STORMWATER REPORT

EVERSOURCE

37 DOTY STREET WAREHAM, MASSACHUSETTS 02576

Applicant:

NSTAR ELECTRIC COMPANY DBA EVERSOURCE ENERGY 247 STATION DRIVE WESTWOOD, MA 02090

Prepared By:

CIVIL & ENVIRONMENTAL CONSULTANTS, INC. 31 BELLOWS ROAD RAYNHAM, MASSACHUSETTS 02767

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31 Bellows Road | Raynham, MA 02767 | p: 774-501-2176 f: 774-501-2669 | www.cecinc.com

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1.0 PROJECT NARRATIVE

1.1 INTRODUCTION

On behalf of NSTAR Electric Company (DBA Eversource Energy), (the "Applicant"), Civil & Environmental Consultants, Inc. (CEC) has prepared this stormwater report and analysis to demonstrate compliance with the Massachusetts Department of Environmental Protection (MassDEP) Stormwater Management Standards

The Applicant is proposing to redevelop the existing Flagship Cinema site at 37 Doty St. (Assessors Map 103 Lots A1, B1, C1, and D1) as an Eversource Training Facility and will serve as a staging area for emergency response vehicles on an as needed basis. The proposed project will include new gravel areas to serve as various electrified/non-electrified training zones with associated permanent equipment, poles, and structures. In addition, the existing cinema building will be redeveloped into an indoor training area with classrooms and offices (the "Project").

1.2 EXISTING CONDITIONS

The former Flagship Cinemas previously operated on the site. The site is bounded by Doty Street to the south, Route 58 to the west and Route 495 to the north. The existing grounds of the facility consist mostly of pavement, with sidewalks and some vegetation along the north and south property boundaries, with a wetland and well established wooded area to the east.

The former cinema was served by water, electric and gas and a private septic system.

Stormwater is currently collected in an existing stormwater management system, which consists of a series of catch basins and manholes that ultimately discharge into a stormwater detention basin. The stormwater basin discharges overland, eventually reaching the bordering vegetated wetland. See Figure 1 for a Site Locus Map.

1.3 PROPOSED PROJECT

The proposed project will redevelop the cinema into an Eversource Training Facility that will also serve as a staging area for emergency response vehicles on an as-needed basis. The proposed improvements at the site will include new gravel area to serve as various electrified/non-electrified training zones with associated permanent equipment, poles, and structures. In addition, the existing cinema on site will be redeveloped into an indoor training area with classrooms and offices. Other improvements include new light poles with security cameras, installation of new fencing, enlarging the existing stormwater basin removing the existing grassed parking islands and curbing, and installing new landscaping.

The redevelopment will result in a net increase in impervious areas. Stormwater management improvements will be constructed as part of the proposed redevelopment to manage the stormwater runoff generated from the additional impervious areas. The improvements will be incorporated into the existing stormwater management system while maintaining the overall site stormwater drainage patterns.

2.0 STORMWATER MANAGEMENT SYSTEM

2.1 DESCRIPTION OF RUNOFF CONTROLS

The stormwater management improvements consist of components designed to manage runoff from the Site. These components attenuate runoff discharge peaks, minimize erosion, minimize the transport of sediments, improve water quality, and prevent impacts to the municipal drainage system and any downstream resource areas.

The stormwater management system implements a treatment drain of the Best Management Practices designed to provide 90% TSS (Total Suspended Solids) removal and 50% phosphorus removal for stormwater runoff from all impervious areas. The proposed stormwater management system will use the following specific control measures:

- <u>Deep Sump/Hooded Catch Basin</u>: Deep sump hooded catch basins are designed to remove trash, debris, and coarse sediment from stormwater runoff. Sheet flow from paved areas will be directed toward the deep sump hooded catch basins. Existing catch basins at the site will be inspected to confirm they include sumps and will be replaced with sumped catch basins, if required.
- <u>Proprietary particle separators (StormTech water quality units)</u>: The proposed StormTech water quality units provide efficient removal of free oils, debris, and total suspended solids (TSS). Although not the main objective of the water quality unit, some removal of heavy metals and other nutrients is also achieved. Water quality units allow for safe and easy removal of collected material and should be inspected and cleaned in accordance with the Operations and Maintenance (O&M) Plan and per manufacturer's recommendations.

The use of these units for treatment of stormwater is accepted as a good practice and is in accordance with sound professional standards. Testing was performed by a third party in order to determine the maximum treatment flow rates for both 80% and 50% TSS removal. The testing was also verified by the New Jersey Department of Environmental Protection and the results were verified under the NJCAT program. See Appendix C for supporting information.

• <u>Sediment Forebay</u>: The proposed sediment forebays will improve the water quality of stormwater discharging to the wet basin. The sediment forebays have been sized to hold 0.1 inches per contributing impervious acre resulting in a forebay with a capacities of and 1,650 cubic feet (CF) and 535 (CF), respectively, and will be constructed within the footprint of the existing detention basin.

• <u>Wet Basin:</u> Wet basins allow sediments to settle and remove soluble pollutants in a permanent pool as well as provide storage capacity above the permanent water level to control peak discharges rates. The bottom of the basin will contain vegetation allow for vegetative uptake, reduce soil erosion, and scouring of the basin.

The existing detention basin will be converted to function as a wet basin. Water quality pretreatment will be provided by the deep sump hooded catch basins, the proprietary water quality units, and the sediment forebay prior to discharge to the infiltration basin. The bottom of the basin is located at the estimated seasonal high groundwater elevation with will promote the basin having a permanent pool. The basin has been sized to contain all storm events up to and including the 100-year storm event with all runoffs discharging through a new outlet control structure.

- <u>Riprap Outlet Protection/Lever Spreaders:</u> Riprap outlet protection will be placed at all stormwater outfalls in order to reduce flows to non-erosive velocities to prevent erosion and conform to natural topography where appropriate.
- <u>Stormwater Infiltration Chambers</u>: Stormwater recharge for the site is provided through an existing underground stormwater infiltration chamber system that receives clean runoff from the building's roof areas. The chambers are located beneath the paved parking and circulation areas.

All runoff controls should be inspected and cleaned in accordance with the Operations and Maintenance (O&M) Plan included in Section 6.

2.2 CONSTRUCTION SEQUENCE PLAN

The purpose of the Construction Sequence Plan is to develop a working schedule for the implementation of the proposed stormwater improvements. Prior to initiating work, the siltation control barriers will be installed along the limit of work. Once the appropriate permits are obtained, the construction project will commence in the following sequence:

- 1. Notify all appropriate town departments prior to construction commencement in accordance with all approvals
- 2. Flag limits of construction necessary to facilitate a pre-construction meeting.
- Hold a pre-construction meeting. Remember to notify "Call Before You Dig" (1-800-922-4455)
- 4. Install all necessary siltation barriers and inlet protection as shown on the design drawings.
- 5. Placed crushed stoned stabilized construction pad and set up construction trailers and fence
- 6. Demo existing grassed parking islands/ remove existing light poles and install new binder asphalt within demoed parking island areas per Erosion & Sedimentation Control/Demolition Plan

- 7. Clear and grub/remove trees, as shown on the design drawings.
- 8. Perform excavation and install new drainage structures and any subsurface utilities
- 9. Resize and reshape existing grassed water quality swale and detention basin area as shown on the design drawings.
- 10. Construct training zone areas with associated permanent equipment, poles, and structures.
- 11. Loam and seed all disturbed areas and install proposed final landscaping.
- 12. Remove existing erosion control measures upon site stabilization.

All construction water will be collected and treated in accordance with the Erosion and Sediment Control Plan included in Section 5.0.

3.0 STORMWATER ANALYSIS

3.1 METHOD OF ANALYSIS

A hydrologic analysis has been performed for the Site comparing existing conditions and postdevelopment conditions using a software program developed by HydroCAD. This program analyzes site hydrology by the graphic peak discharge method documented in Technical Release No. 20 and Technical Release No. 55 published by the United States Department of Agriculture (USDA) Soil Conservation Service.

The following variables were developed for the contributing watersheds (drainage areas) in order to complete the analysis:

- **Rainfall Depth:** A hydrologic analysis was performed for the 24-hour 2-year, 10-year, 25-year, and 100-year, Type III 24-hr storm events (3.35, 4.95, 6.19, and 8.68 inches respectively) for each drainage area. The rainfall depths for the study area were obtained from available charts published in Atlas-14 for the Site's address.
- **Runoff Curve Number (RCN):** The RCN is a hydrologic characteristic that contributes to the peak rate of runoff and volume from a given storm event. It is dependent upon soil conditions and land use. Generally, higher curve numbers are associated with less pervious soils and, hence, greater amounts of runoff. Per NRCS, the majority of the site consist of Hydrologic Soil Groups (HSG) A and this HSG was used in the HydroCAD analysis. See Appendix B for NRCS custom Soil Resource Report.
- **Time of Concentration:** The time of concentration is defined as the time it takes runoff to travel from the hydraulically most distant part of the watershed to the downstream point of interest. This parameter is dependent on the characteristics of the ground surface and condition of the travel path. Times of concentration were calculated for the various sub catchments using the HydroCAD program, with a minimum time of concentration of six (6) minutes used in accordance with the protocol outlined in Technical Release No. 55.

3.2 DRAINAGE AREAS

In order to perform the analysis, the contributing drainage areas for pre-development, existing, and post-development conditions were delineated. The delineation of the drainage areas was determined by the topography depicted on the Existing Conditions plan. Brief descriptions of the existing conditions and proposed conditions drainage areas are as follows:

• **Existing Conditions:** The Site is divided into two (2) drainage areas and the stormwater runoff was evaluated for one (1) design point, Flow to Wetlands (Design Point 1). Refer to Figure

HYD-EX for the existing conditions drainage areas. For the purpose of the analysis, the times of concentration were calculated to the edge of the wetlands where present.

• **Proposed Conditions:** In the proposed condition, site hydraulic patterns were maintained from existing conditions. The Site is composed of two (2) drainage areas and the stormwater runoff will continue to flow to one (1) design point, Flow to Wetlands (Design Point 1). Refer to Figure HYD-PR for the proposed conditions drainage area.

3.3 RESULTS OF ANALYSIS

A stormwater analysis was performed for the 24-hour 2-year, 10-year, 25-year, and 100-year storm events to determine that there will be no increase in peak stormwater runoff discharge rates offsite once the proposed construction is complete. Detailed calculations are attached in Appendix C. Compliance for existing and post-development conditions was evaluated for the site as a whole. A summary of the peak stormwater runoff rates is provided below.

As shown below in Table 3.1, post-development runoff rates from the Site do not exceed existing runoff rates for the 2, 10, and 25 year storm events. The 100 year event does exceed the predevelopment peak runoff rate. However, downstream flooding is not anticipated to be exacerbated as stormwater discharges to a large network of surrounding wetlands. Supporting calculations are provided in Appendix C.

TABLE 3.1 PROJECT STORMWATER RUNOFF RATES								
	Peak Runoff Rate (cfs)							
Design	2-Year		10-Year		25-Year		100-Year	
Point	Ex.	Prop.	Ex.	Prop.	Ex.	Prop.	Ex.	Prop.
1	0.7	0.5	1.3	1.3	4.2	2.5	16.0	18.0

cfs = cubic feet per second

4.0 STORMWATER CONTROL SYSTEM DESIGN CRITERIA

4.1 MASSDEP STORMWATER MANAGEMENT POLICY

Stormwater discharge from the proposed Project is subject to the Massachusetts DEP Stormwater Management Policy (the Policy). The Policy is designed "to protect the wetlands and waters of the Commonwealth from adverse impacts of storm water runoff." To accomplish this goal, the Policy establishes ten (10) performance standards to control stormwater quantity and quality. These standards establish the level of required controls that can be achieved with site planning, structural and non-structural controls, and other best management practices (BMPs). The Stormwater Checklist is provided in Appendix A. Stormwater modeling methodology is discussed in detail in Section 3.0. Results of the stormwater modeling of the existing and proposed conditions are provided as Appendix C.

4.1.1 Stormwater Management Standards

The following section documents compliance with the MassDEP Stormwater Management Standards.

Standard 1

No new stormwater conveyances (e.g., outfalls) may discharge untreated stormwater directly to or cause erosion in wetlands or waters of the Commonwealth.

The project is designed to limit to the extent possible new stormwater conveyances that could discharge untreated stormwater into, or cause erosion to, wetlands or waters of the Commonwealth. The proposed project captures and provides treatment for all new impervious paved areas and will discharge clean runoff to the existing offsite wetlands.

Stormwater runoff from the site will be conveyed through deep sump catch basins, that discharge into water quality units prior to discharging to a sediment forebay and, ultimately, the wet basin. Each outfall will have riprap installed at the outlet to prevent scour.

Standard 2

Stormwater management systems must be designed so that post-development peak discharge rates do not exceed pre-development peak discharge rates. This Standard may be waived for discharges to land subject to coastal storm flowage as defined in 310 CMR 10.04.

The post-development peak discharge rate to design point 1, does not exceed the pre-development rate. Stormwater modeling methodology is discussed in detail in Section 3.0. The model output is provided as Appendix C. A summary of the model results are provided above in Table 3.1.

Standard 3

Loss of annual recharge to groundwater should be eliminated or minimized through the use of infiltration measures.. The annual recharge from the post-development site should approximate the annual recharge from the pre-development or existing site conditions, based on soil types.

An existing underground stormwater infiltration system receives all the stormwater discharge from the building roof resulting in approximately 4,360 CF of infiltration. Additional infiltration is not practicable at this site due to a high groundwater level.

Standard 4

For new development, stormwater management systems must be designed to remove 80% of the average annual load (post-development conditions) of Total Suspended Solids (TSS). It is presumed that this standard is met when:

- A. Suitable nonstructural practices for source control and pollution prevention are implemented;
- B. Stormwater management best practices (BMPs) are sized to capture the prescribed runoff volume; and
- C. Stormwater management BMPs are maintained as designed.

The proposed development proposes to utilize the existing deep sump catch basins that will discharge into new water quality units before ultimately discharging to the reconfigured detention basin. The detention basin will be converted to a wet basin that includes a sediment forebay and will maintain a permanent pool of water,

The estimated TSS removal rate from the proposed BMP pre-treatment train for the existing reconfigured detention basin exceeds the 80% requirement with approximately 92% TSS removal. Refer to Appendix C for the TSS removal spreadsheet. Supporting information is provided in Appendix C.

A comprehensive Operations and Maintenance Plan (O&M) has been developed and is included in Section 6.0 of this report.

Standard 5

Stormwater discharges from areas with higher potential pollutant loads require the use of specific stormwater management BMPs. The use of infiltration practices without pre-treatment is prohibited.

The site is not within areas with higher potential pollutant loads.

Standard 6

Stormwater discharges to critical areas must utilize certain stormwater management BMPs approved for critical areas. Critical areas are Outstanding Resources Waters (ORWs), shellfish beds, bathing beaches, cold water fisheries, and recharge areas for public water supplies.

The Site is not located within critical areas

Standard 7

Redevelopment of previously developed sites must meet the Stormwater Management Standards to the maximum extent practicable. Where it is not practicable to meet all the Standards, new (retrofitted or expanded) stormwater management systems must be designed to improve existing conditions.

This project is considered a new development due to the small increase in impervious coverage from existing conditions.

Standard 8

Erosion and sediment controls must be implemented to prevent impacts during construction, or land disturbance activities.

Erosion and sediment controls are integral to the project improvements. The plan includes Filter Fabric fence reinforced by staked straw bales, which will be installed down-gradient of the proposed work area. If necessary, a temporary stabilized construction exit will be constructed as well. Prior to, and during construction, the Site's Erosion and Sediment Control Plan, included in Section 5.0 of this report will be followed. These measures will be utilized throughout construction to prevent erosion, control sediments, and stabilize exposed soils as discussed in Section 5.0.

Standard 9

All stormwater management systems must have an operations and maintenance plan to ensure that systems function as designed.

A comprehensive Operations and Maintenance Plan (O&M) has been developed and is included in Section 6.0 of this report.

Standard 10

All illicit discharges to the stormwater management system are prohibited.

There are no known illicit discharges at the Site. If found, any illicit discharges will be eliminated, and the project will not be constructed with any illicit connections. An Illicit Discharge Statement is provided in Appendix D.

5.0 CONSTRUCTION SEDIMENTATION AND EROSION CONTROL PLAN

5.1 INTRODUCTION

The greatest potential for sediment generation will occur during the construction. An extensive erosion and sedimentation program is proposed and will be diligently implemented during construction of the project. The erosion control program will minimize erosion and sedimentation that could potentially impact resources areas. Water quality will be maintained by minimizing erosion of exposed soils and siltation. Erosion control barriers will be installed and exposed soil areas re-vegetated as soon as possible after work in an area is completed.

Responsible Party for Plan Compliance:

NSTAR ELECTRIC COMPANY DBA EVERSOURCE ENERGY 247 STATION DRIVE WESTWOOD, MA 02090

Contact: Jason St. Martin (Facilities Operation Manager) Phone: 617-780-9365

5.2 SITE DESCRIPTION

The propsoed site will become an Eversource Training Facility and will serve as a staging area for emergency response vehicles on an as needed basis. The proposed improvements at the site will include approximately 2.3 acres of new gravel area to serve as various electrified/non-electrified training zones with associated permanent equipment, poles, and structures. In addition, the existing cinema on site will be redeveloped into an indoor training area with classrooms and offices.

Soil disturbing activities will include installing perimeter and other sediment controls, finish grading of the site, followed by the resizing of the stormwater detention system, pavement area, utilities, curbing and sidewalks. Upon completion of construction, landscaping will be installed and all disturbed areas will be stabilized.

5.3 SEQUENCE OF MAJOR ACTIVITIES

- 1. Notify all appropriate town departments prior to construction commencement in accordance with all approvals
- 2. Flag limits of construction necessary to facilitate a pre-construction meeting.

- Hold a pre-construction meeting. Remember to notify "Call Before You Dig" (1-800-922-4455)
- 4. Install all necessary siltation barriers and inlet protection as shown on the design drawings.
- 5. Placed crushed stoned stabilized construction pad and set up construction trailers and fence
- 6. Demo existing parking islands/ remove existing light poles and install new binder asphalt within demoed parking island areas per Erosion & Sedimentation Control/Demolition Plan
- 7. Clear and grub/remove trees, as shown on the design drawings.
- 8. Perform excavation and install new drainage structures and any subsurface utilities
- 9. Resize and reshape existing grassed water quality swale and detention basin area as shown on the design drawings.
- 10. Construct training zone areas with associated permanent equipment, poles, and structures.
- 11. Loam and seed all disturbed areas and install proposed final landscaping.
- 12. Remove existing erosion control measures upon site stabilization.

5.4 EROSION AND SEDIMENT CONTROLS

In addition to the perimeter controls, erosion control will be accomplished using temporary measures such as tracking entrance, seeding or mulching, spraying of liquid stabilizers or any combination of these measures. Seeds should be applied at a rate of 2 lbs/ 1000 square feet at a depth of 1/2 inch. Soil netting or covering should be used in extreme conditions.

Only minor stockpiling of soils will be allowed on site. Soil stockpiles will be ringed with hay bales/ silt fencing or covered in extreme conditions.

Maintenance / Inspection Procedures for Erosion and Sediment Controls

- Construction to commence in a phased manner.
- All control measures will be inspected at least once each week and following any storm event of 0.5 inches of precipitation or greater.
- All measures will be maintained in good working order; if repair is necessary, it will be initiated within 24 hours of report.
- Built up sediment will be removed from erosion control when it has reached one-third the height of the fence or bale.
- Silt fence will be inspected for depth of sediment, tears and to see if fabric is securely attached to the fence post, are firmly in the ground.
- Any temporary sediment basin used will be inspected for depth of sediment. Any buildup of sediment will be removed when it reaches 10% of the design capacity or at the end of the project completion.
- Temporary and permanent seeding and planting will be inspected for bare spots, washouts and healthy growth.
- A maintenance and inspection report will be made after each inspection. A copy of the report form to be completed by the inspector and kept on site.

• Construction site supervisor will be responsible for training workers in all inspection and maintenance practices necessary for keeping erosion and sediment controls in good working order.

5.5 OTHER CONTROLS

5.5.1 Waste Disposal

All waste materials will be disposed of offsite in accordance with all applicable local, State, and Federal regulations. No construction waste is to be buried on site. All personnel will be instructed regarding the correct procedure for waste disposal. The individual who manages the day-to-day site operations will be responsible for seeing that these procedures are followed.

5.5.2 Hazardous Waste

All hazardous waste materials will be disposed of in a manner specified by local, State, and Federal regulations and in accordance with any manufacturer's recommendations.

5.5.3 Sanitary Waste

All sanitary waste will be collected in portable units installed on site. The portable units will be cleaned and emptied by a qualified licensed contractor.

5.5.4 Concrete Waste

All concrete washings will be disposed on in a designated area away from wetlands and any property line. When the concrete hardens it be removed from the site.

5.6 POLLUTION AND SPILL PREVENTION

5.6.1 Materials

The following materials are anticipated to be present onsite during construction:

- General construction materials
- Asphalt/concrete
- Paint
- Petroleum-based products
- Cleaning solvents

5.6.2 Material Management Practices

Good Housekeeping Practices

- Store only enough materials needed for current construction activities.
- All materials that are stored outside will be stored in a neat, orderly manner, in the original containers.
- Materials will be kept in their original containers with manufacturer's labels.
- Whenever possible, all materials should be used before disposing the container.
- The site contractor shall be responsible for daily inspections to ensure proper handling and disposal of materials on site.

Product Specific Practices

Petroleum Products:

- Refueling vehicles shall be DOT certified and shall contain SPCC Plans in place along with emergency equipment to contain and clean up spills.
- All on site construction vehicles shall be inspected for leaks and receive regular preventive maintenance to reduce the chance of leakage.
- Petroleum-based products will be stored in tightly sealed containers, which are properly marked.

Paints:

- All containers will be tightly sealed and stored when not required for use.
- All procedures will be followed to minimize spills and to keep products in the original containers.

Concrete Trucks:

• The site contractor is responsible for designating a safe area, away from abutting property and resource areas, for excess concrete disposal.

Product Specific Practices

In addition to the good housekeeping and material management practices discussed in the previous sections of this plan, the following practices will be followed for spill prevention and cleanup during construction:

- Manufacturer recommended methods for spill clean up will be clearly posted and site personnel will be made aware of the procedures and the location of the information and cleanup supplies.
- All spills will be cleaned up immediately after discovery.
- In any case or threat of explosion or life threatening condition, all personnel shall evacuate the area to safety and then contact the local fire department for assistance.

- The spill area will be ventilated and personnel will wear appropriate protective clothing to prevent injury from contact with a hazardous substance.
- The site contractor shall be responsible for spill prevention and cleanup and will designate at least three personnel who will receive spill prevention and cleanup training. The names of the assigned three personnel will be posted in the material storage area in the field office on site.

5.7 RECORD KEEPING

The following records will be maintained on the Site:

- 1. Dates when major grading activities occur,
- 2. Dates when construction activities temporarily or permanently cease on a portion of the Site,
- 3. Dates when stabilization measures are initiated, and
- 4. In addition, the following records will also be kept:
 - The Order of Conditions; and any additional permit conditions/approvals,
 - All inspection reports, and
 - Any spill reports.

6.0 OPERATIONS AND MAINTENANCE (O&M) PLAN

6.1 GENERAL

Stormwater management systems with multiple components, such as the one proposed for the project, assures the cleanest possible discharges of stormwater to the environment. However, these systems must be routinely maintained to keep them in good working order. Additionally, this plan identifies potential sources of pollution that may affect the quality of stormwater discharges and describes the implementation of Long-Term Pollution Prevention practices to reduce potential pollutants in stormwater discharge. The party identified below will be responsible for the operation and maintenance of the stormwater management system and Site. Schedules and procedures for inspection and maintenance of the existing and proposed stormwater management system components are provided in the following sections.

Responsible Party for Plan Compliance:

NSTAR ELECTRIC COMPANY DBA EVERSOURCE ENERGY 247 STATION DRIVE WESTWOOD, MA 02090

Contact: Jason St. Martin (Facilities Operation Manager) Phone: 617-780-9365

Emergency Contact Information:

Civil & Environmental Consultants, Inc. (774) 501-2176

Upon a transfer of ownership, if any, the future owner shall assume the responsibilities for compliance with this O&M Plan.

6.2 **ROUTINE INSPECTIONS**

Inspections of the stormwater management system as a whole, and of the individual components of the system, will be carried out on a routine basis in accordance with the schedule identified in Section 6.3. Components to be inspected include the catch basins and subsurface infiltration chambers. Each will be inspected for sediment buildup, presence of oil, color, and structural damage. The results of each inspection will be entered into an inspection log. Refer to Table 6.1 for the inspection log forms.

6.3 MAINTENANCE PLAN

The Responsible Party will incorporate a routine maintenance program to assure proper operation of the stormwater management system. The program will include the following maintenance activities:

Catch Basin Structures

- See the attached Manufacturer's instructions on operation and maintenance requirements and methodology.
- Inspect and clean four times per year or as required by manufacturer.
- Remove sediment and other trapped pollutants at whenever the depth of the deposits is greater than two feet.

Water Quality Units

- See the attached Manufacturer's instructions on operation and maintenance requirements and methodology.
- Inspect and clean twice per year or as required by manufacturer.
- Remove sediment and other trapped pollutants at the frequency or level specified by the manufacturer.

Sediment Forebay

- Inspect monthly for accumulated sediment, trash, and debris and remove it.
- Clean four times per year and when sediment depth is greater than 3 feet.

Wet Basin

- Inspect at least once per year to ensure it's operating as designed.
- Mow the embankments at least twice per year.
- Remove sediment from the basin as necessary, and at least once every 10 years.
- Emergency overflow pipes will be examined at least once each year and verified that no blockage has occurred.

Rip-Rap Outlet

- Inspect after the first several rainfall events and after any major storm events within the first year. After the first year, inspect regularly on an annual basis.
- Remove any sediment, trash, debris, leaves and grass clippings. Remove any tree seedlings before they become firmly established.
- Note and repair any erosion or low spots.

Infiltration Chamber

- See the attached Manufacturer's instructions on operation and maintenance requirements and methodology.
- Inspect and clean twice per year or as required by manufacturer.
- Remove sediment and other trapped pollutants at the frequency or level specified by the manufacturer.

6.4 LONG TERM POLLUTION PREVENTION MAINTENANCE

The Responsible Party will incorporate a routine maintenance program to ensure the continued effectiveness of the structural water quality controls. Maintenance will be performed based on the results of inspections in accordance with the schedules identified below. The program will include the following maintenance activities:

Maintenance of Pavement Systems

Regular maintenance of pavement surfaces will prevent pollutants such as oil and grease, trash, and sediments from entering the stormwater management system. The following practices should be performed:

- Sweep or vacuum asphalt pavement areas annually with a commercial cleaning unit and dispose of removed material.
- Routinely pick up and remove litter from the parking areas, islands, and perimeter landscaping.

Maintenance of Vegetated Areas

Proper maintenance of vegetated areas can prevent the pollution of stormwater runoff by controlling the source of pollutants such as suspended sediments, excess nutrients, and chemicals from landscape care products. Practices that should be followed under the regular maintenance of the vegetated landscape include:

- Inspect planted areas on a semi-annual basis and remove any litter.
- Maintain planted areas adjacent to pavement to prevent soil washout.
- Immediately clean any soil deposited on pavement.
- Re-seed bare areas: install appropriate erosion control measures when native soil is exposed, or erosion channels are forming.
- Plant alternative mixture of grass species in the event of unsuccessful establishment.
- Grass vegetation should not be cut to a height less than four inches.

- Pesticide/Herbicide Usage No pesticides are to be used unless a single spot treatment is required for a specific control application.
- Fertilizer usage should be avoided. If deemed necessary, slow-release fertilizer should be used. Fertilizer may be used to begin the establishment of vegetation in bare or damaged areas but should not be applied on a regular basis unless necessary.

Management of Snow and Ice

Should significant snow fall events occur, which result in stockpiled snow impacting the operation of the Project Site, through the temporary loss of parking or limiting access in any way, the property manager may choose to have snow removed from the site. All snow removal operations will be done in accordance with Massachusetts DEP guidelines BRPG01-01, effective date March 8, 2001.

Salt and Deicing Chemicals

The amount of salt and deicing chemicals to be used on the site shall be reduced to the minimum amount needed to provide safe pedestrian and vehicle travel. The following practices should be followed to control the amount of salt and deicing materials that come into contact with stormwater runoff:

- Devices used for spreading salt and deicing chemicals should be capable of varying the rate of application based on the site-specific conditions.
- Sand and salt should be stockpiled under covered storage facilities that prevent precipitation and adjacent runoff from coming in contact with the deicing materials.

6.5 EMPLOYEE TRAINING

Training of personnel is essential to achieving proper operation and maintenance of the stormwater management system. Therefore, those Facility personnel who are responsible for operation and maintenance will be trained on the following subjects:

- Environmental laws and regulations relating to stormwater,
- The components and goals of the current Erosion and Sediment Control Plan,
- Site specific permit conditions and requirements,
- General Facility spill response procedures,
- General good housekeeping procedures, and
- General material management procedures.

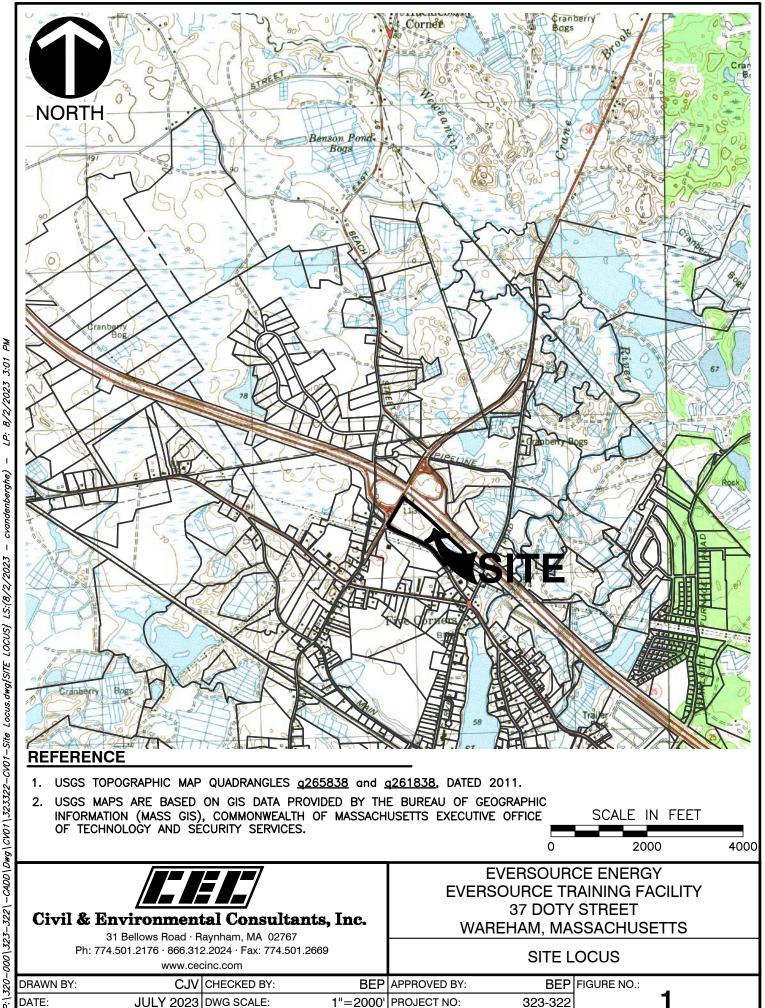
Refresher training sessions will be held once a year following the completion of the Site Compliance Evaluation.

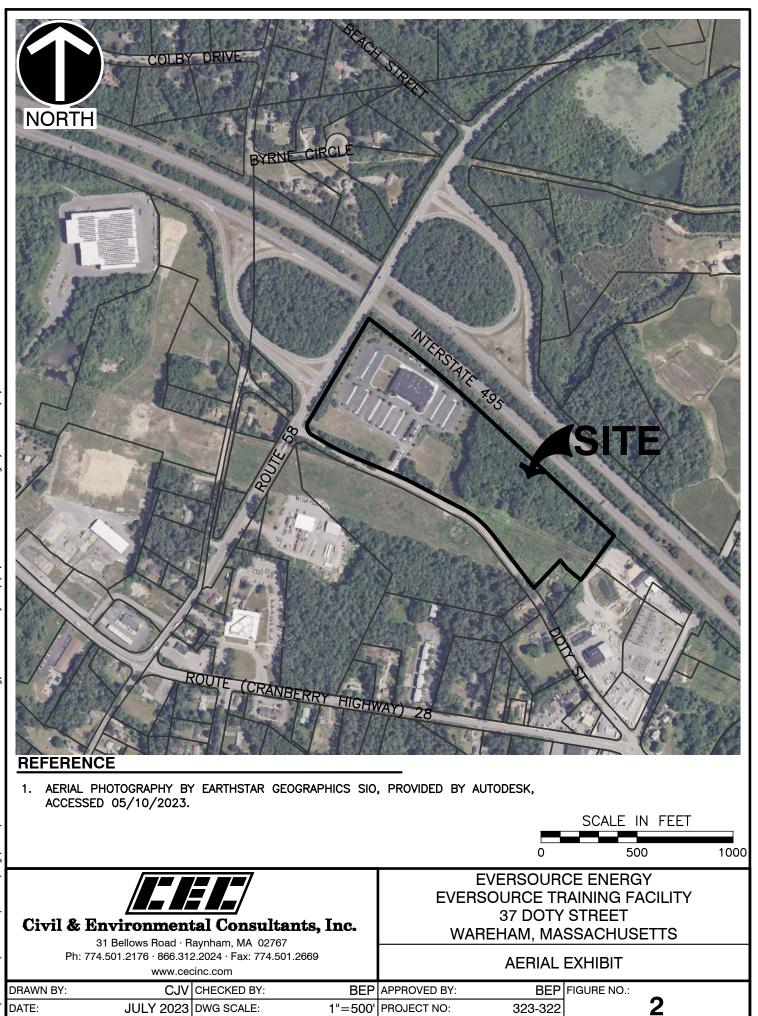
6.6 **RECORDKEEPING**

Records of inspections and maintenance shall be up to date and available for review and inspection, if requested

FIGURES

Figure 1 – Site Locus Figure 2 – Aerial Exhibit Figure 3 – FEMA Firmette Figure 4 – Critical Areas Map Figure HYD-EX – Existing Conditions Drainage Area Map Figure HYD-POST – Proposed Conditions Drainage Area Map



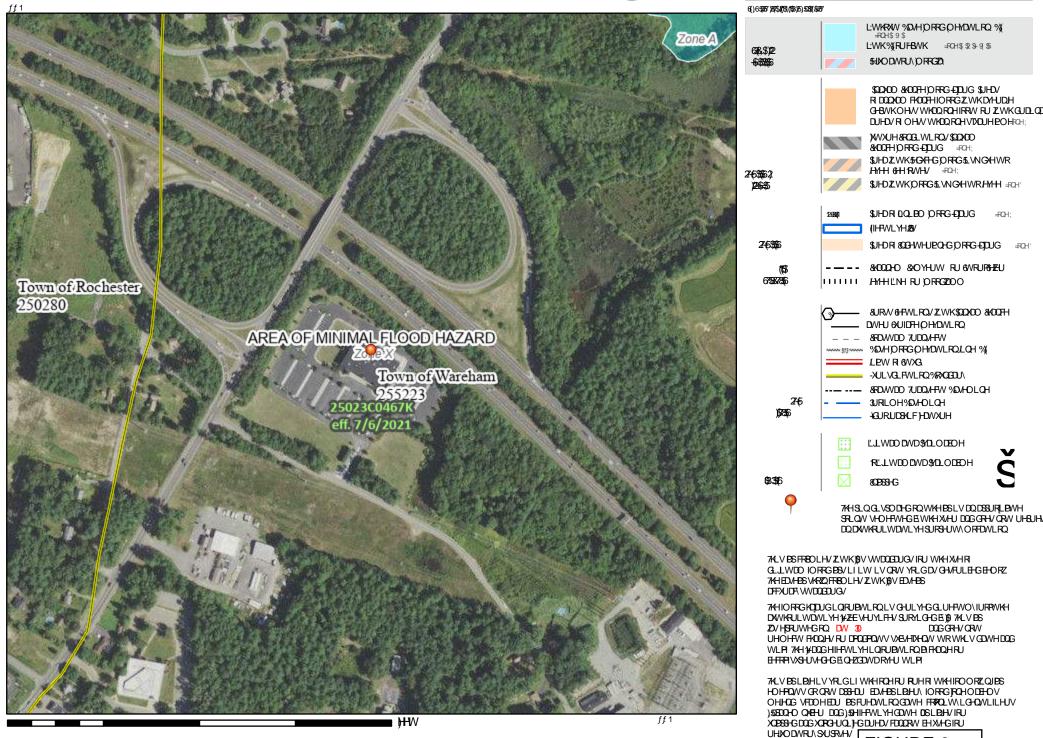


DWLRODO ORRGEDUGDHU)51WWH



HHOG

FIGURE 3



%DVHBS, BUHU\ 6RXUFH 886 DWL RODO DS

Critical Areas Map

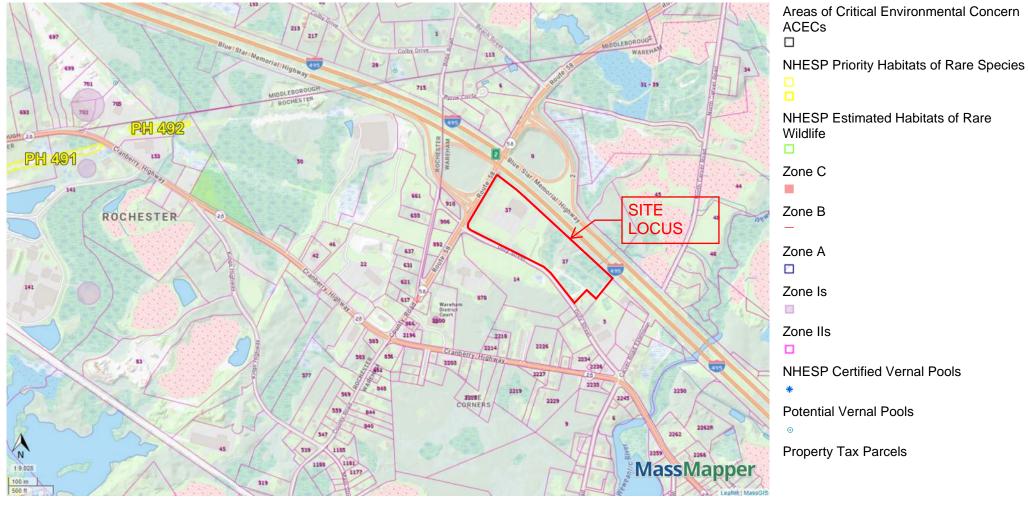
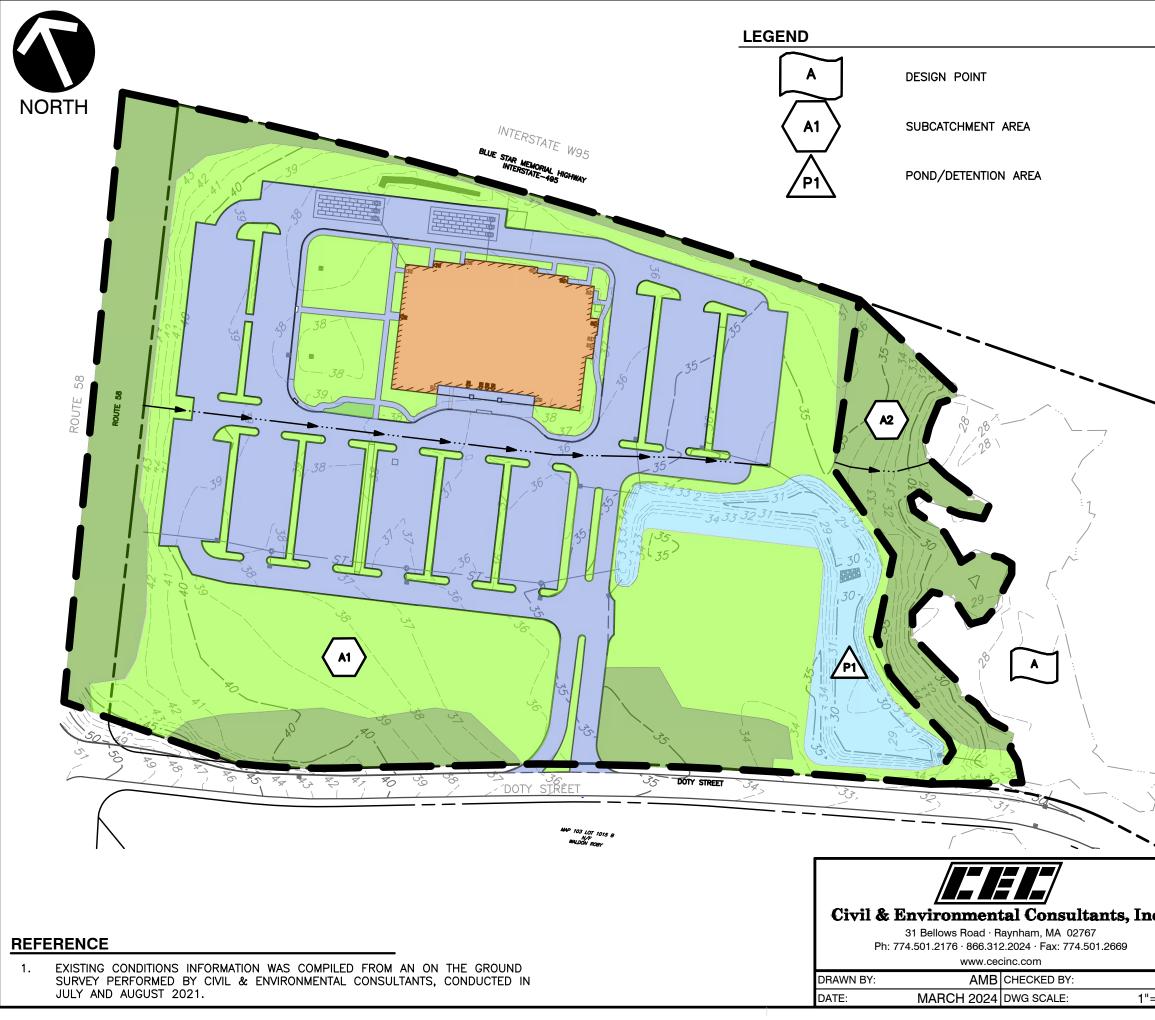


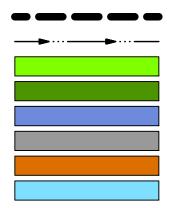
FIGURE 4



	SUBCATCHMENT BOUNDARY
── ►···· ─	TIME OF CONCENTRATION PATH
	VEGETATED AREA
	WOODED AREA
	PAVED AREA
	ROOF AREA
	WATER AREA
\rangle	SCALE IN FEET
-	
` `	0 100 200
FVFI	RSOURCE ENERGY
3	7 DOTY STREET
NC. WAREH	AM, MASSACHUSETTS
DR	AINAGE AREA MAP
	STING CONDITIONS
	BEP FIGURE NO.: 323-322 HYD-PRE
=100' PROJECT NO:	323-322 HYD-PRE



	SCALE IN FEET
nc.	EVERSOURCE ENERGY 37 DOTY STREET WAREHAM, MASSACHUSETTS
CJV	DRAINAGE AREA MAP PROPOSED CONDITIONS APPROVED BY: BEP FIGURE NO.:
	APPROVED BY: BEP FIGURE NO.: PROJECT NO: 323-322 HYD-POST



SUBCATCHMENT BOUNDARY TIME OF CONCENTRATION PA⁻ VEGETATED AREA WOODED AREA PAVED AREA GRAVEL AREA ROOF AREA WATER AREA

APPENDIX A

DEP STORMWATER CHECKLIST



Massachusetts Department of Environmental Protection Bureau of Resource Protection - Wetlands Program Checklist for Stormwater Report

A. Introduction

Important: When filling out forms on the computer, use only the tab key to move your cursor - do not use the return key.



A Stormwater Report must be submitted with the Notice of Intent permit application to document compliance with the Stormwater Management Standards. The following checklist is NOT a substitute for the Stormwater Report (which should provide more substantive and detailed information) but is offered here as a tool to help the applicant organize their Stormwater Management documentation for their Report and for the reviewer to assess this information in a consistent format. As noted in the Checklist, the Stormwater Report must contain the engineering computations and supporting information set forth in Volume 3 of the Massachusetts Stormwater Handbook. The Stormwater Report must be prepared and certified by a Registered Professional Engineer (RPE) licensed in the Commonwealth.

The Stormwater Report must include:

- The Stormwater Checklist completed and stamped by a Registered Professional Engineer (see page 2) that certifies that the Stormwater Report contains all required submittals.¹ This Checklist is to be used as the cover for the completed Stormwater Report.
- Applicant/Project Name
- Project Address
- Name of Firm and Registered Professional Engineer that prepared the Report
- Long-Term Pollution Prevention Plan required by Standards 4-6
- Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan required by Standard 8²
- Operation and Maintenance Plan required by Standard 9

In addition to all plans and supporting information, the Stormwater Report must include a brief narrative describing stormwater management practices, including environmentally sensitive site design and LID techniques, along with a diagram depicting runoff through the proposed BMP treatment train. Plans are required to show existing and proposed conditions, identify all wetland resource areas, NRCS soil types, critical areas, Land Uses with Higher Potential Pollutant Loads (LUHPPL), and any areas on the site where infiltration rate is greater than 2.4 inches per hour. The Plans shall identify the drainage areas for both existing and proposed conditions at a scale that enables verification of supporting calculations.

As noted in the Checklist, the Stormwater Management Report shall document compliance with each of the Stormwater Management Standards as provided in the Massachusetts Stormwater Handbook. The soils evaluation and calculations shall be done using the methodologies set forth in Volume 3 of the Massachusetts Stormwater Handbook.

To ensure that the Stormwater Report is complete, applicants are required to fill in the Stormwater Report Checklist by checking the box to indicate that the specified information has been included in the Stormwater Report. If any of the information specified in the checklist has not been submitted, the applicant must provide an explanation. The completed Stormwater Report Checklist and Certification must be submitted with the Stormwater Report.

¹ The Stormwater Report may also include the Illicit Discharge Compliance Statement required by Standard 10. If not included in the Stormwater Report, the Illicit Discharge Compliance Statement must be submitted prior to the discharge of stormwater runoff to the post-construction best management practices.

² For some complex projects, it may not be possible to include the Construction Period Erosion and Sedimentation Control Plan in the Stormwater Report. In that event, the issuing authority has the discretion to issue an Order of Conditions that approves the project and includes a condition requiring the proponent to submit the Construction Period Erosion and Sedimentation Control Plan before commencing any land disturbance activity on the site.



Massachusetts Department of Environmental Protection Bureau of Resource Protection - Wetlands Program Checklist for Stormwater Report

B. Stormwater Checklist and Certification

The following checklist is intended to serve as a guide for applicants as to the elements that ordinarily need to be addressed in a complete Stormwater Report. The checklist is also intended to provide conservation commissions and other reviewing authorities with a summary of the components necessary for a comprehensive Stormwater Report that addresses the ten Stormwater Standards.

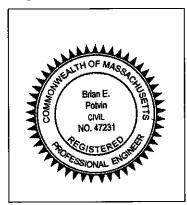
Note: Because stormwater requirements vary from project to project, it is possible that a complete Stormwater Report may not include information on some of the subjects specified in the Checklist. If it is determined that a specific item does not apply to the project under review, please note that the item is not applicable (N.A.) and provide the reasons for that determination.

A complete checklist must include the Certification set forth below signed by the Registered Professional Engineer who prepared the Stormwater Report.

Registered Professional Engineer's Certification

I have reviewed the Stormwater Report, including the soil evaluation, computations, Long-term Pollution Prevention Plan, the Construction Period Erosion and Sedimentation Control Plan (if included), the Longterm Post-Construction Operation and Maintenance Plan, the Illicit Discharge Compliance Statement (if included) and the plans showing the stormwater management system, and have determined that they have been prepared in accordance with the requirements of the Stormwater Management Standards as further elaborated by the Massachusetts Stormwater Handbook. I have also determined that the information presented in the Stormwater Checklist is accurate and that the information presented in the Stormwater Report accurately reflects conditions at the site as of the date of this permit application.

Registered Professional Engineer Block and Signature



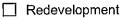
3/8/24 n

Signature and Date

Checklist

Project Type: Is the application for new development, redevelopment, or a mix of new and redevelopment?

New development



Mix of New Development and Redevelopment



Checklist (continued)

LID Measures: Stormwater Standards require LID measures to be considered. Document what environmentally sensitive design and LID Techniques were considered during the planning and design of the project:

\bowtie	No disturbance to any Wetland Resource Areas
	Site Design Practices (e.g. clustered development, reduced frontage setbacks)
	Reduced Impervious Area (Redevelopment Only)
	Minimizing disturbance to existing trees and shrubs
	LID Site Design Credit Requested:
	Credit 1
	Credit 2
	Credit 3
	Use of "country drainage" versus curb and gutter conveyance and pipe
	Bioretention Cells (includes Rain Gardens)
	Constructed Stormwater Wetlands (includes Gravel Wetlands designs)
	Treebox Filter
	Water Quality Swale
	Grass Channel
	Green Roof
	Other (describe):
0 1-	a devid 4. Mac Marca Harfan eta di D'a alteratoria

Standard 1: No New Untreated Discharges

No new untreated discharges

- Outlets have been designed so there is no erosion or scour to wetlands and waters of the Commonwealth
- Supporting calculations specified in Volume 3 of the Massachusetts Stormwater Handbook included.



Checklist (continued)

Standard 2: Peak Rate Attenuation

- Standard 2 waiver requested because the project is located in land subject to coastal storm flowage and stormwater discharge is to a wetland subject to coastal flooding.
- Evaluation provided to determine whether off-site flooding increases during the 100-year 24-hour storm.

Calculations provided to show that post-development peak discharge rates do not exceed predevelopment rates for the 2-year and 10-year 24-hour storms. If evaluation shows that off-site flooding increases during the 100-year 24-hour storm, calculations are also provided to show that post-development peak discharge rates do not exceed pre-development rates for the 100-year 24hour storm.

Standard 3: Recharge

Soil Analysis provided.

- Required Recharge Volume calculation provided.
- Required Recharge volume reduced through use of the LID site Design Credits.
- Sizing the infiltration, BMPs is based on the following method: Check the method used.

Static	Simple Dynamic
--------	----------------

Dynamic Field¹

- Runoff from all impervious areas at the site discharging to the infiltration BMP.
- Runoff from all impervious areas at the site is *not* discharging to the infiltration BMP and calculations are provided showing that the drainage area contributing runoff to the infiltration BMPs is sufficient to generate the required recharge volume.

Recharge BMPs have been sized to infiltrate the Required Recharge Volume.

Recharge BMPs have been sized to infiltrate the Required Recharge Volume only to the maximum
extent practicable for the following reason:

- Site is comprised solely of C and D soils and/or bedrock at the land surface
- M.G.L. c. 21E sites pursuant to 310 CMR 40.0000
- Solid Waste Landfill pursuant to 310 CMR 19.000
- Project is otherwise subject to Stormwater Management Standards only to the maximum extent practicable.
- Calculations showing that the infiltration BMPs will drain in 72 hours are provided.

Property includes a M.G.L. c. 21E site or a solid waste landfill and a mounding analysis is included.

¹ 80% TSS removal is required prior to discharge to infiltration BMP if Dynamic Field method is used.



Checklist (continued)

Standard 3: Recharge (continued)

The infiltration BMP is used to attenuate peak flows during storms greater than or equal to the 10year 24-hour storm and separation to seasonal high groundwater is less than 4 feet and a mounding analysis is provided.

Documentation is provided showing that infiltration BMPs do not adversely impact nearby wetland resource areas.

Standard 4: Water Quality

The Long-Term Pollution Prevention Plan typically includes the following:

- Good housekeeping practices;
- Provisions for storing materials and waste products inside or under cover;
- Vehicle washing controls;
- Requirements for routine inspections and maintenance of stormwater BMPs;
- Spill prevention and response plans;
- · Provisions for maintenance of lawns, gardens, and other landscaped areas;
- Requirements for storage and use of fertilizers, herbicides, and pesticides;
- Pet waste management provisions;
- Provisions for operation and management of septic systems;
- Provisions for solid waste management;
- Snow disposal and plowing plans relative to Wetland Resource Areas;
- Winter Road Salt and/or Sand Use and Storage restrictions;
- Street sweeping schedules;
- Provisions for prevention of illicit discharges to the stormwater management system;
- Documentation that Stormwater BMPs are designed to provide for shutdown and containment in the event of a spill or discharges to or near critical areas or from LUHPPL;
- Training for staff or personnel involved with implementing Long-Term Pollution Prevention Plan;
- List of Emergency contacts for implementing Long-Term Pollution Prevention Plan.
- A Long-Term Pollution Prevention Plan is attached to Stormwater Report and is included as an attachment to the Wetlands Notice of Intent.
- ☐ Treatment BMPs subject to the 44% TSS removal pretreatment requirement and the one inch rule for calculating the water quality volume are included, and discharge:
 - is within the Zone II or Interim Wellhead Protection Area
 - is near or to other critical areas
 - is within soils with a rapid infiltration rate (greater than 2.4 inches per hour)
 - involves runoff from land uses with higher potential pollutant loads.
- The Required Water Quality Volume is reduced through use of the LID site Design Credits.
- Calculations documenting that the treatment train meets the 80% TSS removal requirement and, if applicable, the 44% TSS removal pretreatment requirement, are provided.



Checklist (continue

Standard 4: Water Quality (continued)

- The BMP is sized (and calculations provided) based on:
 - The 1/2" or 1" Water Quality Volume or
 - The equivalent flow rate associated with the Water Quality Volume and documentation is provided showing that the BMP treats the required water quality volume.
- The applicant proposes to use proprietary BMPs, and documentation supporting use of proprietary BMP and proposed TSS removal rate is provided. This documentation may be in the form of the propriety BMP checklist found in Volume 2, Chapter 4 of the Massachusetts Stormwater Handbook and submitting copies of the TARP Report, STEP Report, and/or other third party studies verifying performance of the proprietary BMPs.
- A TMDL exists that indicates a need to reduce pollutants other than TSS and documentation showing that the BMPs selected are consistent with the TMDL is provided.

Standard 5: Land Uses With Higher Potential Pollutant Loads (LUHPPLs)

- The NPDES Multi-Sector General Permit covers the land use and the Stormwater Pollution Prevention Plan (SWPPP) has been included with the Stormwater Report.
- The NPDES Multi-Sector General Permit covers the land use and the SWPPP will be submitted **prior to** the discharge of stormwater to the post-construction stormwater BMPs.
- The NPDES Multi-Sector General Permit does *not* cover the land use.
- LUHPPLs are located at the site and industry specific source control and pollution prevention measures have been proposed to reduce or eliminate the exposure of LUHPPLs to rain, snow, snow melt and runoff, and been included in the long term Pollution Prevention Plan.
- All exposure has been eliminated.
- All exposure has *not* been eliminated and all BMPs selected are on MassDEP LUHPPL list.
- The LUHPPL has the potential to generate runoff with moderate to higher concentrations of oil and grease (e.g. all parking lots with >1000 vehicle trips per day) and the treatment train includes an oil grit separator, a filtering bioretention area, a sand filter or equivalent.

Standard 6: Critical Areas

- The discharge is near or to a critical area and the treatment train includes only BMPs that MassDEP has approved for stormwater discharges to or near that particular class of critical area.
- Critical areas and BMPs are identified in the Stormwater Report.



Checklist (continued)

Standard 7: Redevelopments and Other Projects Subject to the Standards only to the maximum extent practicable

- The project is subject to the Stormwater Management Standards only to the maximum Extent Practicable as a:
 - Limited Project
 - Small Residential Projects: 5-9 single family houses or 5-9 units in a multi-family development provided there is no discharge that may potentially affect a critical area.
 - Small Residential Projects: 2-4 single family houses or 2-4 units in a multi-family development with a discharge to a critical area
 - Marina and/or boatyard provided the hull painting, service and maintenance areas are protected from exposure to rain, snow, snow melt and runoff
 - Bike Path and/or Foot Path
 - Redevelopment Project
 - Redevelopment portion of mix of new and redevelopment.
- Certain standards are not fully met (Standard No. 1, 8, 9, and 10 must always be fully met) and an explanation of why these standards are not met is contained in the Stormwater Report.
- The project involves redevelopment and a description of all measures that have been taken to improve existing conditions is provided in the Stormwater Report. The redevelopment checklist found in Volume 2 Chapter 3 of the Massachusetts Stormwater Handbook may be used to document that the proposed stormwater management system (a) complies with Standards 2, 3 and the pretreatment and structural BMP requirements of Standards 4-6 to the maximum extent practicable and (b) improves existing conditions.

Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan must include the following information:

- Narrative;
- Construction Period Operation and Maintenance Plan;
- Names of Persons or Entity Responsible for Plan Compliance;
- Construction Period Pollution Prevention Measures;
- Erosion and Sedimentation Control Plan Drawings;
- Detail drawings and specifications for erosion control BMPs, including sizing calculations;
- Vegetation Planning;
- Site Development Plan;
- Construction Sequencing Plan;
- Sequencing of Erosion and Sedimentation Controls;
- Operation and Maintenance of Erosion and Sedimentation Controls;
- Inspection Schedule;
- Maintenance Schedule;
- Inspection and Maintenance Log Form.
- A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan containing the information set forth above has been included in the Stormwater Report.



Checklist (continued)

Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control (continued)

- ☐ The project is highly complex and information is included in the Stormwater Report that explains why it is not possible to submit the Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan with the application. A Construction Period Pollution Prevention and Erosion and Sedimentation Control has *not* been included in the Stormwater Report but will be submitted *before* land disturbance begins.
- The project is *not* covered by a NPDES Construction General Permit.
- The project is covered by a NPDES Construction General Permit and a copy of the SWPPP is in the Stormwater Report.
- The project is covered by a NPDES Construction General Permit but no SWPPP been submitted. The SWPPP will be submitted BEFORE land disturbance begins.

Standard 9: Operation and Maintenance Plan

- The Post Construction Operation and Maintenance Plan is included in the Stormwater Report and includes the following information:
 - Name of the stormwater management system owners;
 - Party responsible for operation and maintenance;
 - Schedule for implementation of routine and non-routine maintenance tasks;
 - Plan showing the location of all stormwater BMPs maintenance access areas;
 - Description and delineation of public safety features;
 - Estimated operation and maintenance budget; and
 - Operation and Maintenance Log Form.
- The responsible party is *not* the owner of the parcel where the BMP is located and the Stormwater Report includes the following submissions:
 - A copy of the legal instrument (deed, homeowner's association, utility trust or other legal entity) that establishes the terms of and legal responsibility for the operation and maintenance of the project site stormwater BMPs;
 - A plan and easement deed that allows site access for the legal entity to operate and maintain BMP functions.

Standard 10: Prohibition of Illicit Discharges

- The Long-Term Pollution Prevention Plan includes measures to prevent illicit discharges;
- An Illicit Discharge Compliance Statement is attached;
- NO Illicit Discharge Compliance Statement is attached but will be submitted *prior to* the discharge of any stormwater to post-construction BMPs.

APPENDIX B

GEOTECHNICAL INFORMATION

NRCS Soil Resource Report

NRCS Soil Resource Report

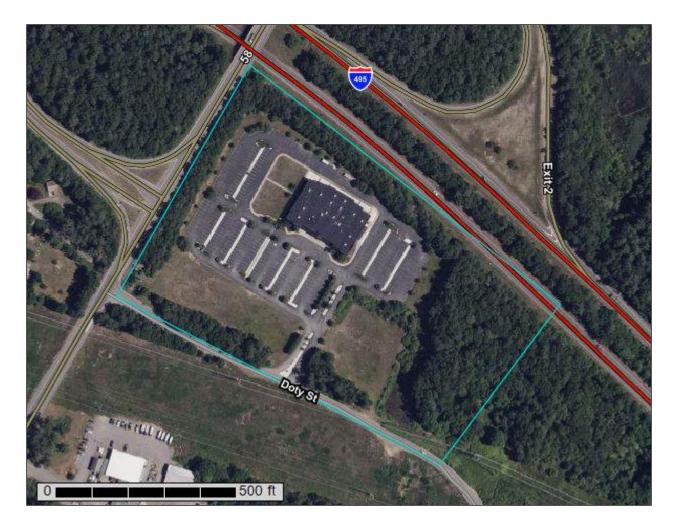


United States Department of Agriculture



Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Plymouth County, Massachusetts



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/? cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

The U.S. Department of Agriculture (USDA) prohibits discrimination in all its programs and activities on the basis of race, color, national origin, age, disability, and where applicable, sex, marital status, familial status, parental status, religion, sexual orientation, genetic information, political beliefs, reprisal, or because all or a part of an individual's income is derived from any public assistance program. (Not all prohibited bases apply to all programs.) Persons with disabilities who require

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Plymouth County, Massachusetts	
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253B—Hinckley loamy sand, 3 to 8 percent slopes	11
256A—Deerfield loamy fine sand, 0 to 3 percent slopes	13
259A—Carver loamy coarse sand, 0 to 3 percent slopes	14
259B—Carver loamy coarse sand, 3 to 8 percent slopes	16
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Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



	MAP L	EGEND)	MAP INFORMATION
Area of Inte	e rest (AOI) Area of Interest (AOI)	8	Spoil Area Stony Spot	The soil surveys that comprise your AOI were mapped at 1:12,000.
Soils	Soil Map Unit Polygons	Ø,	Very Stony Spot	Warning: Soil Map may not be valid at this scale.
ĩ	Soil Map Unit Lines Soil Map Unit Points	\$ ⊳	Wet Spot Other	Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of
Special F	Special Point Features Blowout Water F		Special Line Features itures Streams and Canals	contrasting soils that could have been shown at a more detailed scale.
X X	Borrow Pit Clay Spot	Transport		Please rely on the bar scale on each map sheet for map measurements.
☆ ¥	Closed Depression Gravel Pit	~	 ✓ Interstate Highways ✓ US Routes ✓ Web S 	Source of Map: Natural Resources Conservation Service Web Soil Survey URL:
.: ©	Gravelly Spot Landfill	*	Major Roads Local Roads	Coordinate System: Web Mercator (EPSG:3857) Maps from the Web Soil Survey are based on the Web Mercator
۸. جه	Lava Flow Marsh or swamp Mine or Quarry	Background	ground Aerial Photography	projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.
0	Miscellaneous Water Perennial Water			This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.
× +	Rock Outcrop Saline Spot			Soil Survey Area: Plymouth County, Massachusetts Survey Area Data: Version 15, Sep 9, 2022
:: =	Sandy Spot Severely Eroded Spot			Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.
♦ ≫	Sinkhole Slide or Slip			Date(s) aerial images were photographed: Jun 10, 2022—Jun 30, 2022
ø	Sodic Spot			The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Symbol Map Unit Name		Acres in AOI	Percent of AOI		
253A	Hinckley loamy sand, 0 to 3 percent slopes	4.1	26.2%		
253B	Hinckley loamy sand, 3 to 8 percent slopes	2.3	14.8%		
256A	Deerfield loamy fine sand, 0 to 3 percent slopes	1.9	12.2%		
259A	Carver loamy coarse sand, 0 to 3 percent slopes	3.2	20.6%		
259B	Carver loamy coarse sand, 3 to 8 percent slopes	1.9	12.5%		
321A	Birchwood sand, 0 to 3 percent slopes, very stony	1.9	11.9%		
430C	Barnstable loamy sand, 8 to 15 percent slopes	0.0	0.0%		
656B	Udorthents - Urban land complex, 0 to 8 percent slopes	0.3	1.7%		
Totals for Area of Interest	·	15.6	100.0%		

Map Unit Legend

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas

are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Plymouth County, Massachusetts

253A—Hinckley loamy sand, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 2svm7 Elevation: 0 to 1,420 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 240 days Farmland classification: Farmland of statewide importance

Map Unit Composition

Hinckley and similar soils: 85 percent *Minor components:* 15 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Hinckley

Setting

Landform: Outwash terraces, outwash plains, kame terraces, outwash deltas Landform position (three-dimensional): Tread Down-slope shape: Concave, convex, linear Across-slope shape: Convex, linear, concave Parent material: Sandy and gravelly glaciofluvial deposits derived from gneiss and/or granite and/or schist

Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material *A - 1 to 8 inches:* loamy sand *Bw1 - 8 to 11 inches:* gravelly loamy sand *Bw2 - 11 to 16 inches:* gravelly loamy sand *BC - 16 to 19 inches:* very gravelly loamy sand

C - 19 to 65 inches: very gravelly sand

Properties and qualities

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Excessively drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very high (1.42 to 99.90 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water supply, 0 to 60 inches: Low (about 3.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3s Hydrologic Soil Group: A Ecological site: F144AY022MA - Dry Outwash Hydric soil rating: No

Minor Components

Windsor

Percent of map unit: 5 percent Landform: Outwash deltas, kame terraces, outwash terraces Landform position (three-dimensional): Tread Down-slope shape: Concave, convex, linear Across-slope shape: Convex, linear, concave Hydric soil rating: No

Sudbury

Percent of map unit: 5 percent Landform: Outwash deltas, outwash terraces, kame terraces Landform position (three-dimensional): Tread Down-slope shape: Concave, convex, linear Across-slope shape: Convex, linear, concave Hydric soil rating: No

Merrimac

Percent of map unit: 5 percent Landform: Outwash deltas, outwash terraces, kame terraces Landform position (three-dimensional): Tread Down-slope shape: Concave, convex, linear Across-slope shape: Convex, linear, concave Hydric soil rating: No

253B—Hinckley loamy sand, 3 to 8 percent slopes

Map Unit Setting

National map unit symbol: 2svm8 Elevation: 0 to 1,430 feet Mean annual precipitation: 36 to 53 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 250 days Farmland classification: Farmland of statewide importance

Map Unit Composition

Hinckley and similar soils: 85 percent *Minor components:* 15 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Hinckley

Setting

Landform: Outwash deltas, outwash terraces, kames, kame terraces, moraines, eskers, outwash plains

Landform position (two-dimensional): Summit, shoulder, backslope, footslope Landform position (three-dimensional): Nose slope, side slope, base slope, crest, riser, tread

Down-slope shape: Concave, convex, linear

Across-slope shape: Convex, linear, concave

Parent material: Sandy and gravelly glaciofluvial deposits derived from gneiss and/or granite and/or schist

Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material *A - 1 to 8 inches:* loamy sand *Bw1 - 8 to 11 inches:* gravelly loamy sand *Bw2 - 11 to 16 inches:* gravelly loamy sand *BC - 16 to 19 inches:* very gravelly loamy sand *C - 19 to 65 inches:* very gravelly sand

Properties and qualities

Slope: 3 to 8 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Excessively drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very high (1.42 to 99.90 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water supply, 0 to 60 inches: Very low (about 3.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3s Hydrologic Soil Group: A Ecological site: F144AY022MA - Dry Outwash Hydric soil rating: No

Minor Components

Windsor

Percent of map unit: 8 percent Landform: Outwash deltas, outwash terraces, moraines, eskers, kames, outwash plains, kame terraces Landform position (two-dimensional): Summit, shoulder, backslope, footslope Landform position (three-dimensional): Nose slope, side slope, base slope, crest, riser, tread

Down-slope shape: Concave, convex, linear *Across-slope shape:* Convex, linear, concave

Hydric soil rating: No

Sudbury

Percent of map unit: 5 percent

Landform: Outwash deltas, outwash terraces, moraines, outwash plains, kame terraces

Landform position (two-dimensional): Backslope, footslope

Landform position (three-dimensional): Head slope, side slope, base slope, tread Down-slope shape: Concave, linear Across-slope shape: Concave, linear

Hydric soil rating: No

Agawam

Percent of map unit: 2 percent

Custom Soil Resource Report

Landform: Outwash deltas, outwash terraces, moraines, eskers, kames, outwash plains, kame terraces
 Landform position (two-dimensional): Summit, shoulder, backslope, footslope
 Landform position (three-dimensional): Nose slope, side slope, base slope, crest, riser, tread
 Down-slope shape: Concave, convex, linear
 Across-slope shape: Convex, linear, concave
 Hydric soil rating: No

256A—Deerfield loamy fine sand, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 2xfg8 Elevation: 0 to 1,100 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 145 to 240 days Farmland classification: Farmland of statewide importance

Map Unit Composition

Deerfield and similar soils: 85 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Deerfield

Setting

Landform: Outwash terraces, outwash deltas, outwash plains, kame terraces Landform position (three-dimensional): Tread Down-slope shape: Concave, convex, linear Across-slope shape: Convex, linear, concave Parent material: Sandy outwash derived from granite, gneiss, and/or quartzite

Typical profile

Ap - 0 to 9 inches: loamy fine sand Bw - 9 to 25 inches: loamy fine sand BC - 25 to 33 inches: fine sand Cg - 33 to 60 inches: sand

Properties and qualities

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Moderately well drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very high (1.42 to 99.90 in/hr)
Depth to water table: About 15 to 37 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Sodium adsorption ratio, maximum: 11.0 Available water supply, 0 to 60 inches: Moderate (about 6.5 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2w Hydrologic Soil Group: A Ecological site: F144AY027MA - Moist Sandy Outwash Hydric soil rating: No

Minor Components

Windsor

Percent of map unit: 7 percent Landform: Outwash terraces, kame terraces, outwash deltas, outwash plains Landform position (three-dimensional): Tread Down-slope shape: Concave, convex, linear Across-slope shape: Convex, linear, concave Hydric soil rating: No

Wareham

Percent of map unit: 5 percent Landform: Drainageways, depressions Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

Sudbury

Percent of map unit: 2 percent Landform: Outwash plains, kame terraces, outwash deltas, outwash terraces Landform position (three-dimensional): Tread Down-slope shape: Concave, convex, linear Across-slope shape: Convex, linear, concave Hydric soil rating: No

Ninigret

Percent of map unit: 1 percent Landform: Outwash terraces, kame terraces, outwash plains Landform position (three-dimensional): Tread Down-slope shape: Linear, convex Across-slope shape: Concave, convex Hydric soil rating: No

259A—Carver loamy coarse sand, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 2y07s Elevation: 0 to 990 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 240 days Farmland classification: Not prime farmland

Map Unit Composition

Carver, loamy coarse sand, and similar soils: 80 percent *Minor components:* 20 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Carver, Loamy Coarse Sand

Setting

Landform: Moraines, outwash plains Landform position (two-dimensional): Summit, shoulder Landform position (three-dimensional): Side slope, crest, tread Down-slope shape: Convex, linear Across-slope shape: Linear Parent material: Sandy glaciofluvial deposits

Typical profile

Oi - 0 to 2 inches: slightly decomposed plant material *Oe - 2 to 3 inches:* moderately decomposed plant material *A - 3 to 7 inches:* loamy coarse sand *E - 7 to 10 inches:* coarse sand *Bw1 - 10 to 15 inches:* coarse sand *Bw2 - 15 to 28 inches:* coarse sand *BC - 28 to 32 inches:* coarse sand *C - 32 to 67 inches:* coarse sand

Properties and qualities

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Excessively drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very high (1.42 to 14.17 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water supply, 0 to 60 inches: Low (about 4.5 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3s Hydrologic Soil Group: A Ecological site: F149BY005MA - Dry Outwash Hydric soil rating: No

Minor Components

Deerfield

Percent of map unit: 10 percent Landform: Outwash terraces, outwash deltas, outwash plains, kame terraces Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Concave Hydric soil rating: No

Hinckley

Percent of map unit: 5 percent

Landform: Outwash deltas, outwash terraces, moraines, eskers, kames, outwash plains, kame terraces

Landform position (two-dimensional): Summit, shoulder, backslope, footslope, toeslope

Landform position (three-dimensional): Head slope, nose slope, side slope, crest, riser, tread

Down-slope shape: Convex *Across-slope shape:* Convex

Hydric soil rating: No

Merrimac

Percent of map unit: 3 percent Landform: Outwash terraces, kame terraces, outwash deltas Landform position (three-dimensional): Riser, tread Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

Mashpee

Percent of map unit: 2 percent Landform: Depressions, drainageways, terraces Landform position (three-dimensional): Tread Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

259B—Carver loamy coarse sand, 3 to 8 percent slopes

Map Unit Setting

National map unit symbol: 2y07t Elevation: 0 to 240 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 240 days Farmland classification: Not prime farmland

Map Unit Composition

Carver, loamy coarse sand, and similar soils: 80 percent *Minor components:* 20 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Carver, Loamy Coarse Sand

Setting

Landform: Moraines, outwash plains Landform position (two-dimensional): Summit, shoulder, backslope, footslope, toeslope Landform position (three-dimensional): Head slope, nose slope, side slope, crest, tread Down-slope shape: Convex, linear Across-slope shape: Linear Parent material: Sandy glaciofluvial deposits

Typical profile

Oi - 0 to 2 inches: slightly decomposed plant material *Oe - 2 to 3 inches:* moderately decomposed plant material *A - 3 to 7 inches:* loamy coarse sand *E - 7 to 10 inches:* coarse sand *Bw1 - 10 to 15 inches:* coarse sand *Bw2 - 15 to 28 inches:* coarse sand *BC - 28 to 32 inches:* coarse sand *C - 32 to 67 inches:* coarse sand

Properties and qualities

Slope: 3 to 8 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Excessively drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very high (1.42 to 14.17 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water supply, 0 to 60 inches: Low (about 4.5 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3s Hydrologic Soil Group: A Ecological site: F149BY005MA - Dry Outwash Hydric soil rating: No

Minor Components

Deerfield

Percent of map unit: 10 percent Landform: Outwash terraces, outwash plains, kame terraces, outwash deltas Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Concave Hydric soil rating: No

Hinckley

Percent of map unit: 5 percent

- *Landform:* Moraines, eskers, kames, outwash deltas, outwash terraces, outwash plains, kame terraces
- *Landform position (two-dimensional):* Summit, shoulder, backslope, footslope, toeslope
- Landform position (three-dimensional): Head slope, nose slope, side slope, crest, riser, tread

Down-slope shape: Convex

Across-slope shape: Convex

Hydric soil rating: No

Merrimac

Percent of map unit: 3 percent Landform: Kame terraces, outwash deltas, outwash terraces Landform position (three-dimensional): Riser, tread Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

Mashpee

Percent of map unit: 2 percent Landform: Depressions, drainageways, terraces Landform position (three-dimensional): Tread Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

321A—Birchwood sand, 0 to 3 percent slopes, very stony

Map Unit Setting

National map unit symbol: 9y46 Elevation: 0 to 400 feet Mean annual precipitation: 41 to 54 inches Mean annual air temperature: 43 to 54 degrees F Frost-free period: 145 to 240 days Farmland classification: Farmland of statewide importance

Map Unit Composition

Birchwood, very stony, and similar soils: 80 percent *Minor components:* 20 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Birchwood, Very Stony

Setting

Landform: Till plains, ground moraines, drumlins Landform position (two-dimensional): Summit, footslope Landform position (three-dimensional): Interfluve Down-slope shape: Concave Across-slope shape: Concave Parent material: Sandy eolian deposits and/or sandy glaciofluvial deposits over coarse-loamy lodgment till

Typical profile

Oi - 0 to 1 inches: slightly decomposed plant material Oe - 1 to 3 inches: moderately decomposed plant material Oa - 3 to 4 inches: highly decomposed plant material E - 4 to 5 inches: sand Ap - 5 to 8 inches: loamy sand Bs - 8 to 13 inches: loamy sand Bw1 - 13 to 19 inches: loamy sand *Bw2 - 19 to 29 inches:* loamy sand *BC - 29 to 40 inches:* sand *Cd1 - 40 to 55 inches:* gravelly sandy loam *Cd2 - 55 to 75 inches:* gravelly sandy loam

Properties and qualities

Slope: 0 to 3 percent
Surface area covered with cobbles, stones or boulders: 1.0 percent
Depth to restrictive feature: 35 to 59 inches to densic material
Drainage class: Moderately well drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately high (0.00 to 0.20 in/hr)
Depth to water table: About 12 to 29 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Low (about 3.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 5s Hydrologic Soil Group: B/D Ecological site: F144AY037MA - Moist Dense Till Uplands Hydric soil rating: No

Minor Components

Poquonock, very stony

Percent of map unit: 6 percent Landform: Till plains, ground moraines, drumlins Landform position (two-dimensional): Summit, shoulder Landform position (three-dimensional): Interfluve Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

Mattapoisett, extremely stony

Percent of map unit: 6 percent Landform: Drainageways, depressions Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Base slope Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

Scituate, very stony

Percent of map unit: 5 percent Landform: Drumlins, ridges Landform position (two-dimensional): Summit, footslope Landform position (three-dimensional): Interfluve Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: No

Newfields, extremely stony

Percent of map unit: 3 percent *Landform:* Till plains, hills, moraines

Custom Soil Resource Report

Landform position (two-dimensional): Summit, footslope Landform position (three-dimensional): Interfluve Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: No

430C—Barnstable loamy sand, 8 to 15 percent slopes

Map Unit Setting

National map unit symbol: 9y3r Elevation: 10 to 400 feet Mean annual precipitation: 41 to 54 inches Mean annual air temperature: 43 to 54 degrees F Frost-free period: 145 to 240 days Farmland classification: Farmland of statewide importance

Map Unit Composition

Barnstable and similar soils: 80 percent *Minor components:* 20 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Barnstable

Setting

Landform: Moraines Landform position (two-dimensional): Shoulder, backslope Landform position (three-dimensional): Side slope Down-slope shape: Linear Across-slope shape: Convex Parent material: Coarse-loamy supraglacial meltout till over sandy and gravelly glaciofluvial deposits

Typical profile

Oi - 0 to 2 inches: slightly decomposed plant material *Oe - 2 to 3 inches:* moderately decomposed plant material *Oa - 3 to 4 inches:* highly decomposed plant material *E - 4 to 6 inches:* loamy sand *Bs - 6 to 7 inches:* gravelly sandy loam *Bw1 - 7 to 13 inches:* stony sandy loam *Bw2 - 13 to 27 inches:* very stony coarse sandy loam *2C1 - 27 to 40 inches:* very gravelly coarse sand *2C2 - 40 to 64 inches:* very gravelly coarse sand

Properties and qualities

Slope: 8 to 15 percent
 Depth to restrictive feature: 23 to 27 inches to strongly contrasting textural stratification
 Drainage class: Well drained
 Runoff class: Low

Custom Soil Resource Report

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (0.57 to 1.98 in/hr) Depth to water table: More than 80 inches Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Very low (about 2.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3e Hydrologic Soil Group: B Ecological site: F149BY011MA - Well Drained Till Uplands Hydric soil rating: No

Minor Components

Plymouth

Percent of map unit: 7 percent Landform: Outwash plains, moraines Landform position (two-dimensional): Shoulder, backslope Landform position (three-dimensional): Side slope, riser Down-slope shape: Linear Across-slope shape: Convex Hydric soil rating: No

Merrimac

Percent of map unit: 5 percent Landform: Kames, terraces, outwash plains Landform position (two-dimensional): Shoulder, backslope Landform position (three-dimensional): Riser Down-slope shape: Linear Across-slope shape: Convex Hydric soil rating: No

Canton

Percent of map unit: 5 percent Landform: Till plains, ridges, hills Landform position (two-dimensional): Shoulder, backslope Landform position (three-dimensional): Side slope Down-slope shape: Linear Across-slope shape: Convex Hydric soil rating: No

Newfields

Percent of map unit: 3 percent Landform: Moraines, hills, till plains Landform position (two-dimensional): Shoulder, footslope Landform position (three-dimensional): Interfluve Down-slope shape: Linear Across-slope shape: Concave Hydric soil rating: No

656B—Udorthents - Urban land complex, 0 to 8 percent slopes

Map Unit Setting

National map unit symbol: bd08 Elevation: 0 to 390 feet Mean annual precipitation: 41 to 54 inches Mean annual air temperature: 43 to 54 degrees F Frost-free period: 145 to 240 days Farmland classification: Not prime farmland

Map Unit Composition

Udorthents, loamy, and similar soils: 45 percent Urban land: 40 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Udorthents, Loamy

Setting

Landform position (two-dimensional): Summit, shoulder Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Linear Parent material: Coarse-loamy human transported material

Typical profile

^A - 0 to 5 inches: loam
^C1 - 5 to 21 inches: gravelly loam
^C2 - 21 to 80 inches: gravelly sandy loam

Properties and qualities

Slope: 0 to 8 percent
Depth to restrictive feature: More than 80 inches
Drainage class: Well drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to very high (0.01 to 14.17 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water supply, 0 to 60 inches: Moderate (about 7.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2s Hydrologic Soil Group: B Ecological site: F149BY100NY - Urban Site Complex Hydric soil rating: No

Minor Components

Udipsamments, wet substratum

Percent of map unit: 5 percent Landform: Dikes Landform position (two-dimensional): Footslope Landform position (three-dimensional): Tread Down-slope shape: Linear, convex Across-slope shape: Linear Hydric soil rating: No

Udipsamments

Percent of map unit: 5 percent Landform: Dikes Landform position (two-dimensional): Summit Landform position (three-dimensional): Tread Down-slope shape: Linear, convex Across-slope shape: Linear Hydric soil rating: No

Udorthents, wet substratum

Percent of map unit: 5 percent Landform position (two-dimensional): Footslope Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

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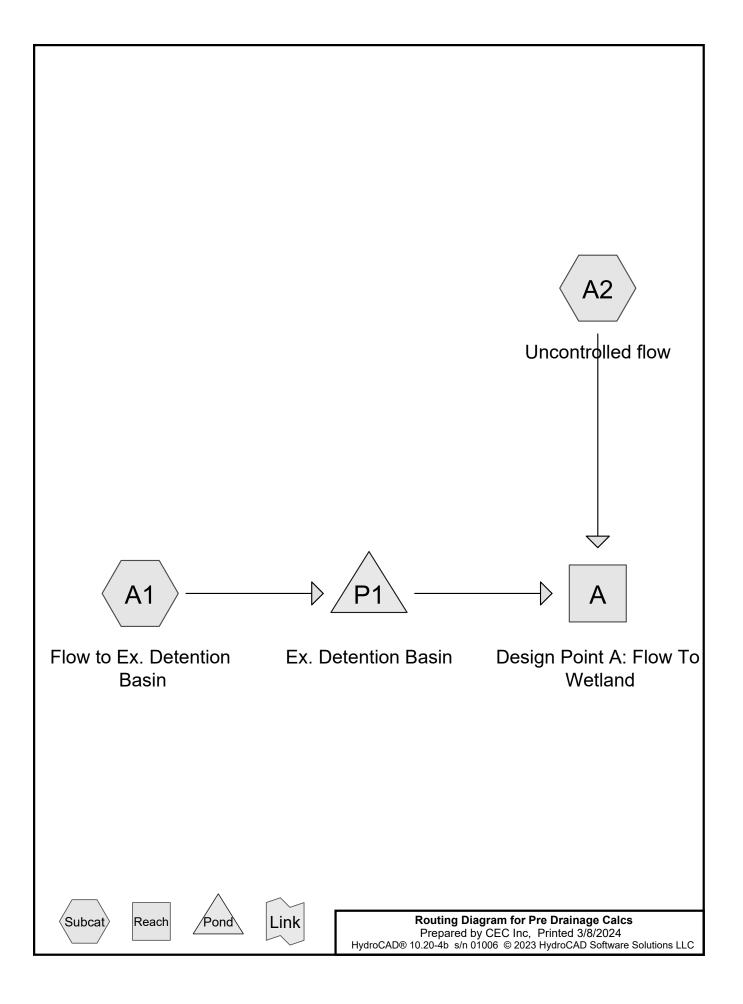
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APPENDIX C

SUPPORTING CALCULATIONS

HydroCAD Drainage Analysis TSS Calculations Phosphorus Removal Calculations Water Quality Volume Calculations Sediment Forebay Sizing Calculations HydroCAD Drainage Analysis



Project Notes

Rainfall events imported from "Atlas-14-Rain.txt" for 447 MA Plymouth

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	2-Year	Type III 24-hr		Default	24.00	1	3.35	2
2	10-Year	Type III 24-hr		Default	24.00	1	4.95	2
3	25-Year	Type III 24-hr		Default	24.00	1	6.19	2
4	100-Year	Type III 24-hr		Default	24.00	1	8.68	2

Rainfall Events Listing

Area Listing (all nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
3.9	39	>75% Grass cover, Good, HSG A (A1)
0.4	39	Landscaped islands, Good, HSG A (A1)
3.4	98	Paved parking, HSG A (A1)
0.5	98	Water Surface, HSG A (A1)
2.8	45	Woods, Poor, HSG A (A1, A2)
0.2	98	paved sidewalks, HSG A (A1)
11.2	62	TOTAL AREA

Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
11.2	HSG A	A1, A2
0.0	HSG B	
0.0	HSG C	
0.0	HSG D	
0.0	Other	
11.2		TOTAL AREA

Pre Drainage Calcs

Prepared by CEC Inc	
HydroCAD® 10.20-4b s/n 01006	© 2023 HydroCAD Software Solutions LLC

Ground Covers (all nodes)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
3.9	0.0	0.0	0.0	0.0	3.9	>75% Grass cover, Good	A1
0.4	0.0	0.0	0.0	0.0	0.4	Landscaped islands, Good	A1
3.4	0.0	0.0	0.0	0.0	3.4	Paved parking	A1
0.5	0.0	0.0	0.0	0.0	0.5	Water Surface	A1
2.8	0.0	0.0	0.0	0.0	2.8	Woods, Poor	A1, A2
0.2	0.0	0.0	0.0	0.0	0.2	paved sidewalks	A1
11.2	0.0	0.0	0.0	0.0	11.2	TOTAL AREA	

Pre Drainage Calcs Prepared by CEC Inc HydroCAD® 10.20-4b s/n 01006 © 2023 HydroCAD Software Sol	Type III 24-hr 2-Year Rainfall=3.35" Printed 3/8/2024 utions LLC Page 7		
Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method			
	10 sf 39.85% Impervious Runoff Depth>0.56" Tc=9.6 min CN=64 Runoff=5.2 cfs 0.482 af		
	860 sf 0.00% Impervious Runoff Depth>0.04" Tc=8.7 min CN=45 Runoff=0.0 cfs 0.003 af		
Reach A: Design Point A: Flow To Wetland	Inflow=0.7 cfs 0.367 af Outflow=0.7 cfs 0.367 af		
Pond P1: Ex. Detention BasinPeak Elev=30	.74' Storage=13,300 cf Inflow=5.2 cfs 0.482 af Outflow=0.7 cfs 0.364 af		
	me = 0.485 af Average Runoff Depth = 0.52" vious = 7.1 ac 36.68% Impervious = 4.1 ac		

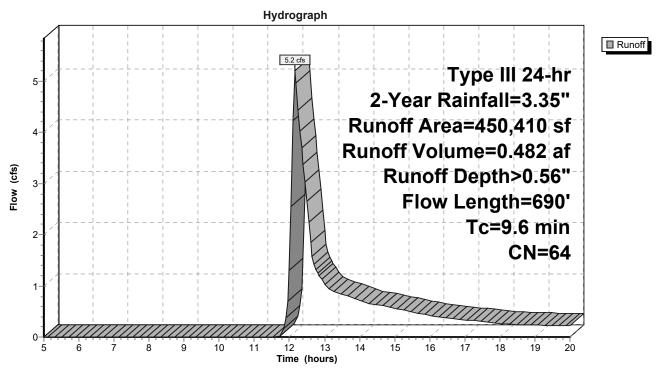
Summary for Subcatchment A1: Flow to Ex. Detention Basin

Runoff	=	5.2 cfs @	12.17 hrs, Volu	ume=	0.482 af,	Depth>	0.56"
Routed	to Pond I	P1 : Ex. Dete	ention Basin				

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.35"

_	A	rea (sf)	CN E	Description					
*		18,731	39 L	Landscaped islands, Good, HSG A					
*		7,841	98 p	aved side	walks, HSG	3 A			
		82,000	45 V	Voods, Poo	or, HSG A				
	1	49,846	98 F	aved park	ing, HSG A	N Contraction of the second seco			
	1	70,212	39 >	•75% Gras	s cover, Go	bod, HSG A			
_		21,780	98 V	Vater Surfa	ace, HSG A	۱			
	4	50,410	64 V	Veighted A	verage				
	2	70,943	6	0.15% Per	rvious Area				
	1	79,467	3	9.85% Imp	pervious Ar	ea			
	Тс	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	4.3	50	0.0400	0.20		Sheet Flow, A-B			
						Grass: Short n= 0.150 P2= 3.20"			
	5.3	640	0.0100	2.03		Shallow Concentrated Flow, B-C			
_						Paved Kv= 20.3 fps			
	9.6	690	Total						

Subcatchment A1: Flow to Ex. Detention Basin



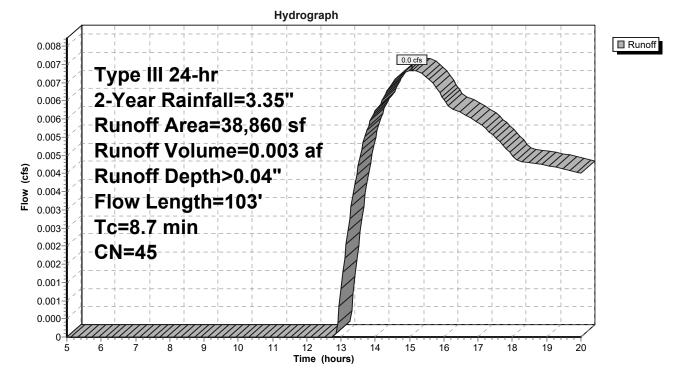
Summary for Subcatchment A2: Uncontrolled flow

Runoff = 0.0 cfs @ 15.06 hrs, Volume= 0.003 af, Depth> 0.04" Routed to Reach A : Design Point A: Flow To Wetland

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.35"

_	A	rea (sf)	CN E	Description		
		38,860	45 V	Voods, Poo	or, HSG A	
		38,860	1	00.00% P	ervious Are	а
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	8.5	50	0.0500	0.10		Sheet Flow, A-B
	0.2	53	0.0900	4.83		Woods: Light underbrush n= 0.400 P2= 3.20" Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps
	8.7	103	Total			

Subcatchment A2: Uncontrolled flow

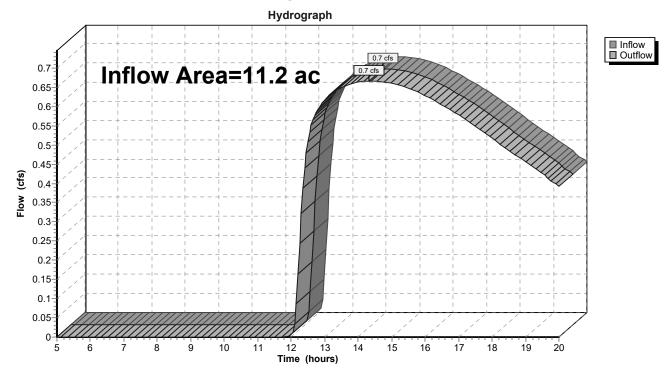


Summary for Reach A: Design Point A: Flow To Wetland

[40] Hint: Not Described (Outflow=Inflow)

Inflow Are	ea =	11.2 ac, 36.68% Impervious, Inflow Depth > 0.39" for 2-Year event	
Inflow	=	0.7 cfs @ 14.34 hrs, Volume= 0.367 af	
Outflow	=	0.7 cfs @ 14.34 hrs, Volume= 0.367 af, Atten= 0%, Lag= 0.0 mi	n

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Reach A: Design Point A: Flow To Wetland

Summary for Pond P1: Ex. Detention Basin

Outflow = Primary =	5.2 0.7 0.7	2 cfs @ 7 cfs @ 7 cfs @	12.17 hrs, 14.27 hrs, 14.27 hrs, 14.27 hrs,	√olume= √olume=	0.482 af	or 2-Year event en= 87%, Lag= 126.2 min
Starting Elev	Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Starting Elev= 30.00' Surf.Area= 10,000 sf Storage= 4,261 cf Peak Elev= 30.74'@ 14.27 hrs Surf.Area= 13,476 sf Storage= 13,300 cf (9,039 cf above start)					
Plug-Flow detention time=261.1 min calculated for 0.265 af (55% of inflow) Center-of-Mass det. time= 108.3 min(953.4 - 845.2)						
Volume	Invert	Avail.Sto	orage Stor	age Descriptio	n	
#1	29.00'	101,1	65 cf Cus	tom Stage Da	i ta (Irregular) Lis	sted below
Elevation (feet)	Surf.A (se	Area F q-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	

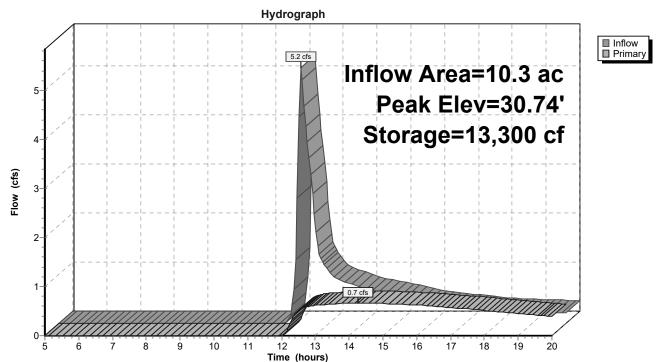
<i>-</i> a	VVCLAN	Oun.otore	110.0000		Ouri.Aica	
ft)	(sq-	(cubic-feet)	(cubic-feet)	(feet)	(sq-ft)	(feet)
15	5	0	0	100.0	515	29.00
42	56,54	4,261	4,261	845.0	10,000	30.00
39	116,23	16,548	12,287	1,210.0	14,725	31.00
36	123,1	33,305	16,757	1,245.0	18,875	32.00
36	125,5	54,121	20,816	1,255.0	22,820	33.00
57	129,7	78,783	24,661	1,275.0	26,550	34.00
32	134,98	101,165	22,382	1,300.0	29,430	34.80

Device	Routing	Invert	Outlet Devices
#1	Device 3	32.00'	2.5' long x 2.80' rise Sharp-Crested Rectangular Weir
			2 End Contraction(s) 3.0' Crest Height
#2	Device 3	30.00'	6.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#3	Primary	28.91'	24.0" Round Culvert
	•		L= 40.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 28.91' / 28.51' S= 0.0100 '/' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 3.14 sf

Primary OutFlow Max=0.7 cfs @ 14.27 hrs HW=30.74' (Free Discharge) **3=Culvert** (Passes 0.7 cfs of 10.9 cfs potential flow)

-1=Sharp-Crested Rectangular Weir (Controls 0.0 cfs)

-2=Orifice/Grate (Orifice Controls 0.7 cfs @ 3.36 fps)



Pond P1: Ex. Detention Basin

Pre Drainage Calcs Prepared by CEC Inc HydroCAD® 10.20-4b s/n 01006 © 2023 HydroCAD Soft	Type III 24-hr 10-Year Rainfall=4.95" Printed 3/8/2024 ware Solutions LLC Page 13			
Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method				
	ea=450,410 sf 39.85% Impervious Runoff Depth>1.41" th=690' Tc=9.6 min CN=64 Runoff=15.4 cfs 1.213 af			
	Area=38,860 sf 0.00% Impervious Runoff Depth>0.36" gth=103' Tc=8.7 min CN=45 Runoff=0.2 cfs 0.027 af			
Reach A: Design Point A: Flow To Wetland	Inflow=1.3 cfs 0.791 af Outflow=1.3 cfs 0.791 af			
Pond P1: Ex. Detention Basin Peak E	lev=31.96' Storage=32,644 cf Inflow=15.4 cfs 1.213 af Outflow=1.2 cfs 0.764 af			
	off Volume = 1.240 af Average Runoff Depth = 1.32" 2% Pervious = 7.1 ac 36.68% Impervious = 4.1 ac			

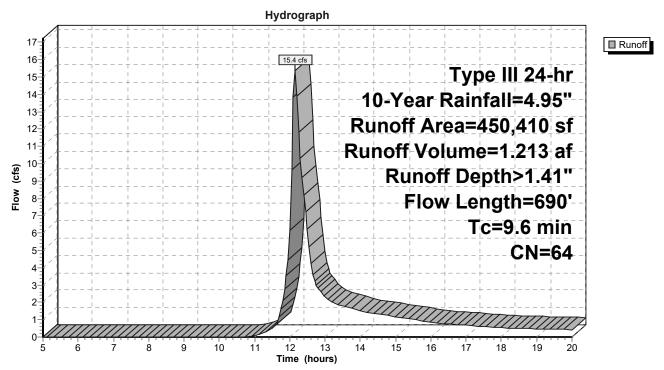
Summary for Subcatchment A1: Flow to Ex. Detention Basin

Runoff = 15.4 cfs @ 12.15 hrs, Volume= 1.213 af, Depth> 1.41" Routed to Pond P1 : Ex. Detention Basin

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.95"

_	A	rea (sf)	CN E	Description					
*		18,731	39 L	Landscaped islands, Good, HSG A					
*		7,841	98 p	aved side	walks, HSG	6 A			
		82,000	45 V	Voods, Poo	or, HSG A				
	1	49,846	98 F	aved park	ing, HSG A	N Contraction of the second			
	1	70,212	39 >	75% Gras	s cover, Go	bod, HSG A			
_		21,780	98 V	Vater Surfa	ace, HSG A	ι			
450,410 64 Weighted Average					verage				
	2	70,943	6	60.15% Pervious Area					
	1	79,467	3	39.85% Impervious Area					
	Тс	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	4.3	50	0.0400	0.20		Sheet Flow, A-B			
						Grass: Short n= 0.150 P2= 3.20"			
	5.3	640	0.0100	2.03		Shallow Concentrated Flow, B-C			
_						Paved Kv= 20.3 fps			
	9.6	690	Total						

Subcatchment A1: Flow to Ex. Detention Basin



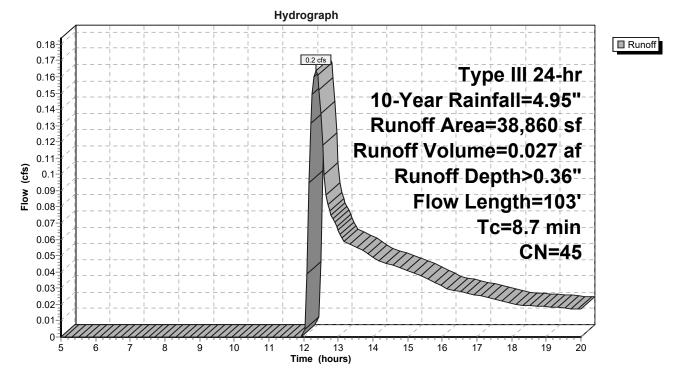
Summary for Subcatchment A2: Uncontrolled flow

Runoff = 0.2 cfs @ 12.35 hrs, Volume= 0.027 af, Depth> 0.36" Routed to Reach A : Design Point A: Flow To Wetland

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.95"

_	A	rea (sf)	CN E	Description				
	38,860 45 Woods, Poor, HSG A							
38,860 100.00% Pervious Area						a		
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
-	8.5	50	0.0500	0.10		Sheet Flow, A-B		
_	0.2	53	0.0900	4.83		Woods: Light underbrush n= 0.400 P2= 3.20" Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps		
_	8.7	103	Total					

Subcatchment A2: Uncontrolled flow

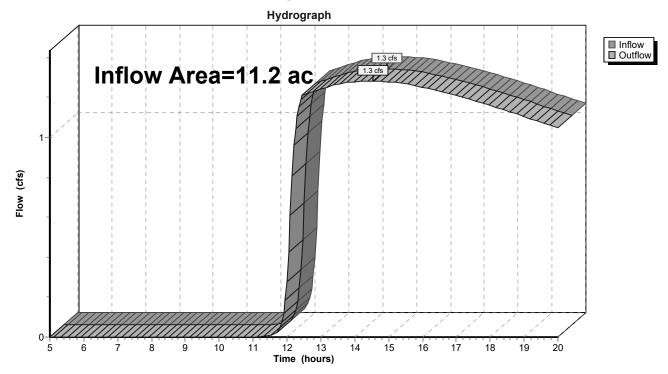


Summary for Reach A: Design Point A: Flow To Wetland

[40] Hint: Not Described (Outflow=Inflow)

Inflow Are	a =	11.2 ac, 36.6	8% Impervious	, Inflow Depth >	0.84"	for 10-Year	event
Inflow	=	1.3 cfs @	14.53 hrs, Vol	ume= 0.	791 af		
Outflow	=	1.3 cfs @	14.53 hrs, Vol	ume= 0.	791 af,	Atten= 0%, L	ag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Reach A: Design Point A: Flow To Wetland

Summary for Pond P1: Ex. Detention Basin

Inflow Area =	10.3 ac, 39.8	35% Imperviou	is, Inflow Dept	h > 1.41"	for 10-Yea	r event	
Inflow =	15.4 cfs @	12.15 hrs, V	olume=	1.213 af			
Outflow =	1.2 cfs @	14.81 hrs, Vo	olume=	0.764 af,	Atten= 92%,	Lag= 159.3 min	
Primary =	1.2 cfs @	14.81 hrs, Vo	olume=	0.764 af			
Routed to Rea	ch A : Design	Point A: Flow	To Wetland				
Routing by Stor-Ir							
Starting Elev= 30.00' Surf.Area= 10,000 sf Storage= 4,261 cf							
Peak Elev= 31.96	'@ 14.81 hrs	Surf.Area= 1	8,711 sf Stora	age= 32,644	1 cf (28,383	cf above start)	

Plug-Flow detention time= 253.9 min calculated for 0.664 af (55% of inflow) Center-of-Mass det. time= 136.8 min (959.5 - 822.7)

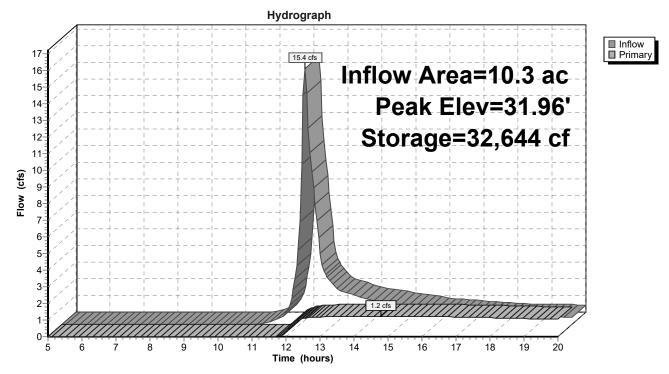
Volume	Inve	rt Avail	.Storage	Storage Descriptio	n		
#1	29.00	D' 10)1,165 cf	Custom Stage Da	i ta (Irregular) Liste	d below	
Elevatio (fee 30.0 31.0 32.0 33.0 34.0 34.0 34.0	et) 00 00 00 00 00 00 00	Surf.Area (sq-ft) 515 10,000 14,725 18,875 22,820 26,550 20,420	Perim. (feet) 100.0 845.0 1,210.0 1,245.0 1,255.0 1,275.0 1,200.0	Inc.Store (cubic-feet) 0 4,261 12,287 16,757 20,816 24,661 22,282	Cum.Store (cubic-feet) 0 4,261 16,548 33,305 54,121 78,783 101 165	Wet.Area (sq-ft) 515 56,542 116,239 123,186 125,536 129,757 134,082	
Jevice	Routing	29,430 Inv	1,300.0 /ert Outl	22,382 et Devices	101,165	134,982	
#1	Device 3		.00' 2.5'	long x 2.80' rise Sharp-Crested Rectangular Weir			
2 End Contraction(s) 3.0'		C= 0.600 Limitong, no headwall, K 91' / 28.51' S= 0.0	0100 '/' Cc= 0.900				

Primary OutFlow Max=1.2 cfs @ 14.81 hrs HW=31.96' (Free Discharge)

-3=Culvert (Passes 1.2 cfs of 17.1 cfs potential flow)

1=Sharp-Crested Rectangular Weir(Controls 0.0 cfs)

-2=Orifice/Grate (Orifice Controls 1.2 cfs @ 6.30 fps)



Pond P1: Ex. Detention Basin

Pre Drainage Calcs Prepared by CEC Inc HydroCAD® 10.20-4b s/n 01006 © 2023 HydroCA	<i>Type III 24-hr 25-Year Rainfall=6.19"</i> Printed 3/8/2024 D Software Solutions LLC Page 19			
Time span=5.00-20 Runoff by SCS TR-20	00 hrs, dt=0.05 hrs, 301 points method, UH=SCS, Weighted-CN method - Pond routing by Stor-Ind method			
	off Area=450,410 sf 39.85% Impervious Runoff Depth>2.20" / Length=690' Tc=9.6 min CN=64 Runoff=24.8 cfs 1.898 af			
	unoff Area=38,860 sf 0.00% Impervious Runoff Depth>0.77" w Length=103' Tc=8.7 min CN=45 Runoff=0.5 cfs 0.057 af			
Reach A: Design Point A: Flow To WetlandInflow=4.2 cfs1.385 atOutflow=4.2 cfs1.385 atOutflow=4.2 cfs1.385 at				
Pond P1: Ex. Detention Basin	Peak Elev=32.48' Storage=43,211 cf Inflow=24.8 cfs 1.898 af Outflow=4.0 cfs 1.328 af			
Total Runoff Area = 11.2 ac	Runoff Volume = 1.955 af 63.32% Pervious = 7.1 acAverage Runoff Depth = 2.09" 36.68% Impervious = 4.1 ac			

Summary for Subcatchment A1: Flow to Ex. Detention Basin

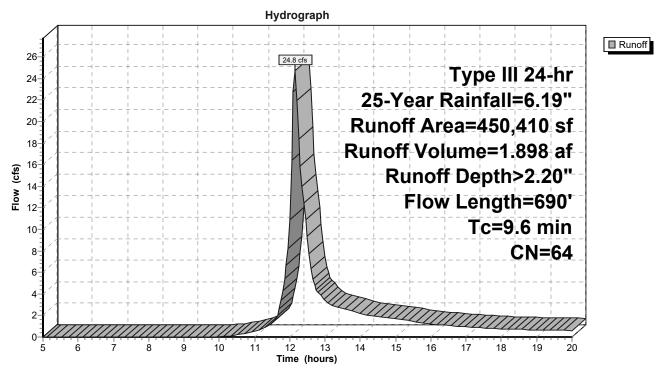
Runoff	=	24.8 cfs @	12.15 hrs,	Volume=	1.898	3 af,	Depth>	2.20"
Routed	d to Pond	d P1 : Ex. Dete	ention Basir	า				

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=6.19"

_	A	rea (sf)	CN E	Description					
*		18,731	39 L	Landscaped islands, Good, HSG A					
*		7,841	98 p	aved side	walks, HSG	3 A			
		82,000	45 V	Voods, Poo	or, HSG A				
	1	49,846	98 F	Paved park	ing, HSG A	N Contraction of the second			
	1	70,212			,	bod, HSG A			
_		21,780	98 V	Vater Surfa	ace, HSG A	N			
450,410 64			64 V	Weighted Average					
	270,943		-	60.15% Pervious Area					
	1	79,467	3	9.85% Imp	pervious Ar	ea			
	_				-				
	Tc	Length	Slope		Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	4.3	50	0.0400	0.20		Sheet Flow, A-B			
						Grass: Short n= 0.150 P2= 3.20"			
	5.3	640	0.0100	2.03		Shallow Concentrated Flow, B-C			
_						Paved Kv= 20.3 fps			
	0.6	600	Total						

9.6 690 Total

Subcatchment A1: Flow to Ex. Detention Basin



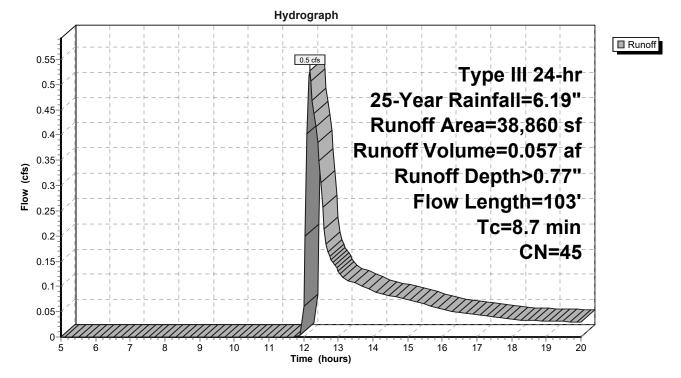
Summary for Subcatchment A2: Uncontrolled flow

Runoff = 0.5 cfs @ 12.17 hrs, Volume= 0.057 af, Depth> 0.77" Routed to Reach A : Design Point A: Flow To Wetland

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=6.19"

_	A	rea (sf)	CN E	Description				
	38,860 45 Woods, Poor, HSG A							
		38,860	1	00.00% P	ervious Are	a		
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
_	8.5	50	0.0500	0.10		Sheet Flow, A-B		
_	0.2	53	0.0900	4.83		Woods: Light underbrush n= 0.400 P2= 3.20" Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps		
	8.7	103	Total					

Subcatchment A2: Uncontrolled flow

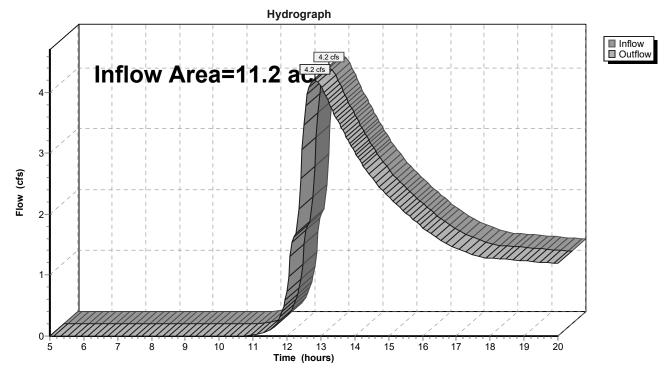


Summary for Reach A: Design Point A: Flow To Wetland

[40] Hint: Not Described (Outflow=Inflow)

Inflow Are	a =	11.2 ac, 36.6	8% Impervious,	Inflow Depth >	1.48"	for 25-Year	event
Inflow	=	4.2 cfs @	12.81 hrs, Volu	ume= 1.3	385 af		
Outflow	=	4.2 cfs @	12.81 hrs, Volu	ume= 1.3	385 af,	Atten= 0%, L	ag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Reach A: Design Point A: Flow To Wetland

Summary for Pond P1: Ex. Detention Basin

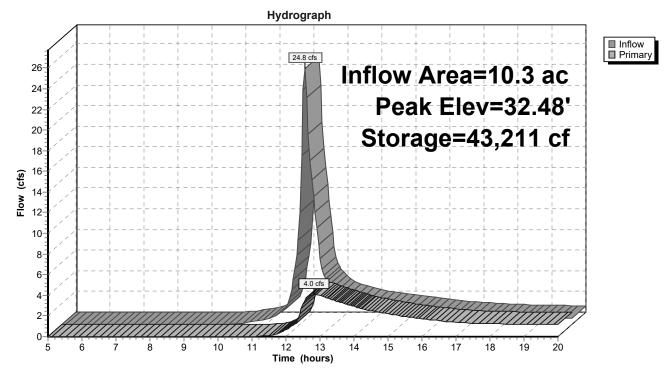
Inflow A Inflow Outflow Primary Rout	= = =	24.8 cfs (4.0 cfs (4.0 cfs (2) 12.15 2) 12.83 2) 12.83 2) 12.83	pervious, Inflow De hrs, Volume= hrs, Volume= hrs, Volume= Flow To Wetland	pth > 2.20" for 2 1.898 af 1.328 af, Atten= 1.328 af	5-Year event 84%, Lag= 41.2 min	
Starting	Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Starting Elev= 30.00' Surf.Area= 10,000 sf Storage= 4,261 cf Peak Elev= 32.48' @ 12.83 hrs Surf.Area= 20,752 sf Storage= 43,211 cf (38,950 cf above start)						
Center-	Plug-Flow detention time= 187.3 min calculated for 1.230 af (65% of inflow) Center-of-Mass det. time= 97.5 min(910.1 - 812.7)						
Volume	Inve	ert Avail	.Storage	Storage Description	on		
#1	29.0	0' 10)1,165 cf	Custom Stage Da	ata (Irregular)Listed	below	
				-			
Elevatio	on	Surf.Area	Perim.	Inc.Store	Cum.Store	Wet.Area	
(fee	et)	(sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	<u>(sq-ft)</u>	
29.0	00	515	100.0	0	0	515	
30.0	00	10,000	845.0	4,261	4,261	56,542	
31.0	00	14,725	1,210.0	12,287	16,548	116,239	
32.0	00	18,875	1,245.0	16,757	33,305	123,186	
33.0	00	22,820	1,255.0	20,816	54,121	125,536	
34.0	00	26,550	1,275.0	24,661	78,783	129,757	
34.8	80	29,430	1,300.0	22,382	101,165	134,982	
Device	Routing	١n	vert Outle	et Devices			
#1	Device 3	32.	00' 2.5'	long x 2.80' rise S	harp-Crested Recta	angular Weir	
				d Contraction(s) 3		-	
#2	Device 3	30.				d to weir flow at low hea	ds
#3	Primary	28.	91' 24.0	" Round Culvert			
	-		L= 4	0.0' CPP, projecti	ng, no headwall, Ke	= 0.900	
			Inlet	/ Outlet Invert= 28	91'/2851' S= 0.0'	100 '/' Cc= 0.900	

Inlet / Outlet Invert= 28.91' / 28.51' S= 0.0100 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 3.14 sf

Primary OutFlow Max=4.0 cfs @ 12.83 hrs HW=32.48' (Free Discharge)

-3=Culvert (Passes 4.0 cfs of 19.1 cfs potential flow)

-1=Sharp-Crested Rectangular Weir (Weir Controls 2.6 cfs @ 2.30 fps) -2=Orifice/Grate (Orifice Controls 1.4 cfs @ 7.18 fps)



Pond P1: Ex. Detention Basin

Pre Drainage Calcs Prepared by CEC Inc	Type III 24-hr 100-Year Rainfall=8.68" Printed 3/8/2024
HydroCAD® 10.20-4b s/n 01006 © 2023 Hyd	roCAD Software Solutions LLC Page 25
Runoff by SCS T	0-20.00 hrs, dt=0.05 hrs, 301 points R-20 method, UH=SCS, Weighted-CN Frans method - Pond routing by Stor-Ind method
SubcatchmentA1: Flow to Ex. Detention	Runoff Area=450,410 sf 39.85% Impervious Runoff Depth>4.02" Flow Length=690' Tc=9.6 min CN=64 Runoff=45.7 cfs 3.460 af
SubcatchmentA2: Uncontrolled flow	Runoff Area=38,860 sf 0.00% Impervious Runoff Depth>1.89" Flow Length=103' Tc=8.7 min CN=45 Runoff=1.7 cfs 0.141 af
Reach A: Design Point A: Flow To Wetlar	nd Inflow=16.0 cfs 2.933 af Outflow=16.0 cfs 2.933 af
Pond P1: Ex. Detention Basin	Peak Elev=33.46' Storage=65,578 cf Inflow=45.7 cfs 3.460 af Outflow=15.3 cfs 2.792 af
Total Runoff Area = 11.2	2 ac Runoff Volume = 3.601 af Average Runoff Depth = 3.85" 63.32% Pervious = 7.1 ac 36.68% Impervious = 4.1 ac

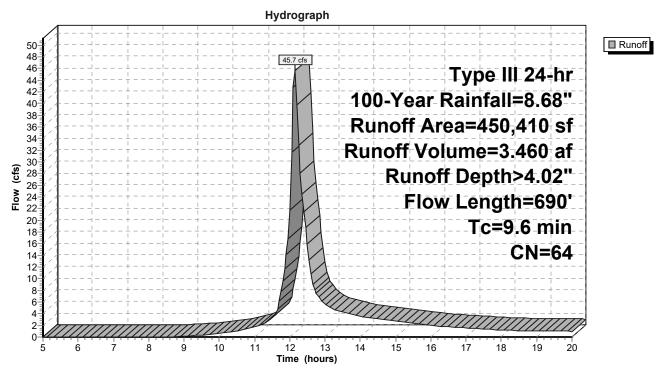
Summary for Subcatchment A1: Flow to Ex. Detention Basin

Runoff = 45.7 cfs @ 12.14 hrs, Volume= 3.460 af, Depth> 4.02" Routed to Pond P1 : Ex. Detention Basin

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=8.68"

	A	rea (sf)	CN E	Description						
*		18,731	39 L	Landscaped islands, Good, HSG A						
*		7,841	98 p	aved side	walks, HSG	6 A				
		82,000	45 V	Voods, Poo	or, HSG A					
	1	49,846	98 F	aved park	ing, HSG A	N Contraction of the second				
	1	70,212	39 >	75% Gras	s cover, Go	bod, HSG A				
_		21,780	98 V	Vater Surfa	ace, HSG A	ι				
	4	50,410	64 V	Veighted A	verage					
	2	70,943	6	0.15% Per	vious Area					
	1	79,467	3	9.85% Imp	pervious Ar	ea				
	Тс	Length	Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	4.3	50	0.0400	0.20		Sheet Flow, A-B				
						Grass: Short n= 0.150 P2= 3.20"				
	5.3	640	0.0100	2.03		Shallow Concentrated Flow, B-C				
_						Paved Kv= 20.3 fps				
	9.6	690	Total							

Subcatchment A1: Flow to Ex. Detention Basin



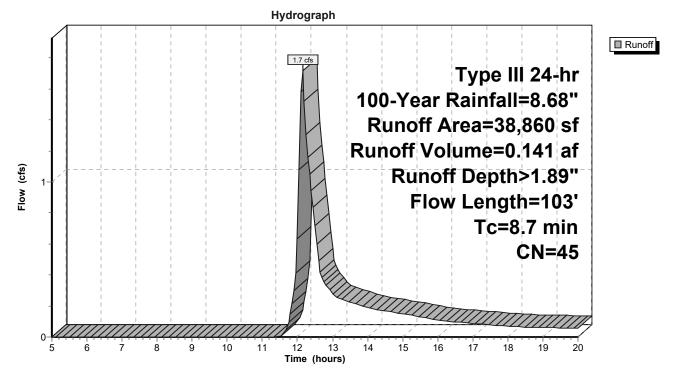
Summary for Subcatchment A2: Uncontrolled flow

Runoff = 1.7 cfs @ 12.15 hrs, Volume= 0.141 af, Depth> 1.89" Routed to Reach A : Design Point A: Flow To Wetland

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=8.68"

_	A	rea (sf)	CN E	Description		
		38,860	45 V	Voods, Po	or, HSG A	
_		38,860	1	00.00% P	ervious Are	a
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	8.5	50	0.0500	0.10		Sheet Flow, A-B
_	0.2	53	0.0900	4.83		Woods: Light underbrush n= 0.400 P2= 3.20" Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps
	8.7	103	Total			

Subcatchment A2: Uncontrolled flow

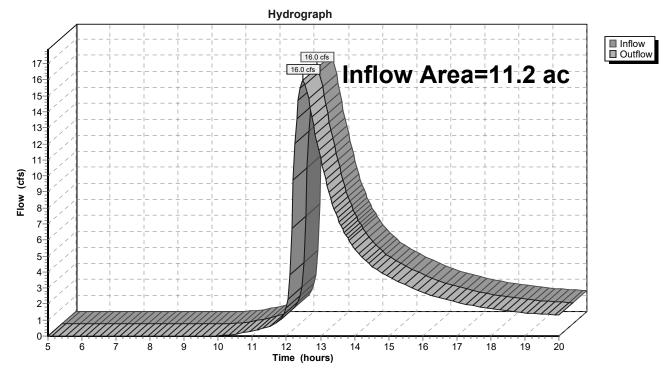


Summary for Reach A: Design Point A: Flow To Wetland

[40] Hint: Not Described (Outflow=Inflow)

Inflow Are	a =	11.2 ac, 36.68% Imperv	vious, Inflow Depth	n > 3.13"	for 100-Year event
Inflow	=	16.0 cfs @ 12.49 hrs	, Volume=	2.933 af	
Outflow	=	16.0 cfs @ 12.49 hrs	, Volume=	2.933 af,	Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Reach A: Design Point A: Flow To Wetland

Summary for Pond P1: Ex. Detention Basin

Inflow Are	a =	10.3 ac, 39.8	35% Impervious,	Inflow Depth >	4.02"	for 100-Yea	r event	
Inflow	=	45.7 cfs @	12.14 hrs, Volui	me= 3.4	l60 af			
Outflow	=	15.3 cfs @	12.51 hrs, Volui	me= 2.7	′92 af,	Atten= 67%,	Lag= 22.4 min	
Primary	=	15.3 cfs @	12.51 hrs, Volui	me= 2.7	′92 af			
Routed to Reach A : Design Point A: Flow To Wetland								

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Starting Elev= 30.00' Surf.Area= 10,000 sf Storage= 4,261 cf Peak Elev= 33.46' @ 12.51 hrs Surf.Area= 24,553 sf Storage= 65,578 cf (61,317 cf above start)

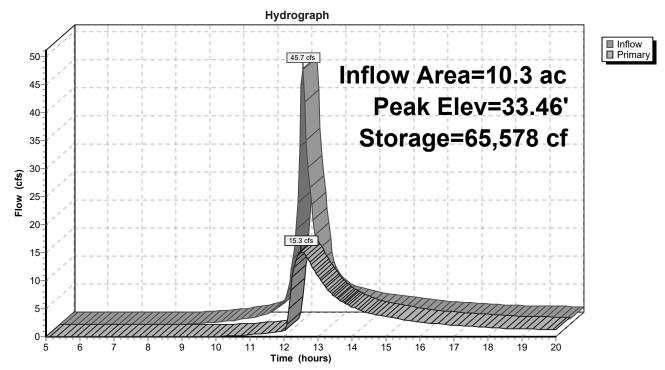
Plug-Flow detention time= 122.3 min calculated for 2.694 af (78% of inflow) Center-of-Mass det. time= 59.3 min (858.6 - 799.3)

Volume	Inve	vert Avail.Storage		Storage Description				
#1	29.00	0' 10	01,165 cf	Custom Stage Da	Custom Stage Data (Irregular)Listed below			
Elevatio (fee 29.0	et)	Surf.Area (sq-ft) 515	Perim. (feet) 100.0	Inc.Store (cubic-feet) 0	Cum.Store (cubic-feet) 0	Wet.Area (sq-ft) 515		
29.0 30.0 31.0	00	10,000 14,725	845.0 1,210.0	4,261 12,287	4,261 16,548	56,542 116,239		
32.0 33.0 34.0	00	18,875 22,820 26,550	1,245.0 1,255.0 1,275.0	16,757 20,816 24,661	33,305 54,121 78,783	123,186 125,536 129,757		
34.8		20,550 29,430	1,300.0	22,382	101,165	134,982		
Device	Routing	Invert Out		tlet Devices				
#1	Device 3			5' long x 2.80' rise Sharp-Crested Rectangular Weir End Contraction(s) 3.0' Crest Height				
#2 #3	Device 3 Primary		.00' 6.0'' .91' 24.0 L= 4 Inlet		e C= 0.600 Limite ng, no headwall, Ke 91' / 28.51' S= 0.0	100 '/' Cc= 0.900		

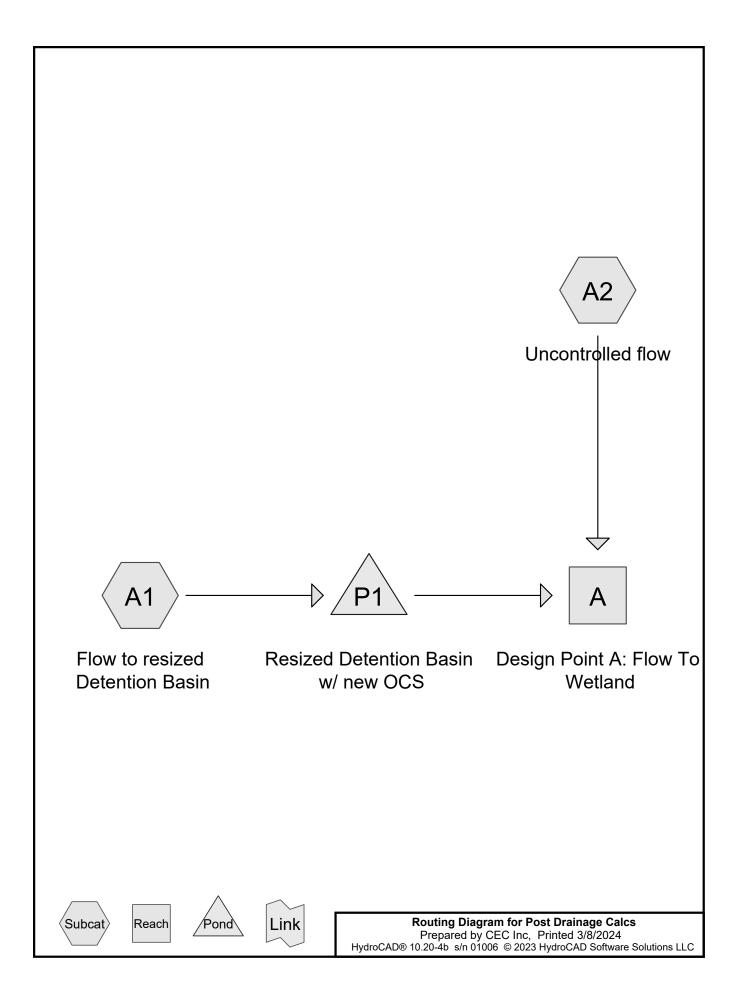
Primary OutFlow Max=15.2 cfs @ 12.51 hrs HW=33.46' (Free Discharge)

-3=Culvert (Passes 15.2 cfs of 22.5 cfs potential flow)

-1=Sharp-Crested Rectangular Weir (Weir Controls 13.5 cfs @ 4.19 fps) -2=Orifice/Grate (Orifice Controls 1.7 cfs @ 8.63 fps)



Pond P1: Ex. Detention Basin



Project Notes

Rainfall events imported from "Atlas-14-Rain.txt" for 447 MA Plymouth

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	2-Year	Type III 24-hr		Default	24.00	1	3.35	2
2	10-Year	Type III 24-hr		Default	24.00	1	4.95	2
3	25-Year	Type III 24-hr		Default	24.00	1	6.19	2
4	100-Year	Type III 24-hr		Default	24.00	1	8.68	2

Rainfall Events Listing

Area Listing (all nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
1.8	39	>75% Grass cover, Good, HSG A (A1)
0.1	98	Conc. slab areas/Shed roofs, HSG A (A1)
0.1	76	Field Transmission Material Storage area, HSG A (A1)
2.2	76	Gravel areas, HSG A (A1)
4.1	98	Paved parking, HSG A (A1)
0.8	98	Water Surface, HSG A (A1)
2.0	45	Woods, Poor, HSG A (A1, A2)
0.2	98	paved sidewalks, HSG A (A1)
11.2	75	TOTAL AREA

Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
11.2	HSG A	A1, A2
0.0	HSG B	
0.0	HSG C	
0.0	HSG D	
0.0	Other	
11.2		TOTAL AREA

Post Drainage Calcs

Prepared by CEC Inc	
HydroCAD® 10.20-4b s/n 01006	© 2023 HydroCAD Software Solutions LLC

Ground Covers (all nodes)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchmen Numbers
1.8	0.0	0.0	0.0	0.0	1.8	>75% Grass cover, Good	A1
0.1	0.0	0.0	0.0	0.0	0.1	Conc. slab areas/Shed roofs	A1
0.1	0.0	0.0	0.0	0.0	0.1	Field Transmission Material Storage area	A1
2.2	0.0	0.0	0.0	0.0	2.2	Gravel areas	A1
4.1	0.0	0.0	0.0	0.0	4.1	Paved parking	A1
0.8	0.0	0.0	0.0	0.0	0.8	Water Surface	A1
2.0	0.0	0.0	0.0	0.0	2.0	Woods, Poor	A1, A2
0.2	0.0	0.0	0.0	0.0	0.2	paved sidewalks	A1
11.2	0.0	0.0	0.0	0.0	11.2	TOTAL AREA	

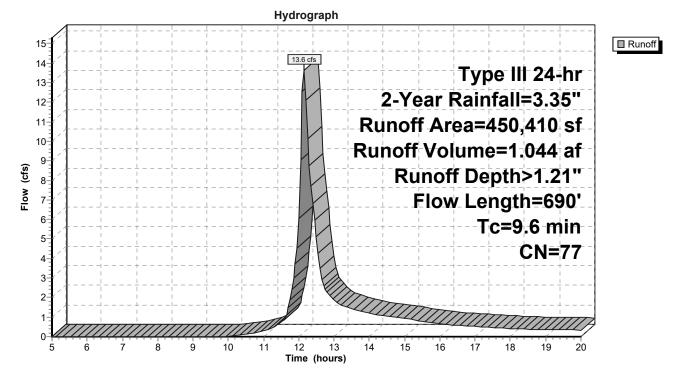
Post Drainage Calcs Prepared by CEC Inc <u>HydroCAD® 10.20-4b s/n 01006 © 2023 Hyd</u>	<i>Type III 24-hr 2-Year Rainfall=3.35"</i> Printed 3/8/2024 droCAD Software Solutions LLC Page 7					
Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method						
SubcatchmentA1: Flow to resized	Runoff Area=450,410 sf 49.60% Impervious Runoff Depth>1.21" Flow Length=690' Tc=9.6 min CN=77 Runoff=13.6 cfs 1.044 af					
SubcatchmentA2: Uncontrolled flow	Runoff Area=38,860 sf 0.00% Impervious Runoff Depth>0.04" Flow Length=103' Tc=8.7 min CN=45 Runoff=0.0 cfs 0.003 af					
Reach A: Design Point A: Flow To Wetla	nd Inflow=0.5 cfs 0.302 af Outflow=0.5 cfs 0.302 af					
Pond P1: Resized Detention Basin w/ ne	W Peak Elev=32.23' Storage=65,562 cf Inflow=13.6 cfs 1.044 af Outflow=0.5 cfs 0.298 af					
Total Runoff Area = 11.	2 ac Runoff Volume = 1.048 af Average Runoff Depth = 1.12" 54.34% Pervious = 6.1 ac 45.66% Impervious = 5.1 ac					

Summary for Subcatchment A1: Flow to resized Detention Basin

Runoff = 13.6 cfs @ 12.15 hrs, Volume= 1.044 af, Depth> 1.21" Routed to Pond P1 : Resized Detention Basin w/ new OCS

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.35"

	A	rea (sf)	CN [Description							
*		7,841	98 p	paved sidewalks, HSG A							
		47,778	45 \	Voods, Poor, HSG A							
	1	77,900	98 F	Paved park	ing, HSG A	N Contraction of the second seco					
		79,926	39 >	•75% Gras	s cover, Go	bod, HSG A					
		32,875	98 \	Vater Surfa	ace, HSG A	N Contraction of the second seco					
*		94,298	76 (Gravel area	as, HSG A						
*		4,792				l roofs, HSG A					
*		5,000	76 F	Field Trans	mission Ma	aterial Storage area, HSG A					
	4	50,410	77 \	Veighted A	verage						
	2	27,002	Ę	50.40% Pe	rvious Area	l					
	2	23,408	2	l9.60% Imp	pervious Ar	ea					
	Тс	Length	Slope	Velocity	Capacity	Description					
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
	4.3	50	0.0400	0.20		Sheet Flow, A-B					
						Grass: Short n= 0.150 P2= 3.20"					
	5.3	640	0.0100	2.03		Shallow Concentrated Flow, B-C					
_						Paved Kv= 20.3 fps					
	9.6	690	Total								



Subcatchment A1: Flow to resized Detention Basin

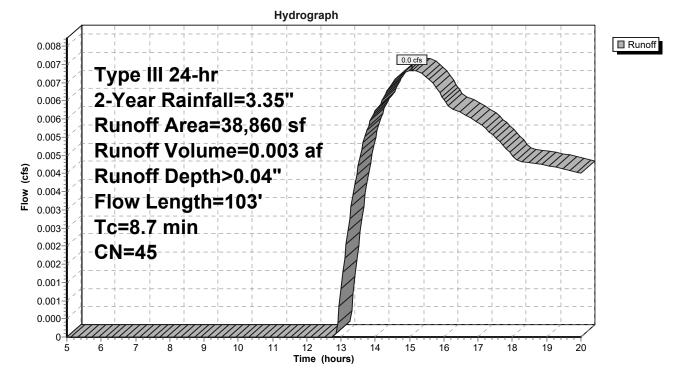
Summary for Subcatchment A2: Uncontrolled flow

Runoff = 0.0 cfs @ 15.06 hrs, Volume= 0.003 af, Depth> 0.04" Routed to Reach A : Design Point A: Flow To Wetland

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.35"

_	A	rea (sf)	CN E	Description		
		38,860	45 V	Voods, Poo	or, HSG A	
	38,860		100.00% Pervious Are			а
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	8.5	50	0.0500	0.10		Sheet Flow, A-B
	0.2	53	0.0900	4.83		Woods: Light underbrush n= 0.400 P2= 3.20" Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps
	8.7	103	Total			

Subcatchment A2: Uncontrolled flow

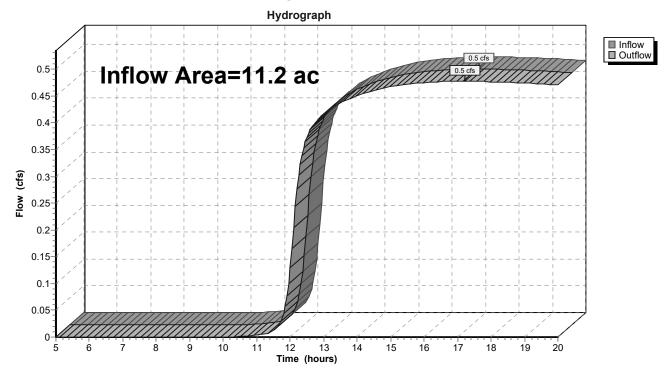


Summary for Reach A: Design Point A: Flow To Wetland

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =	11.2 ac, 4	5.66% Impervious, Inflow	Depth > 0.32" fo	or 2-Year event
Inflow =	0.5 cfs (② 17.22 hrs, Volume=	0.302 af	
Outflow =	0.5 cfs (0 17.22 hrs, Volume=	0.302 af, Att	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Reach A: Design Point A: Flow To Wetland

Summary for Pond P1: Resized Detention Basin w/ new OCS

Inflow Area = 10.3 ac, 49.60% Impervious, Inflow Depth > 1.21" for 2-Year event Inflow = 13.6 cfs @ 12.15 hrs, Volume= 1.044 af Outflow = 0.5 cfs @ 17.49 hrs, Volume= 0.298 af, Atten= 97%, Lag= 320.7 min Primary = 0.5 cfs @ 17.49 hrs, Volume= 0.298 af Routed to Reach A : Design Point A: Flow To Wetland 0.298 af										
Starting	Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Starting Elev= 30.80' Surf.Area= 20,690 sf Storage= 32,247 cf Peak Elev= 32.23' @ 17.49 hrs Surf.Area= 25,985 sf Storage= 65,562 cf (33,315 cf above start)									
Center-o	Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= 156.9 min (968.8 - 811.9)									
Volume				Storage Descriptio		h a lavo				
#1	29.00	J [*] 143, [*]	189 cf	Custom Stage Da	ata (Irregular) Listed	below				
Elevatio	on S	Surf.Area	Perim.	Inc.Store	Cum.Store	Wet.Area				
(fee	et)	(sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	<u>(sq-ft)</u>				
29.0		14,700	950.0		0	14,700				
30.0			,005.0	16,443	16,443	23,312				
31.0		,	,220.0	19,755	36,198	61,396				
32.0			,250.0	23,198	59,397	67,421				
33.0			,260.0		86,351	69,780				
34.0			,285.0		117,007	75,000				
34.8	50	32,905 1	,295.0	26,182	143,189	77,298				
Device	Routing	Invert	Outl	et Devices						
#1	Primary	29.18		" Round Culvert						
	,				ng, no headwall, Ke	= 0.900				
					18' / 29.00' S= 0.00					
			n= 0	0.012 Corrugated P	P, smooth interior, I	Flow Area= 3.14 sf				
#2	Device 1	30.80				d to weir flow at low heads				
#3	Device 1	32.50		Vert. Orifice/Grate						
ща	Davias 1	22.02		ted to weir flow at lo						
#4	Device 1	33.83		d (feet) 0.20 0.40	h Broad-Crested R	ectangular weir				
					.92 3.08 3.30 3.32					
#5	Device 1	34.50			ce/Grate X 8.00 col					
	2011001	000			4.0" x 24.0" Grate (4					
				ted to weir flow at lo		· /				

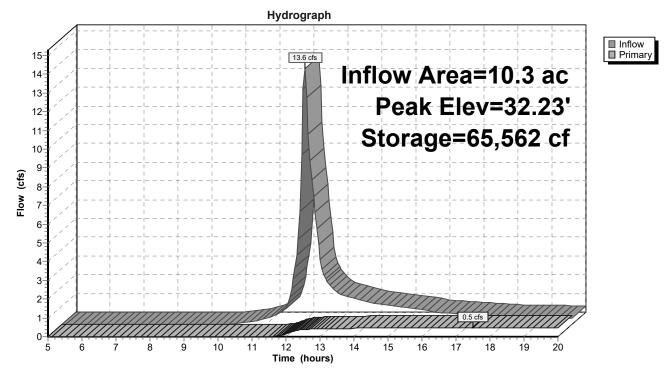
Primary OutFlow Max=0.5 cfs @ 17.49 hrs HW=32.23' (Free Discharge)

-1=Culvert (Passes 0.5 cfs of 17.1 cfs potential flow) -2=Orifice/Grate (Orifice Controls 0.5 cfs @ 5.41 fps)

-3=Orifice/Grate (Controls 0.0 cfs)

-4=Broad-Crested Rectangular Weir (Controls 0.0 cfs)

-5=Orifice/Grate (Controls 0.0 cfs)



Pond P1: Resized Detention Basin w/ new OCS

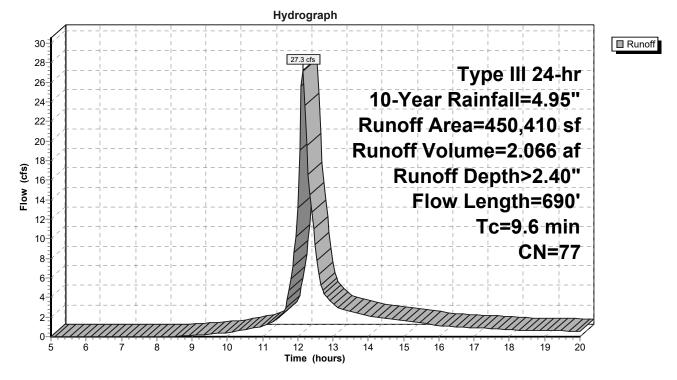
Post Drainage Calcs Prepared by CEC Inc HydroCAD® 10.20-4b s/n 01006 © 2023 Hyd	IroCAD Software Solutions L	LC	<i>10-Year Rainfall=4.95"</i> Printed 3/8/2024 Page 14
)0-20.00 hrs, dt=0.05 hrs, 3 R-20 method, UH=SCS, V		
Reach routing by Stor-Ind+	, , ,	0	nd method
SubcatchmentA1: Flow to resized	Runoff Area=450,410 sf 4 Flow Length=690' Tc=9.6		•
SubcatchmentA2: Uncontrolled flow		•	ious Runoff Depth>0.36" Runoff=0.2 cfs 0.027 af
Reach A: Design Point A: Flow To Wetla	nd		Inflow=1.3 cfs 0.817 af
-			Outflow=1.3 cfs 0.817 af
Pond P1: Resized Detention Basin w/ net	₩ Peak Elev=33.26' Stora	age=94,465 cf	Inflow=27.3 cfs 2.066 af
			Outflow=1.3 cfs 0.790 af
Total Runoff Area = 11.			rage Runoff Depth = 2.24" .66% Impervious = 5.1 ac

Summary for Subcatchment A1: Flow to resized Detention Basin

Runoff = 27.3 cfs @ 12.14 hrs, Volume= 2.066 af, Depth> 2.40" Routed to Pond P1 : Resized Detention Basin w/ new OCS

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.95"

	A	rea (sf)	CN [Description		
*		7,841	98 p	aved side	walks, HSG	6 A
		47,778	45 N	Voods, Poo	or, HSG A	
	1	77,900	98 F	Paved park	ing, HSG A	N Contraction of the second seco
		79,926	39 >	•75% Gras	s cover, Go	bod, HSG A
		32,875	98 \	Vater Surfa	ace, HSG A	N Contraction of the second seco
*		94,298	76 (Gravel area	as, HSG A	
*		4,792				d roofs, HSG A
*		5,000	76 F	Field Trans	mission Ma	aterial Storage area, HSG A
	4	50,410	77 \	Veighted A	verage	
		27,002	Ę	50.40% Pei	rvious Area	
	2	23,408	2	19.60% Imp	pervious Ar	ea
	_					
	Tc	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	4.3	50	0.0400	0.20		Sheet Flow, A-B
						Grass: Short n= 0.150 P2= 3.20"
	5.3	640	0.0100	2.03		Shallow Concentrated Flow, B-C
						Paved Kv= 20.3 fps
	9.6	690	Total			



Subcatchment A1: Flow to resized Detention Basin

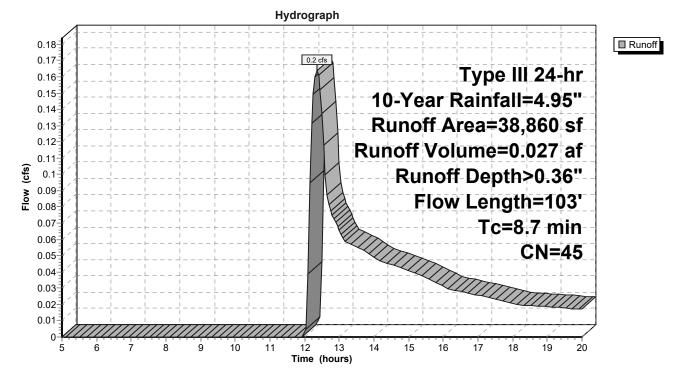
Summary for Subcatchment A2: Uncontrolled flow

Runoff = 0.2 cfs @ 12.35 hrs, Volume= 0.027 af, Depth> 0.36" Routed to Reach A : Design Point A: Flow To Wetland

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=4.95"

_	A	rea (sf)	CN E	Description		
		38,860	45 V	Voods, Po	or, HSG A	
_	38,860 100.00% Pervious Area					a
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	8.5	50	0.0500	0.10		Sheet Flow, A-B
_	0.2	53	0.0900	4.83		Woods: Light underbrush n= 0.400 P2= 3.20" Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps
_	8.7	103	Total			

Subcatchment A2: Uncontrolled flow

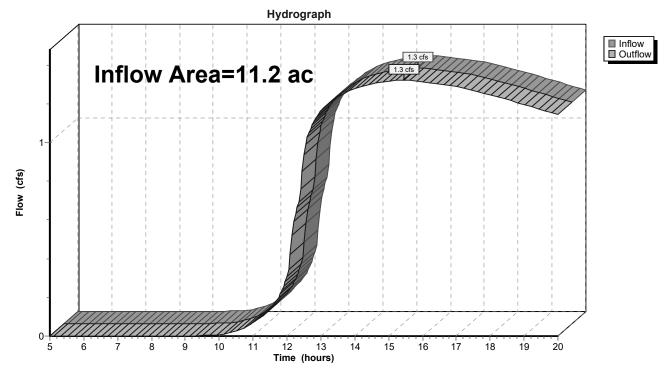


Summary for Reach A: Design Point A: Flow To Wetland

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	11.2 ac, 45.66% Impervious, Inflow Depth > 0.87" for 10-Year ever	nt
Inflow	=	1.3 cfs @ 15.44 hrs, Volume= 0.817 af	
Outflow	=	1.3 cfs @ 15.44 hrs, Volume= 0.817 af, Atten= 0%, Lag= 0	0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Reach A: Design Point A: Flow To Wetland

Summary for Pond P1: Resized Detention Basin w/ new OCS

Inflow Area = 10.3 ac, 49.60% Impervious, Inflow Depth > 2.40" for 10-Year event Inflow = 27.3 cfs @ 12.14 hrs, Volume= 2.066 af Outflow = 1.3 cfs @ 15.71 hrs, Volume= 0.790 af, Atten= 95%, Lag= 213.9 min Primary = 1.3 cfs @ 15.71 hrs, Volume= 0.790 af Routed to Reach A : Design Point A: Flow To Wetland 0.790 af									
Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Starting Elev= 30.80' Surf.Area= 20,690 sf Storage= 32,247 cf Peak Elev= 33.26'@ 15.71 hrs Surf.Area= 29,793 sf Storage= 94,465 cf (62,218 cf above start)									
Center-	of-Mass de	t. time= 168	8.3 min (9	lculated for 0.050 a 65.0 - 796.6)					
Volume				Storage Descriptio					
#1	29.00	J' 14	3,189 cf	Custom Stage Da	ata (Irregular)Listed	below			
Elevati	on S	Surf.Area	Perim.	Inc.Store	Cum.Store	Wet.Area			
(fe		(sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	<u>(sq-ft)</u>			
29.	00	14,700	950.0	0	0	14,700			
30.		18,250	1,005.0	16,443	16,443	23,312			
31.		21,300	1,220.0	19,755	36,198	61,396			
32.		25,150	1,250.0	23,198	59,397	67,421			
33.		28,800	1,260.0	26,954	86,351	69,780			
34.		32,550	1,285.0	30,656	117,007	75,000			
34.	80	32,905	1,295.0	26,182	143,189	77,298			
Device	Routing	Inv	ert Outle	et Devices					
#1	Primary	29.1		" Round Culvert					
	,				ng, no headwall, Ke				
					18' / 29.00' S= 0.0				
					P, smooth interior,				
#2	Device 1	30.8				d to weir flow at low heads			
#3	Device 1	32.5		Vert. Orifice/Grate					
#4	Device 1	33.8		ted to weir flow at lo	h Broad-Crested F	Poctangular Woir			
π	Device I	55.0		d (feet) 0.20 0.40					
					92 3.08 3.30 3.32				
#5	Device 1	34.5			ce/Grate X 8.00 col				
					I.0" x 24.0" Grate (4				
				0.000 11 2					

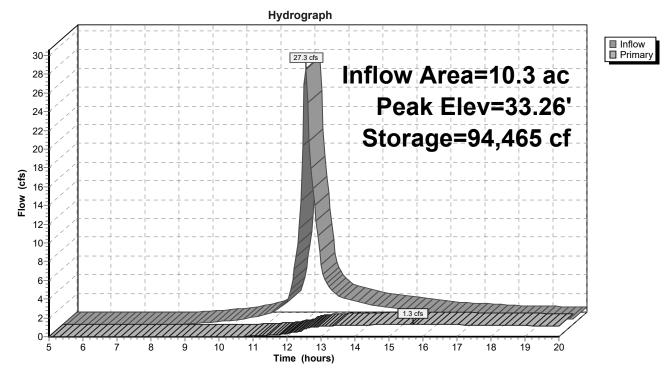
Primary OutFlow Max=1.3 cfs @ 15.71 hrs HW=33.26' (Free Discharge)

-1=Culvert (Passes 1.3 cfs of 21.0 cfs potential flow) -2=Orifice/Grate (Orifice Controls 0.6 cfs @ 7.30 fps)

-3=Orifice/Grate (Orifice Controls 0.6 cfs @ 3.72 fps)

-4=Broad-Crested Rectangular Weir (Controls 0.0 cfs)

-5=Orifice/Grate (Controls 0.0 cfs)



Pond P1: Resized Detention Basin w/ new OCS

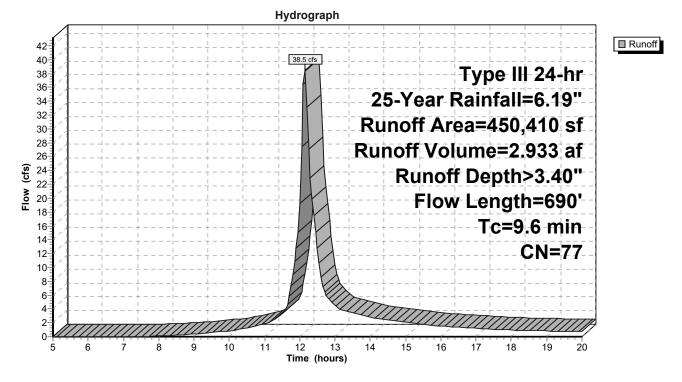
Post Drainage Calcs Prepared by CEC Inc <u>HydroCAD® 10.20-4b_s/n 01006_© 2023 Hyd</u>	<i>Type III 24-hr 25-Year Rainfall=6.19"</i> Printed 3/8/2024 droCAD Software Solutions LLC Page 21						
Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method							
SubcatchmentA1: Flow to resized	Runoff Area=450,410 sf 49.60% Impervious Runoff Depth>3.40" Flow Length=690' Tc=9.6 min CN=77 Runoff=38.5 cfs 2.933 af						
SubcatchmentA2: Uncontrolled flow	Runoff Area=38,860 sf 0.00% Impervious Runoff Depth>0.77" Flow Length=103' Tc=8.7 min CN=45 Runoff=0.5 cfs 0.057 af						
Reach A: Design Point A: Flow To Wetla	nd Inflow=2.5 cfs 1.305 af Outflow=2.5 cfs 1.305 af						
Pond P1: Resized Detention Basin w/ ne	♥ Peak Elev=34.00' Storage=116,916 cf Inflow=38.5 cfs 2.933 af Outflow=2.5 cfs 1.247 af						
Total Runoff Area = 11.	2 ac Runoff Volume = 2.990 af Average Runoff Depth = 3.19" 54.34% Pervious = 6.1 ac 45.66% Impervious = 5.1 ac						

Summary for Subcatchment A1: Flow to resized Detention Basin

Runoff = 38.5 cfs @ 12.14 hrs, Volume= 2.933 af, Depth> 3.40" Routed to Pond P1 : Resized Detention Basin w/ new OCS

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=6.19"

	A	rea (sf)	CN [Description		
*		7,841	98 p	aved side	walks, HSG	6 A
		47,778	45 N	Voods, Poo	or, HSG A	
	1	77,900	98 F	Paved park	ing, HSG A	N Contraction of the second seco
		79,926	39 >	•75% Gras	s cover, Go	bod, HSG A
		32,875	98 \	Vater Surfa	ace, HSG A	N Contraction of the second seco
*		94,298	76 (Gravel area	as, HSG A	
*		4,792				d roofs, HSG A
*		5,000	76 F	Field Trans	mission Ma	aterial Storage area, HSG A
	4	50,410	77 \	Veighted A	verage	
		27,002	Ę	50.40% Pei	rvious Area	
	2	23,408	2	19.60% Imp	pervious Ar	ea
	_					
	Tc	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	4.3	50	0.0400	0.20		Sheet Flow, A-B
						Grass: Short n= 0.150 P2= 3.20"
	5.3	640	0.0100	2.03		Shallow Concentrated Flow, B-C
						Paved Kv= 20.3 fps
	9.6	690	Total			



Subcatchment A1: Flow to resized Detention Basin

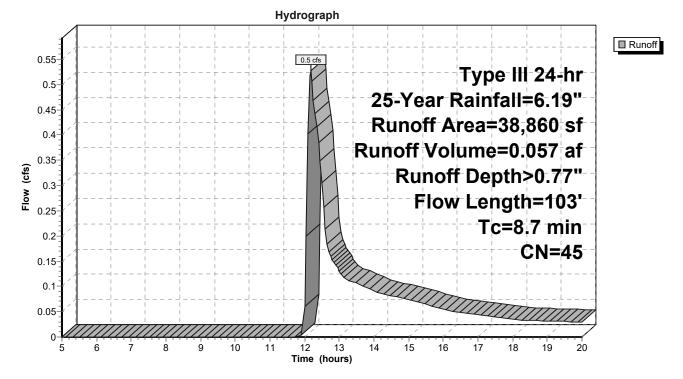
Summary for Subcatchment A2: Uncontrolled flow

Runoff = 0.5 cfs @ 12.17 hrs, Volume= 0.057 af, Depth> 0.77" Routed to Reach A : Design Point A: Flow To Wetland

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=6.19"

_	A	rea (sf)	CN E	Description		
		38,860	45 V	Voods, Po	or, HSG A	
		38,860	1	00.00% P	ervious Are	a
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	8.5	50	0.0500	0.10		Sheet Flow, A-B
_	0.2	53	0.0900	4.83		Woods: Light underbrush n= 0.400 P2= 3.20" Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps
_	8.7	103	Total			

Subcatchment A2: Uncontrolled flow

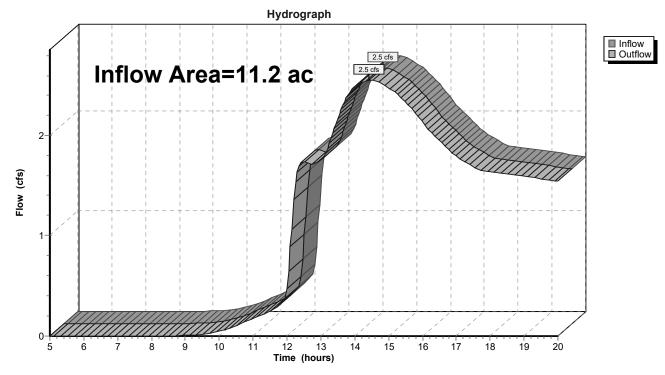


Summary for Reach A: Design Point A: Flow To Wetland

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	=	11.2 ac, 45.66	5% Impervio	us, Inflow	Depth > 1.39"	for 25-Year event
Inflow	=	2.5 cfs @	14.43 hrs, V	/olume=	1.305 af	
Outflow	=	2.5 cfs @	14.43 hrs, ∖	/olume=	1.305 af,	Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Reach A: Design Point A: Flow To Wetland

Summary for Pond P1: Resized Detention Basin w/ new OCS

Inflow Outflow Primary	Inflow Area =10.3 ac, 49.60% Impervious, Inflow Depth > 3.40"for 25-Year eventInflow =38.5 cfs @12.14 hrs, Volume=2.933 afOutflow =2.5 cfs @14.46 hrs, Volume=1.247 af, Atten= 94%, Lag= 139.4 minPrimary =2.5 cfs @14.46 hrs, Volume=1.247 afRouted to Reach A : Design Point A: Flow To Wetland1.247 af									
Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Starting Elev= 30.80' Surf.Area= 20,690 sf Storage= 32,247 cf Peak Elev= 34.00' @ 14.46 hrs Surf.Area= 32,539 sf Storage= 116,916 cf (84,668 cf above start)										
Plug-Flow detention time= 420.6 min calculated for 0.507 af (17% of inflow) Center-of-Mass det. time= 159.0 min (947.6 - 788.6)										
Volume	Inver			Storage Descriptio						
#1	29.00)' 143, ⁻	89 cf	Custom Stage Da	ta (Irregular)Listed	below				
Elevatio	an C	Surf.Area	^{>} erim.	Inc.Store	Cum.Store	Wet.Area				
(fee		(sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	(sq-ft)				
29.0	_/	14,700	950.0	0	0	14,700				
30.0		,	,005.0	16,443	16,443	23,312				
31.0	00	21,300 1	,220.0	19,755	36,198	61,396				
32.0	00	25,150 1	,250.0	23,198	59,397	67,421				
33.0	00		,260.0	26,954	86,351	69,780				
34.0			,285.0	30,656	117,007	75,000				
34.8	30	32,905 1	,295.0	26,182	143,189	77,298				
Device	Routing	Invert	Outl	et Devices						
<u>====</u> #1	Primary	29.18		" Round Culvert						
π I	Timary	23.10			ıg, no headwall, Ke	= 0 900				
					18' / 29.00' S= 0.00					
					P, smooth interior, F					
#2	Device 1	30.80				to weir flow at low heads				
#3	Device 1	32.50		Vert. Orifice/Grate						
				ted to weir flow at lo						
#4	Device 1	33.83	4.0'	long x 0.5' breadtl	h Broad-Crested Re	ectangular Weir				
			Hea	d (feet) 0.20 0.40	0.60 0.80 1.00	-				
			Coe	f. (English) 2.80 2.9	92 3.08 3.30 3.32					
#5	Device 1	34.50	2.0"	x 2.0" Horiz. Orific	ce/Grate X 8.00 colu	umns				
					.0" x 24.0" Grate (44	1% open area)				
			Limi	ted to weir flow at lo	wheads					

Limited to weir flow at low heads

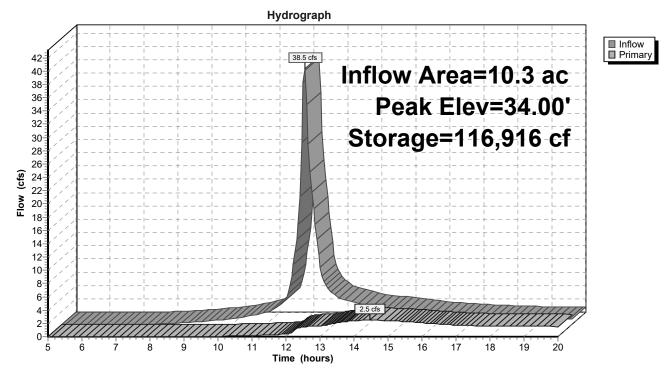
Primary OutFlow Max=2.5 cfs @ 14.46 hrs HW=34.00' (Free Discharge)

1=Culvert (Passes 2.5 cfs of 23.3 cfs potential flow) **2=Orifice/Grate** (Orifice Controls 0.7 cfs @ 8.38 fps)

-3=Orifice/Grate (Orifice Controls 1.0 cfs @ 5.55 fps)

-4=Broad-Crested Rectangular Weir (Weir Controls 0.8 cfs @ 1.14 fps)

-5=Orifice/Grate (Controls 0.0 cfs)



Pond P1: Resized Detention Basin w/ new OCS

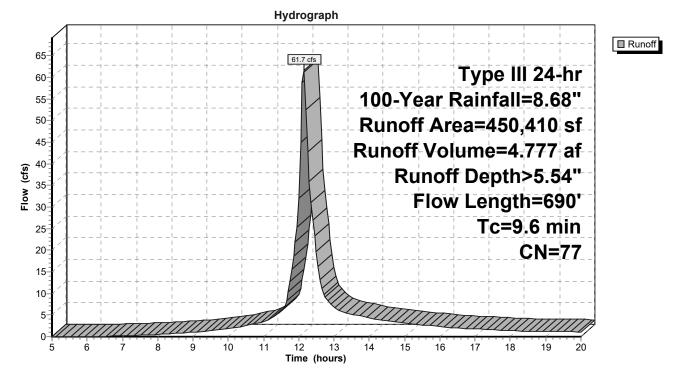
Post Drainage Calcs Prepared by CEC Inc HydroCAD® 10.20-4b s/n 01006 © 2023 Hyd	Type III 24-hr 100-Year Rainfall=8.68" Printed 3/8/2024 droCAD Software Solutions LLC Page 28			
Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method				
SubcatchmentA1: Flow to resized	Runoff Area=450,410 sf 49.60% Impervious Runoff Depth>5.54" Flow Length=690' Tc=9.6 min CN=77 Runoff=61.7 cfs 4.777 af			
SubcatchmentA2: Uncontrolled flow	Runoff Area=38,860 sf 0.00% Impervious Runoff Depth>1.89" Flow Length=103' Tc=8.7 min CN=45 Runoff=1.7 cfs 0.141 af			
Reach A: Design Point A: Flow To Wetla	nd Inflow=18.0 cfs 3.110 af Outflow=18.0 cfs 3.110 af			
Pond P1: Resized Detention Basin w/ ne	✔ Peak Elev=34.76' Storage=141,808 cf Inflow=61.7 cfs 4.777 af Outflow=17.3 cfs 2.969 af			
Total Runoff Area = 11.	2 ac Runoff Volume = 4.917 af Average Runoff Depth = 5.25" 54.34% Pervious = 6.1 ac 45.66% Impervious = 5.1 ac			

Summary for Subcatchment A1: Flow to resized Detention Basin

Runoff = 61.7 cfs @ 12.14 hrs, Volume= 4.777 af, Depth> 5.54" Routed to Pond P1 : Resized Detention Basin w/ new OCS

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=8.68"

	A	rea (sf)	CN I	Description			
*		7,841	98	paved sidewalks, HSG A			
		47,778	45	Noods, Po	or, HSG A		
	1	77,900	98 I	Paved park	ing, HSG A	A	
		79,926	39 :	>75% Gras	s cover, Go	bod, HSG A	
		32,875	98	Nater Surfa	ace, HSG A	A	
*		94,298		Gravel area	,		
*		4,792				d roofs, HSG A	
*		5,000	76	Field Trans	mission Ma	aterial Storage area, HSG A	
	4	50,410		Weighted Average			
		27,002			rvious Area		
	2	23,408	4	19.60% Imp	pervious Ar	ea	
	_		<u>.</u>		• •	— • • • •	
	ŢĊ	Length	Slope	•	Capacity	Description	
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	4.3	50	0.0400	0.20		Sheet Flow, A-B	
						Grass: Short n= 0.150 P2= 3.20"	
	5.3	640	0.0100	2.03		Shallow Concentrated Flow, B-C	
						Paved Kv= 20.3 fps	
	9.6	690	Total				



Subcatchment A1: Flow to resized Detention Basin

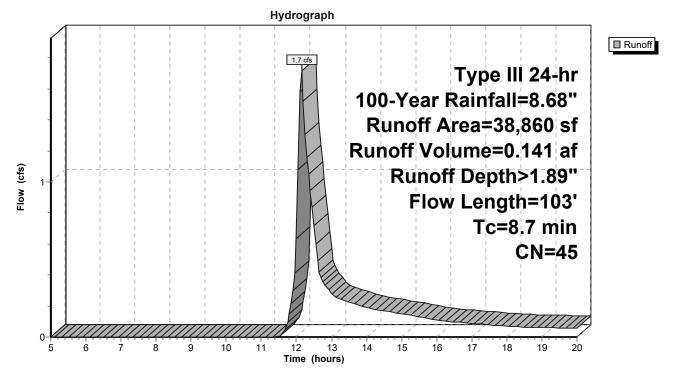
Summary for Subcatchment A2: Uncontrolled flow

Runoff = 1.7 cfs @ 12.15 hrs, Volume= 0.141 af, Depth> 1.89" Routed to Reach A : Design Point A: Flow To Wetland

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=8.68"

_	A	rea (sf)	CN E	Description		
		38,860	45 V	Voods, Po	or, HSG A	
_		38,860	100.00% Pervious Area			
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	8.5	50	0.0500	0.10		Sheet Flow, A-B
_	0.2	53	0.0900	4.83		Woods: Light underbrush n= 0.400 P2= 3.20" Shallow Concentrated Flow, B-C Unpaved Kv= 16.1 fps
	8.7	103	Total			

Subcatchment A2: Uncontrolled flow

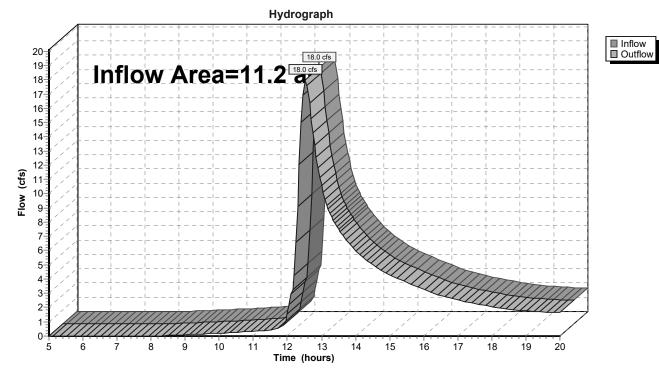


Summary for Reach A: Design Point A: Flow To Wetland

[40] Hint: Not Described (Outflow=Inflow)

Inflow Are	a =	11.2 ac, 45.66% Impervious, Inflow Depth > 3.32" for 100-Year event	
Inflow	=	18.0 cfs @ 12.53 hrs, Volume= 3.110 af	
Outflow	=	18.0 cfs @ 12.53 hrs, Volume= 3.110 af, Atten= 0%, Lag= 0.0	min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Reach A: Design Point A: Flow To Wetland

Summary for Pond P1: Resized Detention Basin w/ new OCS

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Inflow Area = 10.3 ac, 49.60% Impervious, Inflow Depth > 5.54" for 100-Year event Inflow = 61.7 cfs @ 12.14 hrs, Volume= 4.777 af Outflow = 17.3 cfs @ 12.54 hrs, Volume= 2.969 af, Atten= 72%, Lag= 24.1 min Primary = 17.3 cfs @ 12.54 hrs, Volume= 2.969 af Routed to Reach A : Design Point A: Flow To Wetland 12.54 hrs, Volume= 1.969 af							
Starting	Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Starting Elev= 30.80' Surf.Area= 20,690 sf Storage= 32,247 cf Peak Elev= 34.76' @ 12.54 hrs Surf.Area= 32,886 sf Storage= 141,808 cf (109,560 cf above start)						
Center-o	of-Mass det	. time= 93.1 ı	min (87	lculated for 2.222 a 70.3 - 777.2)	, , , , , , , , , , , , , , , , , , ,		
Volume				Storage Description			
#1	29.00	o' 143,	189 cf	Custom Stage Da	ata (Irregular)Liste	d below	
Elevatio	on S	Surf.Area	Perim.	Inc.Store	Cum.Store	Wet.Area	
(fee		(sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	(sq-ft)	
29.0	00	14,700	950.0	0	0	14,700	
30.0			,005.0	16,443	16,443	23,312	
31.0			,220.0	19,755	36,198	61,396	
32.0			,250.0	23,198	59,397	67,421	
33.0			,260.0	26,954	86,351	69,780	
34.0			,285.0	30,656	117,007	75,000	
34.8	80	32,905 1	,295.0	26,182	143,189	77,298	
Device	Routing	Inver	t Outl	et Devices			
#1	Primary	29.18	' 24.0	" Round Culvert			
	,		L= 3	5.0' CPP, projectir	ng, no headwall, K	e= 0.900	
						0051 '/' Cc= 0.900	
						Flow Area= 3.14 sf	
#2	Device 1	30.80				ed to weir flow at low heads	
#3	Device 1	32.50		Vert. Orifice/Grate			
			Limited to weir flow at low heads				
#4 Device 1 33.83' 4.0' long x 0.5' breadth Broad-Crested Rectangular Weir				Rectangular Weir			
	Head (feet) 0.20 0.40 0.60 0.80 1.00						
#5	Device 1	21 E0	Coef. (English) 2.80 2.92 3.08 3.30 3.32 34.50' 2.0" x 2.0" Horiz. Orifice/Grate X 8.00 columns				
#5	Device I	34.30		rows C= 0.600 in 2^2			
				ted to weir flow at lo			

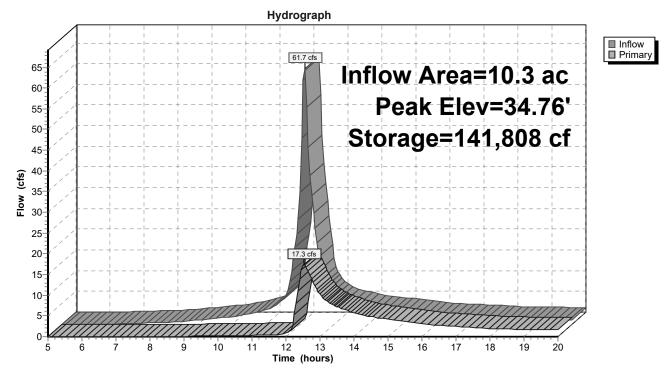
Primary OutFlow Max=17.2 cfs @ 12.54 hrs HW=34.76' (Free Discharge)

1=Culvert (Passes 17.2 cfs of 25.5 cfs potential flow) **2=Orifice/Grate** (Orifice Controls 0.8 cfs @ 9.37 fps)

-3=Orifice/Grate (Orifice Controls 1.2 cfs @ 6.96 fps)

-4=Broad-Crested Rectangular Weir (Weir Controls 11.8 cfs @ 3.19 fps)

-5=Orifice/Grate (Weir Controls 3.4 cfs @ 1.66 fps)



Pond P1: Resized Detention Basin w/ new OCS

TSS Calculations

INSTRUCTIONS:

1. In BMP Column, click on Blue Cell to Activate Drop Down Menu

2. Select BMP from Drop Down Menu

3. After BMP is selected, TSS Removal and other Columns are automatically completed.

	Location:	BMP Treatment Train 1]		
	В	С	D	E	F
	BMP ¹	TSS Removal Rate ¹	Starting TSS Load*	Amount Removed (C*D)	Remaining Load (D-E)
heet	Deep Sump and Hooded Catch Basin	0.25	1.00	0.25	0.75
TSS Removal Calculation Worksheet	Proprietary WQU (STC 900)	0.60	0.75	0.45	0.30
TSS Removal ulation Works	Wet Basin (w/Sediment Forebay)	0.80	0.30	0.24	0.06
TSS culati		0.00	0.06	0.00	0.06
Cal		0.00	0.06	0.00	0.06
		Total T	SS Removal =	94%	Separate Form Needs to be Completed for Each Outlet or BMP Train
	Prepared By:	Eversource Training Facility CJV 3/8/2024		*Equals remaining load fro which enters the BMP	— m previous BMP (E)

INSTRUCTIONS:

1. In BMP Column, click on Blue Cell to Activate Drop Down Menu

2. Select BMP from Drop Down Menu

3. After BMP is selected, TSS Removal and other Columns are automatically completed.

	Location:	BMP Treatment Train 2]		
	В	C TSS Removal	D Starting TSS	E Amount	F
	BMP ¹	Rate ¹	Load*	Removed (C*D)	Remaining Load (D-E)
heet	Proprietary WQU (STC 450i)	0.60	1.00	0.60	0.40
oval 'orksl	Wet Basin (w/Sediment Forebay)	0.80	0.40	0.32	0.08
TSS Removal Calculation Worksheet		0.00	0.08	0.00	0.08
TSS culati		0.00	0.08	0.00	0.08
Cal		0.00	0.08	0.00	0.08
		Total T	SS Removal =	92%	Separate Form Needs to be Completed for Each Outlet or BMP Train
	Prepared By:	Eversource Training Facility CJV 3/8/2024		*Equals remaining load from which enters the BMP	— m previous BMP (E)



UNIVERSITY OF MASSACHUSETTS

AT AMHERST Water Resources Research Center Blaisdell House, UMass 310 Hicks Way Amherst, MA 01003

(413) 545-5532 (413) 545-2304 FAX www.mastep.net

MASTEP Technology Review

- Technology Name: Stormceptor 450i.
- Studies Reviewed: Multi-Phase Physical Model Testing of a Stormceptor STC450i
- Date: March 14, 2009
- Reviewers: Jerry Schoen
- Rating: 2

Brief rationale for rating:

This laboratory study is generally well conducted and documented. No documentation of a quality assurance project, plan but quality control data was reported. Sediment analysis was done by the SSC method, but not the TSS method. Although SSC is considered by many scientists to be the preferred method, it is at odds with Massachusetts stormwater regulations, which are based on TSS treatment. Comparing SSC and TSS results is considered an inexact science.

TARP Requirements Not Met*:

- No documentation of a Quality Assurance Project Plan
- TSS analysis was not performed.

Other Comments

- SSC removal efficiency, calculated according to the NJDEP weighted formula, was 59.5 63.6%.
- SSC removal evaluated using event mean concentration and modified mass balance method, the latter considered to be a particularly accurate method of evaluating sediment removal in a laboratory setting.
- Particle Size Distribution (with d50 of 67 microns) closely matched the 55% sand, 40% silt, 5% clay mix recommended by NJDEP.
- A full range of flows (2% 125%) was tested.
- Scour test was performed at 500% of design flow. This is more rigorous than the 125% recommended for scour tests. Effluent concentrations for the scour tests ranged from 5.9 – 6.1mg/l, not considered a significant level of scour.

* Laboratory testing was based on the NJDEP TARP laboratory testing guidelines.



UNIVERSITY OF MASSACHUSETTS

AT AMHERST Water Resources Research Center Blaisdell House, UMass 310 Hicks Way Amherst, MA 01003

Massachusetts Stormwater Evaluation Project

(413) 545-5532 (413) 545-2304 FAX www.mastep.net

MASTEP Technology Review

- Technology Name: Stormceptor
- **Studies Reviewed:** Final NJCAT Technology Verification Stormceptor STC900 September 2004; Coventry University Study, 1996; Technology Assessment, University of Massachusetts, 1997; SeaTac Stormceptor Performance report 2001; SWAMP report Ontario 2004; Phoenix Group Edmonton report 1995; Stormceptor 1200 Field Evaluation report 2004; Applied Hydrology Associates Denver report 2003; Rinker Materials Como Park St. Paul MN report 2002; VA DOT / UVA "Testing of Ultra-Urban Stormwater Best Management Practices" report 2001. Hydrodynamic Separator Sediment Retention Testing, Mohseni, 2010.
- Date: September 17, 2013
- Reviewer: Jerry Schoen
- Rating: 2
- **Brief rationale for rating:** This rating is primarily based on the 2005 NJCAT Technology Verification study. In general, this was a well-conducted test, which in large part followed NJDEP test guidelines for laboratory studies, which MASTEP considers as the laboratory equivalent of TARP field protocols. Issues of concern: the study measured suspended sediment concentration (SSC) rather than total suspended solids (TSS). Although SSC is considered by many scientists to be the preferred method, it is at odds with Massachusetts stormwater regulations, which are based on TSS treatment. Comparing SSC and TSS results is considered an inexact science. The test was conducted with higher influent sediment concentrations than is preferred, but results were fairly consistent across all ranges studied. The particle size distribution also appears to be slightly higher than the target test range. There are additional field studies that in general support the results obtained in this laboratory studies. These studies do not satisfy TARP protocols, but they do not contradict results obtained in the NJCAT study.

TARP Requirements Not Met*:

- Measurements in TSS.
- Influent sediment concentration is 100 300 mg/l: actual was 153-460.
- No documentation of a Quality Assurance Project Plan
- Third party studies are preferred. This was conducted by Stormceptor personnel, with sample analyses conducted by an external laboratory.

Other Comments:

* The 2010 Mohseni study evaluates the susceptibility of the Stormceptor to scouring, or washout of collected sediments. Report concluded that the unit does not scour at high flows as long as sediment depth does not exceed maintenance level.

* Criteria also based on NJDEP laboratory testing guidelines.

Phosphorus Removal Calculations

INSTRUCTIONS:

1. In BMP Column, click on Blue Cell to Activate Drop Down Menu

2. Select BMP from Drop Down Menu (values obtained from Massachusetts Stormwater Handbook)

3. After BMP is selected, Phosphorus Removal and other Columns are automatically completed.

	Location:	37 Doty Street Wareham M			
	B BMP ¹	C Phosphorus Removal Rate ¹	D Starting Phosphorus Load*	E Amount Phosphorus Removed (C*D)	F Remaining Phosphorus Load (D-E)
val neet	Non-Use	0.33	1.00	0.33	0.67
Phosphorus Removal Calculation Worksheet	Wet Basin (w/Sediment Forebay)	0.60	0.67	0.40	0.27
on W		0.00	0.27	0.00	0.27
ospho culati		0.00	0.27	0.00	0.27
Pho Calo		0.00	0.27	0.00	0.27
		Total Phospho	rus Removal =	73%	Separate Form Needs to be Completed for Each Outlet or BMP Train
	Prepared By:	Eversource Training Facilty CJV 3/7/2024		*Equals remaining load fron which enters the BMP	n previous BMP (E)

Water Quality Volume Calculations



Water Quality Volume Flow Rate Calculations

Project Name: Eversource Training Facility Project Location: Wareham MA Project Number: 323-322 Date: 3/7/2024 Calculated By: CJV Checked By: BEP

Stormwater BMP:	STC 900	Description:	Flow to Stormce	eptor STC 900 Units
		Total Drainage Area:	150,140 3.45	-
		Total Impervious Area:	63,511 1.46	sq ft ac
	* Roof Areas are consid	red clean and are not subje	ect to WQV calculati	on
	Runo	off Depth to be Treated:	1.0	inches
	Required Wate	r Quality Volume:	5,293 0.122	cf ac ft
		FLOW RATE CONVE	RSION	
		Q = (qu)(A)(WQ)	V)	
Where:		ate associated with the c iit peak discharge, in csi	-	cfs
	A = imper	vious surface drainage a	area, in square mil	es
	WQV = water	quality volume in waters	shed inches	
Given:	1-acre = 5 minute = qu (1/2 -inch) =	0.00156 mi ² 0.083 hours 773 csm/in		
Calculation:				
	qu= 773 A= 1.46 WQV= 1.0	ac in		
	Required Wate	r Quality Flow Rate:	1.76	cfs
		tor STC 900 will pr ficiency for flows ເ		S Removal

(Based on Manufacturer's sizing. See attached documentation in Appendix D.)

* Flow rate conversion based on the Massachusetts Department of Environmental Protection Wetlands Program -Standard Method to Convert Required Water Quality Volume to a Discharge Rate for Sizing Flow Based Manufactured Proprietary Stormwater Treatment Practices Post Drainage CalcsType IIPrepared by CEC IncHydroCAD® 10.20-4b s/n 01006 © 2023 HydroCAD Software Solutions LLC

Stage-Area-Storage for Pond P1: Resized Detention Basin w/ new OCS

Elevation	Surface	Storage	Elevation	Surface	Storage
(feet)	(sq-ft)	(cubic-feet)	(feet)	(sq-ft)	(cubic-feet)
29.00	14,700	0	34.20	32,639	123,553
29.10	15,055	1,644	34.30	32,683	126,825
29.20	15,410	3,289	34.40	32,728	130,098
29.30	15,765	4,933	34.50	32,772	133,371
29.40	16,120	6,577	34.60	32,816	136,643
29.50	16,475	8,222	34.70	32,861	139,916
29.60	16,830	9,866	34.80	32,905	143,189
29.70	17,185	11,510			
29.80	17,540	13,154			
29.90	17,895	14,799			
30.00	18,250	16,443			
30.10	18,555	18,419			
30.20	18,860	20,394			
30.30	19,165	22,370			
30.40	19,470	24,345			
30.50	19,775	26,321			
30.60	20,080	28,296			
30.70	20,385	30,272			
30.80	20,690	32,247			
30.90	20,995	34,223			
31.00	21,300	36,198		LOW FLOW	ORIFICE
31.10	21,685	38,518		ELEVATION	I
31.20	22,070	40,838			•
31.30	22,455	43,158			
31.40	22,840	45,478			
31.50	23,225	47,798			
31.60	23,610	50,117			
31.70	23,995	52,437			
31.80	24,380	54,757			
31.90	24,765	57,077			
32.00	25,150	59,397			
32.10	25,515	62,092			
32.20	25,880	64,788			
32.30	26,245	67,483			
32.40	26,610	70,179			
32.50	26,975	72,874			
32.60	27,340	75,569			
32.70	27,705	78,265			
32.80	28,070	80,960			
32.90	28,435	83,656			
33.00	28,800	86,351			
33.10	29,175	89,417			
33.20	29,550	92,482			
33.30	29,925	95,548			
33.40	30,300	98,614			
33.50	30,675	101,679			
33.60	31,050	104,745			
33.70	31,425	107,810			
33.80	31,800	110,876			
33.90	32,175	113,941			
34.00	32,550	117,007			
34.10	32,594	120,280			
00	,	0,200			
			I		





Detailed Stormceptor Sizing Report – Flow to WQU-1

	Project Information & Location					
Project Name	Project Name Eversource training facility		50259			
City	Wareham	State/ Province	Massachusetts			
Country	United States of America	Date	3/7/2024			
Designer Information	1	EOR Information (optional)				
Name	chris Vandenberghe	Name				
Company CEC		Company				
Phone # 617-416-1964		Phone #				
Email	cvandenberghe@cecinc.com	Email				

Stormwater Treatment Recommendation

The recommended Stormceptor Model(s) which achieve or exceed the user defined water quality objective for each site within the project are listed in the below Sizing Summary table.

Site Name	Flow to WQU-1
Recommended Stormceptor Model	STC 900
Target TSS Removal (%)	80.0
TSS Removal (%) Provided	86
PSD	OK-110
Rainfall Station	HYANNIS

The recommended Stormceptor model achieves the water quality objectives based on the selected inputs, historical rainfall records and selected particle size distribution.

Stormceptor Sizing Summary		
Stormceptor Model	% TSS Removal Provided	
STC 450i	76	
STC 900	86	
STC 1200	86	
STC 1800	86	
STC 2400	89	
STC 3600	90	
STC 4800	92	
STC 6000	93	
STC 7200	94	
STC 11000	96	
STC 13000	96	
STC 16000	97	





Stormceptor

The Stormceptor oil and sediment separator is sized to treat stormwater runoff by removing pollutants through gravity separation and flotation. Stormceptor's patented design generates positive TSS removal for each rainfall event, including large storms. Significant levels of pollutants such as heavy metals, free oils and nutrients are prevented from entering natural water resources and the re-suspension of previously captured sediment (scour) does not occur. Stormceptor provides a high level of TSS removal for small frequent storm events that represent the majority of annual rainfall volume and pollutant load. Positive treatment continues for large infrequent events, however, such events have little impact on the average annual TSS removal as they represent a small percentage of the total runoff volume and pollutant load.

Design Methodology

Stormceptor is sized using PCSWMM for Stormceptor, a continuous simulation model based on US EPA SWMM. The program calculates hydrology using local historical rainfall data and specified site parameters. With US EPA SWMM's precision, every Stormceptor unit is designed to achieve a defined water quality objective. The TSS removal data presented follows US EPA guidelines to reduce the average annual TSS load. The Stormceptor's unit process for TSS removal is settling. The settling model calculates TSS removal by analyzing:

- Site parameters
- · Continuous historical rainfall data, including duration, distribution, peaks & inter-event dry periods
- Particle size distribution, and associated settling velocities (Stokes Law, corrected for drag)
- TSS load
- · Detention time of the system

Hydrology Analysis

PCSWMM for Stormceptor calculates annual hydrology with the US EPA SWMM and local continuous historical rainfall data. Performance calculations of Stormceptor are based on the average annual removal of TSS for the selected site parameters. The Stormceptor is engineered to capture sediment particles by treating the required average annual runoff volume, ensuring positive removal efficiency is maintained during each rainfall event, and preventing negative removal efficiency (scour). Smaller recurring storms account for the majority of rainfall events and average annual runoff volume, as observed in the historical rainfall data analyses presented in this section.

Rainfall Station			
State/Province	Massachusetts	Total Number of Rainfall Events	1268
Rainfall Station Name	HYANNIS	Total Rainfall (in)	531.6
Station ID #	3821	Average Annual Rainfall (in)	33.2
Coordinates	41°24'0"N, 70°10'47"W	Total Evaporation (in)	12.5
Elevation (ft)	50	Total Infiltration (in)	316.5
Years of Rainfall Data	14	Total Rainfall that is Runoff (in)	202.6

Notes

• Stormceptor performance estimates are based on simulations using PCSWMM for Stormceptor, which uses the EPA Rainfall and Runoff modules.

• Design estimates listed are only representative of specific project requirements based on total suspended solids (TSS) removal defined by the selected PSD, and based on stable site conditions only, after construction is completed.

• For submerged applications or sites specific to spill control, please contact your local Stormceptor representative for further design assistance.





Drainage Area		Up Stream Storage		
Total Area (acres)	3.75	Storage (ac-ft) Discharge (cfs)		arge (cfs)
Imperviousness %	40.0	0.000	0.	.000
Water Quality Objective	•	Up Stream	Flow Diversi	on
TSS Removal (%)	80.0	Max. Flow to Stormce	ptor (cfs)	
Runoff Volume Capture (%)		Design Details		
Oil Spill Capture Volume (Gal)		Stormceptor Inlet Invert Elev (ft)		
Peak Conveyed Flow Rate (CFS)		Stormceptor Outlet Invert Elev (ft)		
Water Quality Flow Rate (CFS)	1.79	Stormceptor Rim Elev (ft)		
		Normal Water Level Ele	evation (ft)	
		Pipe Diameter ((in)	
		Pipe Materia		
		Multiple Inlets ()	(/N)	No
		Grate Inlet (Y/I	N)	No

Particle Size Distribution (PSD)

Removing the smallest fraction of particulates from runoff ensures the majority of pollutants, such as metals, hydrocarbons and nutrients are captured. The table below identifies the Particle Size Distribution (PSD) that was selected to define TSS removal for the Stormceptor design.

	OK-110				
Particle Diameter (microns)	Distribution %	Specific Gravity			
1.0	0.0	2.65			
53.0	3.0	2.65			
75.0	15.0	2.65			
88.0	25.0	2.65			
106.0	41.0	2.65			
125.0	15.0	2.65			
150.0	1.0	2.65			
212.0	0.0	2.65			





Site Name		Flow to WQU-1
Site Details		
Drainage Area		Infiltration Parameters
Total Area (acres)	3.75	Horton's equation is used to estimate infiltration
Imperviousness %	40.0	Max. Infiltration Rate (in/hr)2.44
Surface Characteristics	\$	Min. Infiltration Rate (in/hr)0.4
Width (ft)	808.00	Decay Rate (1/sec) 0.00055
Slope %	2	Regeneration Rate (1/sec)0.01
Impervious Depression Storage (in)	0.02	Evaporation
Pervious Depression Storage (in)	0.2	Daily Evaporation Rate (in/day)0.1
Impervious Manning's n	0.015	Dry Weather Flow
Pervious Manning's n	0.25	Dry Weather Flow (cfs) 0
Maintenance Frequency	y	Winter Months
Maintenance Frequency (months) >	12	Winter Infiltration0
	TSS Loadin	ng Parameters
TSS Loading Function		
Buildup/Wash-off Parame	eters	TSS Availability Parameters
Target Event Mean Conc. (EMC) mg/L		Availability Constant A
Exponential Buildup Power		Availability Factor B
Exponential Washoff Exponent		Availability Exponent C
		Min. Particle Size Affected by Availability (micron)

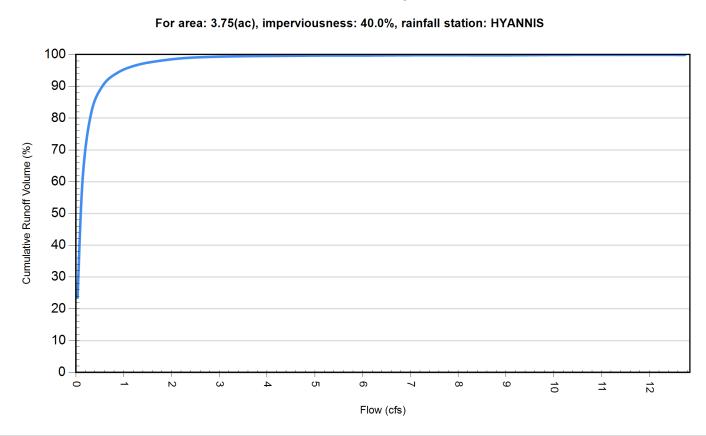




Cumulative Runoff Volume by Runoff Rate				
Runoff Rate (cfs)	Runoff Volume (ft ³)	Volume Over (ft ³)	Cumulative Runoff Volume (%)	
0.035	652498	2123146	23.5	
0.141	1693765	1081843	61.0	
0.318	2260682	514813	81.5	
0.565	2506124	269370	90.3	
0.883	2619165	156335	94.4	
1.271	2683061	92407	96.7	
1.730	2721225	54232	98.0	
2.260	2743631	31816	98.9	
2.860	2755188	20263	99.3	
3.531	2761184	14263	99.5	
4.273	2764968	10480	99.6	
5.085	2766662	8785	99.7	
5.968	2767958	7490	99.7	
6.922	2769101	6346	99.8	
7.946	2770139	5309	99.8	
9.041	2771124	4324	99.8	
10.206	2772173	3275	99.9	
11.442	2773029	2418	99.9	
12.749	2773813	1634	99.9	





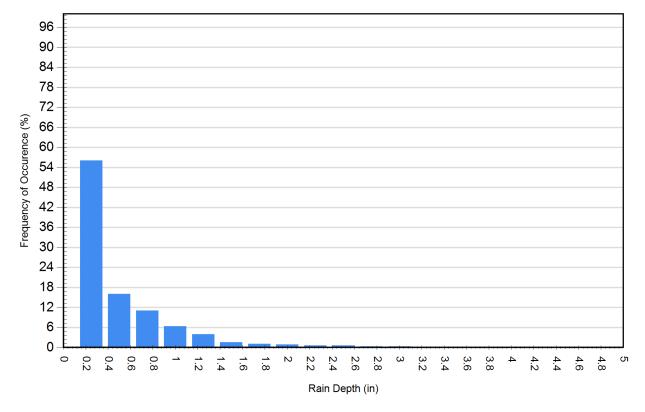






Rainfall Event Analysis				
Rainfall Depth (in)	No. of Events	Percentage of Total Events (%)	Total Volume (in)	Percentage of Annual Volume (%)
0.25	711	56.1	71	13.4
0.50	204	16.1	74	14.0
0.75	141	11.1	88	16.5
1.00	81	6.4	72	13.5
1.25	51	4.0	57	10.7
1.50	20	1.6	28	5.2
1.75	14	1.1	23	4.3
2.00	12	0.9	22	4.2
2.25	7	0.6	15	2.8
2.50	7	0.6	17	3.2
2.75	4	0.3	11	2.0
3.00	4	0.3	12	2.2
3.25	3	0.2	9	1.8
3.50	2	0.2	7	1.3
3.75	2	0.2	7	1.3
4.00	3	0.2	12	2.2
4.25	2	0.2	8	1.6
4.50	0	0.0	0	0.0
4.75	0	0.0	0	0.0

Frequency of Occurence by Rainfall Depths



Stormceptor Detailed Sizing Report - Page 7 of 8





For Stormceptor Specifications and Drawings Please Visit: https://www.conteches.com/technical-guides/search?filter=1WBC005EYX





Detailed Stormceptor Sizing Report – Flow to WQU-1

	Project Information & Location		
Project Name	Eversource training facility	Project Number	50259
City	Wareham	State/ Province	Massachusetts
Country	United States of America	Date	3/7/2024
Designer Information		EOR Information (o	ptional)
Name	chris Vandenberghe	Name	
Company	Company CEC		
Phone #	617-416-1964 Phone #		
Email	cvandenberghe@cecinc.com	Email	

Stormwater Treatment Recommendation

The recommended Stormceptor Model(s) which achieve or exceed the user defined water quality objective for each site within the project are listed in the below Sizing Summary table.

Site Name	Flow to WQU-1
Recommended Stormceptor Model	STC 450i
Target TSS Removal (%)	80.0
TSS Removal (%) Provided	80
PSD	OK-110
Rainfall Station	HYANNIS

The recommended Stormceptor model achieves the water quality objectives based on the selected inputs, historical rainfall records and selected particle size distribution.

Stormceptor Sizing Summary		
Stormceptor Model	% TSS Removal Provided	
STC 450i	80	
STC 900	88	
STC 1200	88	
STC 1800	89	
STC 2400	92	
STC 3600	92	
STC 4800	94	
STC 6000	94	
STC 7200	96	
STC 11000	97	
STC 13000	97	
STC 16000	98	





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Design Methodology

Stormceptor is sized using PCSWMM for Stormceptor, a continuous simulation model based on US EPA SWMM. The program calculates hydrology using local historical rainfall data and specified site parameters. With US EPA SWMM's precision, every Stormceptor unit is designed to achieve a defined water quality objective. The TSS removal data presented follows US EPA guidelines to reduce the average annual TSS load. The Stormceptor's unit process for TSS removal is settling. The settling model calculates TSS removal by analyzing:

- Site parameters
- · Continuous historical rainfall data, including duration, distribution, peaks & inter-event dry periods
- Particle size distribution, and associated settling velocities (Stokes Law, corrected for drag)
- TSS load
- · Detention time of the system

Hydrology Analysis

PCSWMM for Stormceptor calculates annual hydrology with the US EPA SWMM and local continuous historical rainfall data. Performance calculations of Stormceptor are based on the average annual removal of TSS for the selected site parameters. The Stormceptor is engineered to capture sediment particles by treating the required average annual runoff volume, ensuring positive removal efficiency is maintained during each rainfall event, and preventing negative removal efficiency (scour). Smaller recurring storms account for the majority of rainfall events and average annual runoff volume, as observed in the historical rainfall data analyses presented in this section.

	Rainfall Station			
State/Province	Massachusetts	Massachusetts Total Number of Rainfall Events 1		
Rainfall Station Name	HYANNIS	Total Rainfall (in)	531.6	
Station ID #	3821	Average Annual Rainfall (in)	33.2	
Coordinates	41°24'0"N, 70°10'47"W	Total Evaporation (in)	12.0	
Elevation (ft)	50	Total Infiltration (in)	321.7	
Years of Rainfall Data	14	Total Rainfall that is Runoff (in)	197.9	

Notes

• Stormceptor performance estimates are based on simulations using PCSWMM for Stormceptor, which uses the EPA Rainfall and Runoff modules.

• Design estimates listed are only representative of specific project requirements based on total suspended solids (TSS) removal defined by the selected PSD, and based on stable site conditions only, after construction is completed.

• For submerged applications or sites specific to spill control, please contact your local Stormceptor representative for further design assistance.





Drainage Area		Up Stream Storage		
Total Area (acres)	2.81	Storage (ac-ft) Discharge (cfs)		arge (cfs)
Imperviousness %	39.0	0.000	0	.000
Water Quality Objective	•	Up Stream	Flow Diversi	on
TSS Removal (%)	80.0	Max. Flow to Stormce	ptor (cfs)	
Runoff Volume Capture (%)		Design Details		•
Oil Spill Capture Volume (Gal)		Stormceptor Inlet Invert Elev (ft)		
Peak Conveyed Flow Rate (CFS)		Stormceptor Outlet Invert Elev (ft)		
Water Quality Flow Rate (CFS)	1.32	Stormceptor Rim Elev (ft)		
		Normal Water Level Ele	evation (ft)	
		Pipe Diameter ((in)	
		Pipe Materia		
		Multiple Inlets ()	(/N)	No
		Grate Inlet (Y/I	N)	No

Particle Size Distribution (PSD)

Removing the smallest fraction of particulates from runoff ensures the majority of pollutants, such as metals, hydrocarbons and nutrients are captured. The table below identifies the Particle Size Distribution (PSD) that was selected to define TSS removal for the Stormceptor design.

	OK-110				
Particle Diameter (microns)	Distribution %	Specific Gravity			
1.0	0.0	2.65			
53.0	3.0	2.65			
75.0	15.0	2.65			
88.0	25.0	2.65			
106.0	41.0	2.65			
125.0	15.0	2.65			
150.0	1.0	2.65			
212.0	0.0	2.65			





Site Name		Flow to WQU-1
Site Details		Details
Drainage Area		Infiltration Parameters
Total Area (acres)	2.81	Horton's equation is used to estimate infiltration
Imperviousness %	39.0	Max. Infiltration Rate (in/hr)2.44
Surface Characteristics	5	Min. Infiltration Rate (in/hr)0.4
Width (ft)	700.00	Decay Rate (1/sec) 0.00055
Slope %	2	Regeneration Rate (1/sec)0.01
Impervious Depression Storage (in)	0.02	Evaporation
Pervious Depression Storage (in)	0.2	Daily Evaporation Rate (in/day)0.1
Impervious Manning's n	0.015	Dry Weather Flow
Pervious Manning's n	0.25	Dry Weather Flow (cfs) 0
Maintenance Frequency	y	Winter Months
Maintenance Frequency (months) >	12	Winter Infiltration0
	TSS Loading	ng Parameters
TSS Loading Function		
Buildup/Wash-off Parame	eters	TSS Availability Parameters
Target Event Mean Conc. (EMC) mg/L		Availability Constant A
Exponential Buildup Power		Availability Factor B
Exponential Washoff Exponent		Availability Exponent C
	-	Min. Particle Size Affected by Availability (micron)

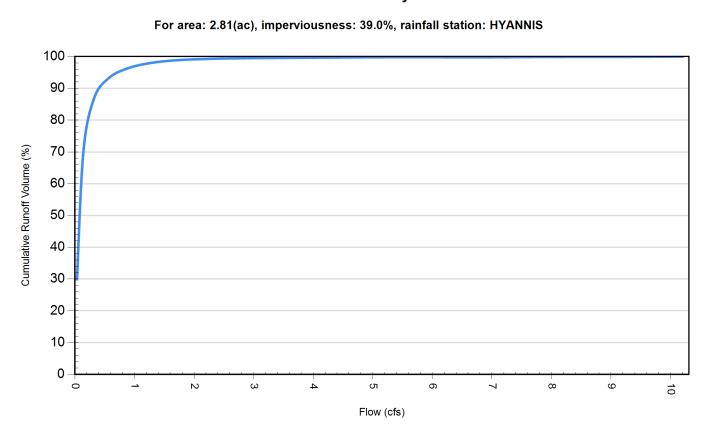




Cumulative Runoff Volume by Runoff Rate					
Runoff Rate (cfs)	Runoff Volume (ft ³)	Volume Over (ft ³)	Cumulative Runoff Volume (%)		
0.035	607280	1424807	29.9		
0.141	1418983	613103	69.8		
0.318	1762463	269635	86.7		
0.565	1893465	138635	93.2		
0.883	1956438	75674	96.3		
1.271	1990918	41197	98.0		
1.730	2009613	22503	98.9		
2.260	2018319	13797	99.3		
2.860	2022645	9471	99.5		
3.531	2024896	7221	99.6		
4.273	2026021	6096	99.7		
5.085	2027039	5078	99.8		
5.968	2027986	4131	99.8		
6.922	2028844	3272	99.8		
7.946	2029766	2351	99.9		
9.041	2030424	1692	99.9		
10.206	2031124	993	100.0		





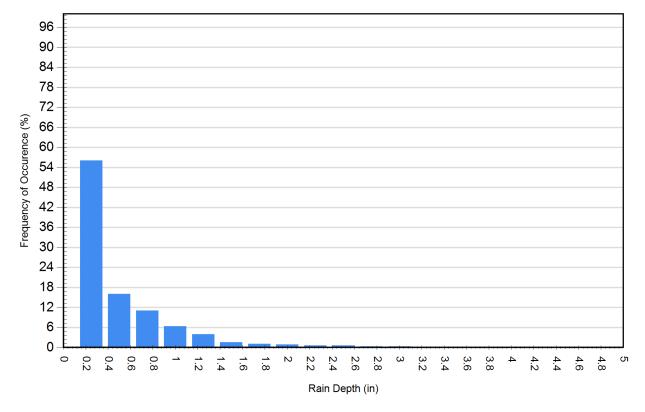






Rainfall Event Analysis						
Rainfall Depth (in)	No. of Events	Percentage of Total Events (%)	Total Volume (in)	Percentage of Annual Volume (%)		
0.25	711	56.1	71	13.4		
0.50	204	16.1	74	14.0		
0.75	141	11.1	88	16.5		
1.00	81	6.4	72	13.5		
1.25	51	4.0	57	10.7		
1.50	20	1.6	28	5.2		
1.75	14	1.1	23	4.3		
2.00	12	0.9	22	4.2		
2.25	7	0.6	15	2.8		
2.50	7	0.6	17	3.2		
2.75	4	0.3	11	2.0		
3.00	4	0.3	12	2.2		
3.25	3	0.2	9	1.8		
3.50	2	0.2	7	1.3		
3.75	2	0.2	7	1.3		
4.00	3	0.2	12	2.2		
4.25	2	0.2	8	1.6		
4.50	0	0.0	0	0.0		
4.75	0	0.0	0	0.0		

Frequency of Occurence by Rainfall Depths



Stormceptor Detailed Sizing Report - Page 7 of 8



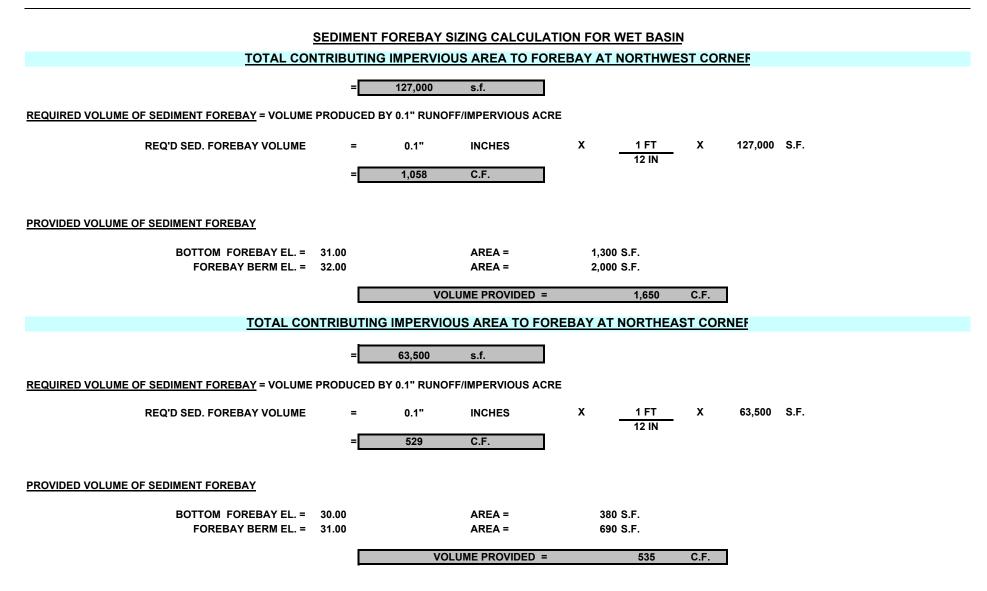


For Stormceptor Specifications and Drawings Please Visit: https://www.conteches.com/technical-guides/search?filter=1WBC005EYX Sediment Forebay Sizing Calculations

Sediment Forebay Calculation

Project Name:Eversource Training FacilityProject Location:37 Doty StreetProject Number:323-322

Date: 3/7/2024 Calculated By: CJV Checked By: BEP



APPENDIX D

SUPPORTING INFORMATION

Illicit Discharge Statement

Illicit Discharge Statement

ILLICIT DISCHARGE COMPLIANCE STATEMENT

I VERIFY THAT NO ILLICIT DISCHARGES EXIST FROM THE EVERSOURCE TRAINING FACILITY DEVELOPMENT. THROUGH THE IMPLEMENTATION OF THE *CONSTRUCTION PERIOD POLLUTION PREVENTION AND SEDIMENTATION AND EROSION CONTROL PLAN* AS WELL AS THE *OPERATION AND MAINTENANCE PLAN*, MEASURES ARE SET FORTH TO PREVENT ILLICIT DISCHARGES FROM ENTERING THE STORMWATER MANAGEMENT DRAINAGE SYSTEM.

<u>Jason St. Martin</u> SIGNATURE	Jason St Martin	3-8-24
SIGNATURE	PRINT NAME	DATE
Manager Facilities Operations	Eversource Energy	
TITLE	COMPANY	
SIGNATURE	PRINT NAME	DATE
SIGNATURE		DATE

NOTE: THIS CERTIFICATION MUST BE SIGNED BEFORE STORMWATER IS CONVEYED TO THE PROPOSED STORMWATER DRAINAGE SYSTEM IN ACCORDANCE WITH STANDARD 10 OF THE MASSACHUSETTS STORMWATER MANAGEMENT STANDARDS.

COMPANY

Civil & Environmental Consultants, Inc.

TITLE

37 Doty Street Wareham MA October 2023