbent pads or other suitable measures and disposed of legally.
- Remove other accumulated debris as necessary.
- Transport and disposal of accumulated sediment off-site shall be in accordance with applicable local, state and federal guidelines and regulations.

4.2.3 Area Drains and Drop Inlets

Area drains and drop inlets shall be inspected and/or cleaned at least once per year.

4.2.4 **Proprietary Separators**

Maintenance of proprietary separators shall be performed according the recommendations set forth by the manufacturer (see Appendix C. Proprietary Separator Technical Manual for complete installation, operation and maintenance procedures). Inspection and maintenance procedures for proprietary devices are provided below:

- Units shall be inspected post-construction, prior to being put into service.
- Units shall be inspected not less than twice per year following installation and no less than once per year thereafter.
- Units shall be inspected immediately after any oil, fuel or chemical spill.
- All inspections shall include checking the oil level and sediment depth in the unit.
- Removal of sediments/oils shall occur per manufacturer recommendations.
- A licensed waste management company shall remove captured petroleum waste products from any oil, chemical or fuel spills and dispose.
- OSHA confined space entry protocols shall be followed if entry into the unit is required.

4.2.5 Modified Depression

The modified depression shall be inspected and maintained after major storm events (rainfall totals greater than 2.5 inches in 24 hours) during the first three months of operation and twice a year and when there are discharges through the outlet control structure thereafter.



Additionally, all pretreatment BMPs shall be inspected in accordance with the minimal requirements specified for those practices and after all major storm events. Inspections shall include the following measures:

- During and after major storm events, the length of time standing water remains in the modified depression shall be recorded.
 - If the time is greater than 72 hours, thoroughly inspect the modified depression for signs of clogging.
 - A corrective action plan shall be developed by a qualified professional to restore infiltrative function. The Site Owner shall take immediate action to implement these corrective measures.
- Examine the outlet structure for evidence of clogging or outflow release velocities that are greater than the design velocity.
- Identify areas of sediment accumulation, differential settlement, cracking, and erosion within the modified depression.
- Inspect embankments for leakage and tree growth.
- Examine the health of the vegetation within the modified depression and on the embankments.

Corrective measures shall be taken immediately as warranted by the inspections. If any evidence of hydrocarbons is found during inspection, the material shall be immediately removed using absorbent pads or other suitable measures and legally disposed.

Preventative maintenance shall include the following activities:

- Mow the buffer area and the modified depression bottom and side slopes, if vegetated.
- Remove trash, debris, and accumulated organic matter.
- Remove clippings after mowing.

4.2.6 Stormwater Outfalls

Flared end sections and associated riprap spillways shall be inspected at least once per year and after major storm events (rainfall totals greater than 2.5 inches in 24 hours) to ensure that the stability of the outlet area is maintained. The outfall area shall be kept clear of debris such as trash, branches, and sediment. Repairs shall be made immediately if riprap displacement or downstream channel scour is observed.



4.3 Estimated Operation and Maintenance Budget

An operations and maintenance budget was prepared to approximate the annual cost of the inspections required in compliance with the DEP Stormwater Management Policy. The table below estimates the annual cost to inspect and maintain each proposed BMP, based on the requirements in Section 4.2.

ВМР Туре	# of BMPS	Annual O&M Cost (per BMP) ¹	Total Cost
Mosquito Control	6	\$50-\$100	\$300-\$600
Catch Basin	4	\$200-\$400	\$800-\$1600
Area Drain/Drop Inlet	1	\$50-\$100	\$50-\$100
Proprietary Separator	1	\$100-\$300	\$100-\$300
Modified Depression	1	\$200 - \$400	\$200-\$400
Riprap Spillway	1	\$50-\$100	\$50-\$100
Flared End Pipe Outfall	3	\$50-\$100	\$150-\$300
		Total	\$1650-\$3400

4.4 Public Safety Features

Multiple safety measures are proposed to protect the public and prevent pollutant contamination of the stormwater management system and other water resources. Proposed curbing, sidewalk, and tree plantings along the access driveway will prevent cars from inadvertently detouring down steep side slopes and into adjacent wetlands or stormwater controls. The Site was designed to ensure protection to the public and prevent pollutant contamination of the stormwater management system.

¹ Annual maintenance cost is based on estimate of the cost to complete all inspection and maintenance measures outlined in Section 4.2. For BMPs that require sediment removal at regular intervals (i.e. every 5 or 10 years), the annual cost includes the annual percentage of that cost.



Figures

Refer to the Approved Definitive Subdivision Plans



Appendices



Appendix A

Operation and Maintenance Log



OPERATION AND MAINTENANCE LOG

This template is intended to comply with the operation and maintenance log requirements of the 2008 DEP Stormwater Management Handbook. Copies of this log should be made for all inspections and kept on file for three years from the inspection date.

Name/Company of Inspector:

Date/Time of Inspection:

Weather Conditions:

(Note current weather and any recent precipitation events)

Stormwater BMP	Inspection Observations	Actions Required



Appendix B

List of Emergency Contacts



List of Emergency Contacts:

Massachusetts DEP Hazardous Waste Incident Response Group Tel: (617) 792-7653

Wareham Fire Department Emergencies: Dial 911 273 Main Street Wareham, MA 02571 Tel: (508) 295-2973 Fire Chief: Matt Rowley

Wareham Police Department Emergencies: Dial 911 2515 Cranberry Hwy Wareham, MA 02571 Tel: (508) 295-1212 Fax: (508) 291-1001 Chief of Police: Walter Correia



Appendix C

Proprietary Separator Technical Manual





CDS Guide Operation, Design, Performance and Maintenance



CDS®

Using patented continuous deflective separation technology, the CDS system screens, separates and traps debris, sediment, and oil and grease from stormwater runoff. The indirect screening capability of the system allows for 100% removal of floatables and neutrally buoyant material without blinding. Flow and screening controls physically separate captured solids, and minimize the re-suspension and release of previously trapped pollutants. Inline units can treat up to 6 cfs, and internally bypass flows in excess of 50 cfs (1416 L/s). Available precast or cast-in-place, offline units can treat flows from 1 to 300 cfs (28.3 to 8495 L/s). The pollutant removal capacity of the CDS system has been proven in lab and field testing.

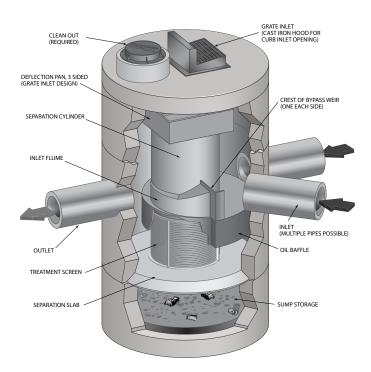
Operation Overview

Stormwater enters the diversion chamber where the diversion weir guides the flow into the unit's separation chamber and pollutants are removed from the flow. All flows up to the system's treatment design capacity enter the separation chamber and are treated.

Swirl concentration and screen deflection force floatables and solids to the center of the separation chamber where 100% of floatables and neutrally buoyant debris larger than the screen apertures are trapped.

Stormwater then moves through the separation screen, under the oil baffle and exits the system. The separation screen remains clog free due to continuous deflection.

During the flow events exceeding the treatment design capacity, the diversion weir bypasses excessive flows around the separation chamber, so captured pollutants are retained in the separation cylinder.



Design Basics

There are three primary methods of sizing a CDS system. The Water Quality Flow Rate Method determines which model size provides the desired removal efficiency at a given flow rate for a defined particle size. The Rational Rainfall Method[™] or the and Probabilistic Method is used when a specific removal efficiency of the net annual sediment load is required.

Typically in the Unites States, CDS systems are designed to achieve an 80% annual solids load reduction based on lab generated performance curves for a gradation with an average particle size (d50) of 125 microns (μ m). For some regulatory environments, CDS systems can also be designed to achieve an 80% annual solids load reduction based on an average particle size (d50) of 75 microns (μ m) or 50 microns (μ m).

Water Quality Flow Rate Method

In some cases, regulations require that a specific treatment rate, often referred to as the water quality design flow (WQQ), be treated. This WQQ represents the peak flow rate from either an event with a specific recurrence interval, e.g. the six-month storm, or a water quality depth, e.g. 1/2-inch (13 mm) of rainfall.

The CDS is designed to treat all flows up to the WQQ. At influent rates higher than the WQQ, the diversion weir will direct most flow exceeding the WQQ around the separation chamber. This allows removal efficiency to remain relatively constant in the separation chamber and eliminates the risk of washout during bypass flows regardless of influent flow rates.

Treatment flow rates are defined as the rate at which the CDS will remove a specific gradation of sediment at a specific removal efficiency. Therefore the treatment flow rate is variable, based on the gradation and removal efficiency specified by the design engineer.

Rational Rainfall Method™

Differences in local climate, topography and scale make every site hydraulically unique. It is important to take these factors into consideration when estimating the long-term performance of any stormwater treatment system. The Rational Rainfall Method combines site-specific information with laboratory generated performance data, and local historical precipitation records to estimate removal efficiencies as accurately as possible.

Short duration rain gauge records from across the United States and Canada were analyzed to determine the percent of the total annual rainfall that fell at a range of intensities. US stations' depths were totaled every 15 minutes, or hourly, and recorded in 0.01-inch increments. Depths were recorded hourly with 1-mm resolution at Canadian stations. One trend was consistent at all sites; the vast majority of precipitation fell at low intensities and high intensity storms contributed relatively little to the total annual depth.

These intensities, along with the total drainage area and runoff coefficient for each specific site, are translated into flow rates using the Rational Rainfall Method. Since most sites are relatively small and highly impervious, the Rational Rainfall Method is appropriate. Based on the runoff flow rates calculated for each intensity, operating rates within a proposed CDS system are determined. Performance efficiency curve determined from full scale laboratory tests on defined sediment PSDs is applied to calculate solids removal efficiency. The relative removal efficiency at each operating rate is added to produce a net annual pollutant removal efficiency estimate.

Probabilistic Rational Method

The Probabilistic Rational Method is a sizing program Contech developed to estimate a net annual sediment load reduction for a particular CDS model based on site size, site runoff coefficient, regional rainfall intensity distribution, and anticipated pollutant characteristics.

The Probabilistic Method is an extension of the Rational Method used to estimate peak discharge rates generated by storm events of varying statistical return frequencies (e.g. 2-year storm event). Under the Rational Method, an adjustment factor is used to adjust the runoff coefficient estimated for the 10-year event, correlating a known hydrologic parameter with the target storm event. The rainfall intensities vary depending on the return frequency of the storm event under consideration. In general, these two frequency dependent parameters (rainfall intensity and runoff coefficient) increase as the return frequency increases while the drainage area remains constant.

These intensities, along with the total drainage area and runoff coefficient for each specific site, are translated into flow rates using the Rational Method. Since most sites are relatively small and highly impervious, the Rational Method is appropriate. Based on the runoff flow rates calculated for each intensity, operating rates within a proposed CDS are determined. Performance efficiency curve on defined sediment PSDs is applied to calculate solids removal efficiency. The relative removal efficiency at each operating rate is added to produce a net annual pollutant removal efficiency estimate.

Treatment Flow Rate

The inlet throat area is sized to ensure that the WQQ passes through the separation chamber at a water surface elevation equal to the crest of the diversion weir. The diversion weir bypasses excessive flows around the separation chamber, thus preventing re-suspension or re-entrainment of previously captured particles.

Hydraulic Capacity

The hydraulic capacity of a CDS system is determined by the length and height of the diversion weir and by the maximum allowable head in the system. Typical configurations allow hydraulic capacities of up to ten times the treatment flow rate. The crest of the diversion weir may be lowered and the inlet throat may be widened to increase the capacity of the system at a given water surface elevation. The unit is designed to meet project specific hydraulic requirements.

Performance

Full-Scale Laboratory Test Results

A full-scale CDS system (Model CDS2020-5B) was tested at the facility of University of Florida, Gainesville, FL. This CDS unit was evaluated under controlled laboratory conditions of influent flow rate and addition of sediment.

Two different gradations of silica sand material (UF Sediment & OK-110) were used in the CDS performance evaluation. The particle size distributions (PSDs) of the test materials were analyzed using standard method "Gradation ASTM D-422 "Standard Test Method for Particle-Size Analysis of Soils" by a certified laboratory.

UF Sediment is a mixture of three different products produced by the U.S. Silica Company: "Sil-Co-Sil 106", "#1 DRY" and "20/40 Oil Frac". Particle size distribution analysis shows that the UF Sediment has a very fine gradation (d50 = 20 to 30 μ m) covering a wide size range (Coefficient of Uniformity, C averaged at 10.6). In comparison with the hypothetical TSS gradation specified in the NJDEP (New Jersey Department of Environmental Protection) and NJCAT (New Jersey Corporation for Advanced Technology) protocol for lab testing, the UF Sediment covers a similar range of particle size but with a finer d50 (d50 for NJDEP is approximately 50 μ m) (NJDEP, 2003).

The OK-110 silica sand is a commercial product of U.S. Silica Sand. The particle size distribution analysis of this material, also included in Figure 1, shows that 99.9% of the OK-110 sand is finer than 250 microns, with a mean particle size (d50) of 106 microns. The PSDs for the test material are shown in Figure 1.

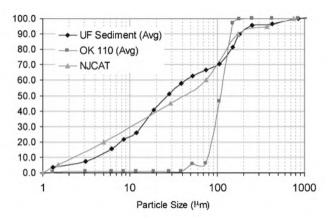


Figure 1. Particle size distributions

Tests were conducted to quantify the performance of a specific CDS unit (1.1 cfs (31.3-L/s) design capacity) at various flow rates, ranging from 1% up to 125% of the treatment design capacity of the unit, using the 2400 micron screen. All tests were conducted with controlled influent concentrations of approximately 200 mg/L. Effluent samples were taken at equal time intervals across the entire duration of each test run. These samples were then processed with a Dekaport Cone sample splitter to obtain representative sub-samples for Suspended Sediment Concentration (SSC) testing using ASTM D3977-97 "Standard Test Methods for Determining Sediment Concentration in Water Samples", and particle size distribution analysis.

Results and Modeling

Based on the data from the University of Florida, a performance model was developed for the CDS system. A regression analysis was used to develop a fitting curve representative of the scattered data points at various design flow rates. This model, which demonstrated good agreement with the laboratory data, can then be used to predict CDS system performance with respect to SSC removal for any particle size gradation, assuming the particles are inorganic sandy-silt. Figure 2 shows CDS predictive performance for two typical particle size gradations (NJCAT gradation and OK-110 sand) as a function of operating rate.

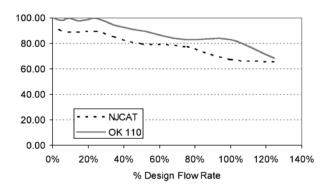


Figure 2. CDS stormwater treatment predictive performance for various particle gradations as a function of operating rate.

Many regulatory jurisdictions set a performance standard for hydrodynamic devices by stating that the devices shall be capable of achieving an 80% removal efficiency for particles having a mean particle size (d50) of 125 microns (e.g. Washington State Department of Ecology — WASDOE - 2008). The model can be used to calculate the expected performance of such a PSD (shown in Figure 3). The model indicates (Figure 4) that the CDS system with 2400 micron screen achieves approximately 80% removal at the design (100%) flow rate, for this particle size distribution (d50 = 125 μ m).

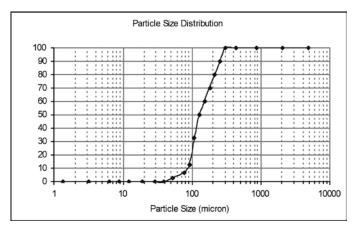
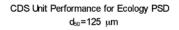


Figure 3. WASDOE PSD



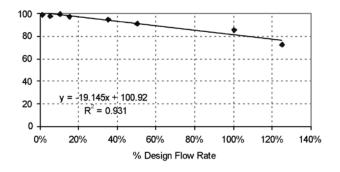


Figure 4. Modeled performance for WASDOE PSD.

Maintenance

The CDS system should be inspected at regular intervals and maintained when necessary to ensure optimum performance. The rate at which the system collects pollutants will depend more heavily on site activities than the size of the unit. For example, unstable soils or heavy winter sanding will cause the grit chamber to fill more quickly but regular sweeping of paved surfaces will slow accumulation.

Inspection

Inspection is the key to effective maintenance and is easily performed. Pollutant transport and deposition may vary from year to year and regular inspections will help ensure that the system is cleaned out at the appropriate time. At a minimum, inspections should be performed twice per year (e.g. spring and fall) however more frequent inspections may be necessary in climates where winter sanding operations may lead to rapid accumulations, or in equipment washdown areas. Installations should also be inspected more frequently where excessive amounts of trash are expected.

The visual inspection should ascertain that the system components are in working order and that there are no blockages or obstructions in the inlet and separation screen. The inspection should also quantify the accumulation of hydrocarbons, trash, and sediment in the system. Measuring pollutant accumulation can be done with a calibrated dipstick, tape measure or other measuring instrument. If absorbent material is used for enhanced removal of hydrocarbons, the level of discoloration of the sorbent material should also be identified



during inspection. It is useful and often required as part of an operating permit to keep a record of each inspection. A simple form for doing so is provided.

Access to the CDS unit is typically achieved through two manhole access covers. One opening allows for inspection and cleanout of the separation chamber (cylinder and screen) and isolated sump. The other allows for inspection and cleanout of sediment captured and retained outside the screen. For deep units, a single manhole access point would allows both sump cleanout and access outside the screen.

The CDS system should be cleaned when the level of sediment has reached 75% of capacity in the isolated sump or when an appreciable level of hydrocarbons and trash has accumulated. If absorbent material is used, it should be replaced when significant discoloration has occurred. Performance will not be impacted until 100% of the sump capacity is exceeded however it is recommended that the system be cleaned prior to that for easier removal of sediment. The level of sediment is easily determined by measuring from finished grade down to the top of the sediment pile. To avoid underestimating the level of sediment in the chamber, the measuring device must be lowered to the top of the sediment pile carefully. Particles at the top of the pile typically offer less resistance to the end of the rod than consolidated particles toward the bottom of the pile. Once this measurement is recorded, it should be compared to the as-built drawing for the unit to determine weather the height of the sediment pile off the bottom of the sump floor exceeds 75% of the total height of isolated sump.

Cleaning

Cleaning of a CDS systems should be done during dry weather conditions when no flow is entering the system. The use of a vacuum truck is generally the most effective and convenient method of removing pollutants from the system. Simply remove the manhole covers and insert the vacuum hose into the sump. The system should be completely drained down and the sump fully evacuated of sediment. The area outside the screen should also be cleaned out if pollutant build-up exists in this area.

In installations where the risk of petroleum spills is small, liquid contaminants may not accumulate as quickly as sediment. However, the system should be cleaned out immediately in the event of an oil or gasoline spill. Motor oil and other hydrocarbons that accumulate on a more routine basis should be removed when an appreciable layer has been captured. To remove these pollutants, it may be preferable to use absorbent pads since they are usually less expensive to dispose than the oil/water emulsion that may be created by vacuuming the oily layer. Trash and debris can be netted out to separate it from the other pollutants. The screen should be cleaned to ensure it is free of trash and debris.

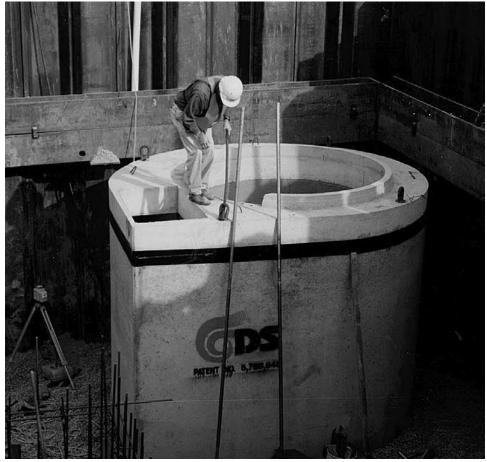
Manhole covers should be securely seated following cleaning activities to prevent leakage of runoff into the system from above and also to ensure that proper safety precautions have been followed. Confined space entry procedures need to be followed if physical access is required. Disposal of all material removed from the CDS system should be done in accordance with local regulations. In many jurisdictions, disposal of the sediments may be handled in the same manner as the disposal of sediments removed from catch basins or deep sump manholes. Check your local regulations for specific requirements on disposal.



CDS Model	Dian	neter	Distance from to Top of Se		Sediment Sto	rage Capacity
	ft	m	ft	m	У³	m³
CDS1515	3	0.9	3.0	0.9	0.5	0.4
CDS2015	4	1.2	3.0	0.9	0.9	0.7
CDS2015	5	1.5	3.0	0.9	1.3	1.0
CDS2020	5	1.5	3.5	1.1	1.3	1.0
CDS2025	5	1.5	4.0	1.2	1.3	1.0
CDS3020	6	1.8	4.0	1.2	2.1	1.6
CDS3025	6	1.8	4.0	1.2	2.1	1.6
CDS3030	6	1.8	4.6	1.4	2.1	1.6
CDS3035	6	1.8	5.0	1.5	2.1	1.6
CDS4030	8	2.4	4.6	1.4	5.6	4.3
CDS4040	8	2.4	5.7	1.7	5.6	4.3
CDS4045	8	2.4	6.2	1.9	5.6	4.3
CDS5640	10	3.0	6.3	1.9	8.7	6.7
CDS5653	10	3.0	7.7	2.3	8.7	6.7
CDS5668	10	3.0	9.3	2.8	8.7	6.7
CDS5678	10	3.0	10.3	3.1	8.7	6.7

Table 1: CDS Maintenance Indicators and Sediment Storage Capacities

Note: To avoid underestimating the volume of sediment in the chamber, carefully lower the measuring device to the top of the sediment pile. Finer silty particles at the top of the pile may be more difficult to feel with a measuring stick. These finer particles typically offer less resistance to the end of the rod than larger particles toward the bottom of the pile.



CDS Inspection & Maintenance Log

DS Mode	l:	Location:						
Date	Water depth to sediment ¹	Floatable Layer Thickness ²	Describe Maintenance Performed	Maintenance Personnel	Comments			

1. The water depth to sediment is determined by taking two measurements with a stadia rod: one measurement from the manhole opening to the top of the sediment pile and the other from the manhole opening to the water surface. If the difference between these measurements is less than the values listed in table 1 the system should be cleaned out. Note: to avoid underestimating the volume of sediment in the chamber, the measuring device must be carefully lowered to the top of the sediment pile.

2. For optimum performance, the system should be cleaned out when the floating hydrocarbon layer accumulates to an appreciable thickness. In the event of an oil spill, the system should be cleaned immediately.

SUPPORT

- Drawings and specifications are available at www.ContechES.com.
- Site-specific design support is available from our engineers.



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